On Robust Inference in Time Series Regression

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Abstract: Least squares regression with heteroskedasticity consistent standard errors ("OLS-HC regression") has proved very useful in cross section environments. However, several major difficulties, which are generally overlooked, must be confronted when transferring the HC technology to time series environments via heteroskedasticity and autocorrelation consistent standard errors ("OLS-HAC regression"). First, in plausible time-series environments, OLS parameter estimates can be inconsistent, so that OLS-HAC inference fails even asymptotically. Second, most economic time series have autocorrelation, which renders OLS parameter estimates inefficient. Third, autocorrelation similarly renders conditional predictions based on OLS parameter estimates inefficient. Finally, the structure of popular HAC covariance matrix estimators is ill-suited for capturing the autoregressive autocorrelation typically present in economic time series, which produces large size distortions and reduced power in HAC-based hypothesis testing, in all but the largest samples. We show that all four problems are largely avoided by the use of a simple and easily-implemented dynamic regression procedure, which we call DURBIN. We demonstrate the advantages of DURBIN with detailed simulations covering a range of practical issues.

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Key Words: Serial correlation, heteroskedasticity and autocorrelation consistent (HAC) regression, Durbin regression, dynamic regression

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1 Introduction

For nearly a century, regression with heteroskedastic and/or autocorrelated disturbances has featured prominently in empirical economics research. For many decades, attention centered on modeling the heteroskedasticity or autocorrelation in the context of feasible generalized least squares (FGLS) estimation.

The dominant estimation approach in recent decades, however, is ordinary least squares (OLS) with standard errors adjusted to achieve valid asymptotic inference without taking a stand on the form of heteroskedasticity or autocorrelation. The idea traces to the classic contribution of White (1980), who considered OLS regression with heteroskedasticity consistent (HC) standard errors ("OLS-HC regression") in cross-sectional environments, where sample sizes are typically very large, little or no information is available regarding the form of any possible heteroskedasticity, and serial correlation is irrelevant. In such environments HC standard errors are appropriate and justly emphasized (e.g. Angrist and Pischke (2008)).

In an elegant extension, Newey and West (1987) generalize White's estimator from cross sections to time series, with possible heteroskedasticity *and* serial correlation, by replacing White's covariance matrix estimator with an appropriate time-series analog based on an estimator of a spectral density at frequency zero.¹ Such OLS regression with heteroskedasticity and autocorrelation consistent (HAC) standard errors ("OLS-HAC regression") has become extremely popular in time series environments.

In this paper we argue, however, that, in contrast to cross section OLS-HC regression, time series OLS-HAC regression as typically implemented is likely to be problematic, for a variety of reasons:

1. In plausible time-series environments, OLS parameter estimates can be inconsistent, so that OLS-HAC inference fails even asymptotically.

And moreover, even when OLS parameter estimates are consistent:

- 2. OLS parameter estimates can be highly inefficient in the presence of serial correlation, compared to estimators that account for the serial correlation.
- 3. OLS-HAC regression discards valuable predictive information in serially-correlated disturbances and hence produces sub-optimal (inefficient) forecasts, whereas accurate outof-sample prediction is often a central concern in time series econometrics.

¹The Newey-West estimator collapses to the White (1980) estimator if serial correlation is absent, but appropriately incorporates serial correlation in the calculation of robust standard errors when serial correlation is present.

4. Newey-West-style HAC covariance matrix estimators are ill-suited for capturing the autoregressive autocorrelation typically present in economic time series, which can produce large size distortions, and large power reductions even when the size is not distorted.

Claim 1 is not widely appreciated, with the exception of Perron and González-Coya (2022), whose results and approach complement ours.² Claim 2 is well known, but its importance in finite samples is ignored when using OLS-HAC regression. Claim 3 is obvious, but again ignored when using OLS-HAC regression. Claim 4 is appreciated and has motivated several important refinements of the Newey-West HAC covariance matrix estimator (e.g., Andrews (1991), Kiefer and Vogelsang (2002), Lazarus et al. (2018)), as well as use of spectral density estimators that differ from the Newey-West lag-window estimator (e.g., Müller (2014)). However, those refinements have been only partially successful.

Against the background of the above claims 1-4, which we will substantiate in detail, we proceed to make a constructive contribution. We propose an alternative to OLS-HAC regression based on so-called "Durbin regressions" (Durbin (1970)). Working in a very general environment that includes most dynamic specifications of interest as special cases, we show that the new procedure simultaneously addresses claims 1-4 above. Indeed, the Durbin regression procedure performs well in all situations, dominating the traditional OLS-HAC and FGLS procedures.

Our paper proceeds as follows. In section 2 we introduce the basic data-generating process and estimators, including not only traditional OLS-HAC regression and our Durbin regression, but also traditional FGLS and a recently-proposed modified FGLS procedure. In section 3 we present a generalized modeling framework. In section 4 we present extensive simulation evidence. We conclude in section 5, and we present supplementary results in three Appendices.

2 Data Generating Process and Estimators

Traditional OLS-HAC regression focuses exclusively on OLS parameter estimation, assuming consistency and surrendering on efficiency. But, as we emphasize in this section, even OLS

²By now parts of our paper and theirs are entangled. A preliminary version of our paper was presented at the 2016 NBER-NSF Time Series Conference at Columbia University. Our first-draft working paper was released in March 2022, with no knowledge of their work-in-progress. Their first-draft working paper was released in September 2022, with knowledge of ours. Our second-draft working paper was released in June 2022, with knowledge of theirs. This third draft of our paper was released on May 29, 2024.

consistency cannot be assumed without significant loss of generality. Moreover, aspects of the consistency and efficiency of OLS and various competitors, under various conditions, are nuanced and not widely appreciated. Hence in this section we begin by reviewing aspects of OLS consistency and efficiency in comparison to competitors – in particular, a new procedure that we propose based on Durbin (1970) regressions, a new modified FGLS procedure, and traditional FGLS – in a sequence of progressively-richer dynamic environments.

2.1 Data-Generating Process

We start with the standard data-generating process (DGP) in the OLS-HAC regression literature,

$$y_t = x_t'\beta + u_t,\tag{1}$$

where $t = 1, 2, ..., T, \beta$ is a k-vector of parameters, x_t is a k-vector of covariance-stationary covariates and u_t is a scalar covariance-stationary disturbance with $E(u_t u'_t) = \sigma^2 \Omega$.³ DGP (1) is usually augmented with conditions such that OLS is consistent. Then the econometrician generally aims to provide standard error corrections that enable asymptotically valid inference. Note that such OLS-HAC regression involves just a static regression of y_t on x_t , basically imported directly from cross-sectional micro-econometrics, with dynamics allowed only through u_t . We will later argue that such a framework is uncompelling in time-series environments, but it is the industry standard in OLS-HAC regression, so we maintain it for now.

Crucial insights will flow from adopting a starting point that allows for significant generality regarding possible relationships between x_t and u_t . In particular, consider the Wold representation of the Gaussian vector process $z_t = (x'_t, u_t)'$,

$$z_t = \sum_{i=0}^{\infty} \Xi_i \varepsilon_{t-i}.$$
 (2)

³Because u_t is covariance-stationary, it can be serially correlated and/or conditionally heteroskedastic. In this paper we emphasize serial correlation exclusively, because serial correlation is the unique feature of time-series data relative to cross-section data. Cross sections do of course sometimes have a spatial dimension and therefore a natural ordering in space if not in time, and spatial correlation has recently begun to receive attention from a HAC estimation perspective, as in Müller and Watson (2022). Spatial HAC estimation is, however, beyond the scope of this paper.

The coefficient matrices are $\Xi_0 = I$ and

$$\Xi_i = \begin{pmatrix} \xi_{x,i} & \xi_{xu,i} \\ \xi'_{ux,i} & \xi_{u,i} \end{pmatrix},$$

and $\varepsilon_t = (\varepsilon'_{x,t}, \varepsilon_{u,t})'$ is a vector white noise innovation process with $E(\varepsilon_t) = 0$ and $E(\varepsilon_t \varepsilon'_s) = 0$ for $s \neq t$, and contemporaneous covariance matrix $E(\varepsilon_t \varepsilon'_t) = \Sigma$, where

$$\Sigma = \begin{pmatrix} \Sigma_x & \Sigma_{xu} \\ \Sigma'_{xu} & \sigma_u \end{pmatrix}.$$

Under mild regularity conditions, the infinite vector moving-average representation (2) is equivalent to the infinite vector-autoregressive (VAR) representation⁴

$$z_t = \sum_{i=1}^{\infty} \Psi_i z_{t-i} + \varepsilon_t, \tag{3}$$

where

$$\Psi_i = \begin{pmatrix} \Psi_{x,i} & \Psi_{xu,i} \\ \Psi_{ux,i} & \psi_{u,i} \end{pmatrix}.$$

This setting encompasses a variety of DGPs, and we will consider the consistency and efficiency properties of different estimators under various restrictions imposed on (3).

We now proceed to consider various estimation strategies that may be appropriate in the environment given by (1) and (3).

2.2 OLS Parameter Estimation and HAC Covariance Matrix Estimation

The OLS estimator of the regression parameter is of course

$$\hat{\beta} = (X'X)^{-1}X'Y.$$

If $\Omega = I$, the limiting distribution of the OLS estimator is

$$T^{1/2}\left(\hat{\beta}_{OLS}-\beta\right) \to N\left(0,\sigma^2 Q^{-1}\right),$$

⁴Such regularity conditions include assumptions on the rate of decline of $\|\Xi_i\|$ towards zero as $i \to \infty$, for suitable norm $\|.\|$, to control the persistence of the process and to avoid phenomena such as long memory that complicate the analysis. For details see, e.g., Davidson (2002) and references cited therein.

where $Q = p \lim_{T \to \infty} (T^{-1}X'X)$.

Based on the VAR representation (3), we define "block diagonality" (BD) as holding when $\Psi_{ux,i} = \Psi_{xu,i} = 0$, for all *i*, and $\Sigma_{xu} = 0$. The BD condition implies strong exogeneity, namely that $E(u_s|x_t) = 0$ for all *s* and t.⁵ In the BD environment OLS is consistent but asymptotically inefficient, with limiting distribution

$$T^{1/2}(\hat{\beta}_{OLS} - \beta) \to N(0, V)$$

where $V = Q^{-1}\Omega Q^{-1}$. The key object in V is Ω , which is the spectrum of $x_t u_t$ at frequency zero. HAC inference estimates V using

$$\widehat{V} = Q^{-1}\widehat{\Omega}Q^{-1},$$

where $\widehat{\Omega}$ is a consistent estimator of Ω , so that \widehat{V} is consistent for V. Different choices for $\widehat{\Omega}$ therefore define different HAC covariance matrix estimators and are the main issue in implementing OLS-HAC regression, as we discuss subsequently in section 4.2.1.

2.3 FGLS Estimation

If condition BD holds, and if the matrix Ω is known, then GLS is a consistent and asymptotically efficient estimator of β . However, Ω is almost always unknown, in which case attention turns to FGLS as defined by Amemiya (1973), which is again both consistent and asymptotically efficient provided that condition BD holds.⁶

The OLS-HAC regression literature was historically motivated by environments where OLS is consistent for β , but where condition *BD* simultaneously fails in such a way that FGLS is inconsistent. Such situations are possible, and we will discuss a classic such situation (Hansen and Hodrick, 1980) at some length in section 3.4 below, but they are by no means the only or the most important possibility. Indeed there is much more to investigate when *BD* fails, as emphasized in the insightful work of Perron and González-Coya (2022).

We now consider an alternative estimation procedure that avoids the above discussed OLS-HAC and FGLS complications and *always* delivers consistent (and sometimes fully efficient) estimates of β , together with reliable asymptotic inference.

⁵Strong exogeneity is sometimes called strict exogeneity.

⁶Recent contributions to the FGLS literature include Romano and Wolf (2017) for heteroskedastic environments, and Kapetanios and Psaradakis (2016) for dynamic environments.

2.4 Durbin Estimation and its Relatives

A natural third approach to estimation and inference, which we will argue is generally preferable to both OLS-HAC and FGLS, is based on the "Durbin (1970) regression", given by

$$y_t = x'_t \beta + \sum_{j=1}^{\infty} \phi_j y_{t-j} + \sum_{j=1}^{\infty} x'_{t-j} \gamma_j + \varepsilon_{y,t}, \qquad (4)$$

where $\varepsilon_{y,t}$ is serially uncorrelated, and uncorrelated with y_{t-j} and x_{t-j} for all j. The Durbin regression "cleans out" disturbance dynamics by its direct inclusion of y_{t-j} and x_{t-j} , so that standard OLS estimation and inference are trustworthy. We refer to the Durbin regression, and the associated estimator of β , as DURBIN. Crucially, note well that the DGP remains (1) and (3); DURBIN is simply a certain procedure (regression) that can be implemented on data from that DGP, just as OLS and FGLS are certain procedures that can be implemented on data from that DGP.

Operationally, it is of course necessary to use a finite order approximation to the infinite order DURBIN regression (4),

$$y_{t} = x_{t}'\beta + \sum_{j=1}^{p} \phi_{j}y_{t-j} + \sum_{j=1}^{p} x_{t-j}'\gamma_{j} + \varepsilon_{y,t}, \qquad (5)$$

with finite lag order p selected using a data based procedure, typically an information criterion, and increasing at a suitable rate. The theoretical validity of such a procedure for producing valid asymptotic estimation and inference is well known (see, e.g., Lewis and Reinsel (1985) or Hannan and Deistler (1988)), and we shall have more to say about it when we later implement DURBIN in the simulations of section 4.

We can also write the finite order DURBIN approximation as

$$y_{t} = \sum_{j=1}^{p} \phi_{j} y_{t-j} + \sum_{i=1}^{k} \beta_{i} x_{i,t} + \sum_{j=1}^{p} \sum_{i=1}^{k} \gamma_{i,j} x_{i,t-j} + \varepsilon_{y,t},$$
(6)

which emphasizes the extent of the parameterization and lag structure. We will later explore in greater detail the relationship between the DGP given by (1) and (3) and the DURBIN regression (6), which is effectively one equation of a VAR and appears to be the originator of the autoregressive distributed lag (ADL) model model, which is widely used in empirical econometric work.

An estimator closely related to DURBIN, recently proposed by Perron and González-

Coya (2022), is a variation on FGLS. We refer to it as FGLS-D (short for "FGLS-Durbin"). While FGLS uses a first-stage OLS regression, FGLS-D uses a first-stage DURBIN regression (6). Under *BD*, it follows that FGLS-D is also efficient. However, when *BD* does not hold, FGLS-D may not be efficient or even consistent, while DURBIN remains consistent.

Given that condition BD may not hold, it is important to consider the implications of its violation for the various methods of estimation and inference. To see the effects of the various sub-conditions embedded in condition BD, we will relax it in sequential stages. First, we impose only that $\Psi_{ux,i} = 0$ for all i and that $\Sigma_{xu} = 0$, so that x is weakly exogenous (that is, $E(u_s|x_t) = 0, \forall s, t \leq s$) but not strongly exogenous.⁷ x_t now depends on lags of u_t , but not vice versa. We refer to this restriction as GEXOG ("GLS exogeneity"). Clearly, OLS is now inconsistent, as is FGLS, which uses OLS residuals, while FGLS-D remains consistent and efficient. Importantly, DURBIN remains consistent, even if not fully efficient, throughout.

Second, we impose only $\Sigma_{xu} = 0$, so that x is neither strongly nor weakly exogenous. We denote this condition by *EBD* ("error variance block diagonal"). u_t now depends on lags of x_t , and the finite-ordered FGLS autoregression for u_t is no longer valid. Therefore, neither FGLS nor FGLS-D is consistent. DURBIN, however, remains consistent under *EBD*, and moreover it is also efficient.

To see the consistency and efficiency of DURBIN under EBD, note that, using (3) and $u_t = y_t - x'_t \beta$, we can write (1) as

$$y_{t} = x_{t}^{\prime}\beta + u_{t}$$

$$= x_{t}^{\prime}\beta + \sum_{j=1}^{\infty} \psi_{u,j}u_{t-j} + \sum_{j=1}^{\infty} \Psi_{xu,j}x_{t-j} + \varepsilon_{u,t}$$

$$= x_{t}^{\prime}\beta + \sum_{j=1}^{\infty} \psi_{u,j} \left(y_{t-j} - x_{t-j}^{\prime}\beta\right) + \sum_{j=1}^{\infty} \Psi_{xu,j}x_{t-j} + \varepsilon_{u,t}$$

$$= x_{t}^{\prime}\beta + \sum_{j=1}^{\infty} \psi_{u,j}y_{t-j} + \sum_{j=1}^{\infty} x_{t-j}^{\prime} \left(\Psi_{xu,j}^{\prime} - \psi_{u,j}\beta\right) + \varepsilon_{u,t}.$$

$$(7)$$

Noting that the relationship $\gamma_j = \Psi_{xu,j} - \psi_{u,j}\beta$ gives a one-to-one mapping between γ_j and $\Psi_{xu,j}$, given values for $\psi_{u,j}$ and β , we immediately obtain efficiency for DURBIN.⁸

Finally, we impose no restrictions at all, in which case all methods become inconsistent and the use of instrumentation appears to be the only way forward.

⁷Weak exogeneity is sometimes called predeterminedness. See Mikusheva and Sølvsten (2023).

⁸Of course, if $\Psi_{xu,j} = 0$, then DURBIN, which estimates γ_j , is over-parameterized, providing a simple argument showing that DURBIN is inefficient under *GEXOG*.

In summary, OLS requires stronger conditions for consistency than the FGLS variants. The FGLS variants, in turn, require stronger conditions for consistency than DURBIN. Hence, overall, DURBIN has attractive consistency features in comparison with OLS and the FGLS variants. On the other hand, when the FGLS variants are consistent, they are also fully efficient. We shall see how such trade-offs resolve themselves in the simulations of section 4 below.

3 A Generalized Data-Generating Process

We now move from the basic DGP (1) to a generalized version that subsumes all cases of interest.

3.1 Data-Generating Process

Henceforth we work with the data-generating process given by

$$y_t = \sum_{j=1}^p \phi_j y_{t-j} + \sum_{i=1}^k \beta_i x_{i,t} + \sum_{j=1}^p \sum_{i=1}^k \gamma_{i,j} x_{i,t-j} + u_t.$$
(8)

We emphasize that u_t may also be a dynamic process, to allow, for example, for missing covariates. In particular, we continue to allow $(x'_t, u_t)'$ to follow the the vector moving average (2), or equivalently, the vector autoregression (3). This generalized DGP covers most linear dynamic relationships of conceivable interest. We use NDY ("no dynamics in y") to refer to the restriction imposed on the generalized DGP (8) to get the basic DGP (1), namely $\phi_j = \gamma_{i,j} = 0 \quad \forall i, j$.

We also emphasize that (8) is now the data generating process, and various regressions could be fit to its data realizations in various attempts at estimation and inference for β . One such regression, for example, is FGLS. Clearly the use of FGLS in environments characterized by the generalized DGP (8) accounts only for $x'_t\beta$ and therefore ignores all terms involving lags, resulting in misspecification of the conditional mean part of the fitted regression. That is, the only way lagged information is used in FGLS is through estimation of the error covariance matrix, which neglects the problem of misspecification of the conditional mean.

DURBIN is another such regression that can be fit to the generalized DGP (8). Indeed DURBIN can perfectly accommodate the generalized DGP, because, in precise parallel to (7), we have

$$\begin{aligned} y_{t} &= x_{t}'\beta + \sum_{j=1}^{\infty} \lambda_{j} y_{t-j} + \sum_{j=1}^{\infty} x_{t-j}' \theta_{j} + u_{t} \\ &= x_{t}'\beta + \sum_{j=1}^{\infty} \lambda_{j} y_{t-j} + \sum_{j=1}^{\infty} x_{t-j}' \theta_{j} + \sum_{j=1}^{\infty} \psi_{u,j} u_{t-j} + \sum_{j=1}^{\infty} x_{t-j}' \psi_{xu,j} + \varepsilon_{u,t} \\ &= x_{t}'\beta + \sum_{j=1}^{\infty} \lambda_{j} y_{t-j} + \sum_{j=1}^{\infty} x_{t-j}' \theta_{j} \\ &+ \sum_{j=1}^{\infty} \psi_{u,j} \left(y_{t-j} - x_{t-j}'\beta - \sum_{s=1}^{\infty} \lambda_{s} y_{t-j-s} - \sum_{s=1}^{\infty} x_{t-j-s}' \theta_{s} \right) + \sum_{j=1}^{\infty} x_{t-j}' \Psi_{xu,j} + \varepsilon_{u,t} \\ &= x_{t}'\beta + \sum_{j=0}^{\infty} \left(\lambda_{j} + \psi_{u,j} - \sum_{s=1}^{j-1} \psi_{u,s} \lambda_{j-s} \right) y_{t-j} + \sum_{j=1}^{\infty} x_{t-j}' \left(\Psi_{xu,j} - \psi_{u,j} \beta - \sum_{s=1}^{j-1} \psi_{u,s} \theta_{j-s} \right) + \varepsilon_{u,t}, \end{aligned}$$

which is a DURBIN regression with

$$\phi_j = \lambda_j + \psi_{u,j} - \sum_{s=1}^{j-1} \psi_{u,s} \lambda_{j-s}$$
$$\gamma_j = \psi_{xu,j} - \psi_{u,j} \beta - \sum_{s=1}^{j-1} \psi_{u,s} \theta_{j-s}$$

The above relationships between the parameters of the generalized DGP (8) and the DURBIN regression (6) also show that the generalized DGP is so richly parameterized that not all parameters are identified through estimation of (6) alone. β is always identified and consistently estimable via DURBIN, however, even in cases where OLS, FGLS, and FGLS-D are inconsistent.

3.2 Estimator Comparisons

In Table 1 we summarize the consistency and efficiency properties of all estimators in the leading environments that we have considered, all of which are specializations of the generalized DGP given by (8) and (3). Table 1 makes clear the important trade-off between the occasional efficiency of FGLS/FGLS-D and the robust consistency of DURBIN. That is, although FGLS is sometimes efficient when DURBIN is not (under NDY + BD and NDY + GEXOG), DURBIN is always at least consistent, and FGLS is not.

Restriction	Estimator					
	OLS	DURBIN	FGLS	FGLS-D		
NDY + BD	$\checkmark \times$	$\checkmark \times$	$\checkmark\checkmark$	$\checkmark\checkmark$		
NDY + GEXOG	\times \times	$\checkmark \times$	\times \times	$\checkmark\checkmark$		
NDY + EBD	\times \times	$\checkmark\checkmark$	\times \times	\times \times		
EBD	\times \times	$\checkmark\checkmark$	\times \times	\times \times		
None	\times \times	\times \times	\times \times	\times \times		

Table 1: Estimator Consistency and Efficiency Under Various Conditions

Notes: We show the consistency and efficiency properties of various estimators under various restrictions on the generalized DGP (8) with $(x_t, u_t)'$ governed by (3). In each cell of the table, the first checkmark, or lack thereof, relates to consistency and the second to efficiency.

Indeed the EBD row of Table 1 is starkly revealing, as for example it includes simple and natural DGPs like

$$y_t = x_t\beta + \phi y_{t-1} + x_{t-1}\gamma + u_t$$

The conventional FGLS procedure would be to regress y_t on x_t , and then to regress the residuals on lagged residuals, thereby obtaining the Cochrane-Orcutt filter to apply to the y_t and x_t series. One strongly suspects, and our subsequent simulations in section 4 show clearly, that FGLS will perform poorly in this environment unless $\gamma \approx \beta \phi$, in which case the DGP reduces (approximately) to just a static regression of y_t on x_t with AR(1) disturbances.⁹

3.3 Hausman Tests

Table 1 also highlights the potential usefulness of tests for validity of the various restrictions. If for example, one "knew" that NDY+GEXOG held, then FGLS or FGLS-D would be fully appealing estimators (consistent and efficient) whereas DURBIN would be less appealing (consistent but not efficient). Alternatively, if one knew that instead NDY + EBD held, then FGLS or FGLS-D would be highly *un*appealing (inconsistent) whereas DURBIN would be fully appealing (consistent and efficient).

Hausman tests are available, as follows. Clearly, restrictions on the parameters of (3) determine the comparative desirability of alternative methods of estimation and inference for β . The key restriction is *BD*. Under the null hypothesis that *BD* holds with *u* serially correlated, OLS is consistent but not efficient, while FGLS is both consistent and efficient. Under the alternative hypothesis that *BD* fails, OLS and FGLS are generally both inconsis-

⁹The restriction $\gamma \approx \beta \phi$ is known as the common factor restriction.

tent but have different limits, which depend on the parameters of (3). As a result, Hausman tests can be used.

In particular, one may wish to query whether $\beta_1 = \beta_2$, where

$$E(y_t|x_t) = x_t'\beta_1$$

and

$$E(y_t|x_t, x_{t-1}, y_{t-1}, x_{t-2}, y_{t-2}, \dots) = x_t'\beta_2 + \sum_{j=1}^{\infty} \phi_j y_{t-j} + \sum_{j=1}^{\infty} x_{t-j}' \gamma_j.$$

Under the null hypothesis, FGLS should be used. Otherwise one should consider using FGLS-D or DURBIN if one is interested in β_2 as would typically be the case, or consider using OLS if for some reason β_1 is of interest.

Overall, however, we find it preferable simply to use DURBIN under all circumstances, unless there is some compelling reason to do otherwise. There are three reasons:

- 1. An acceptable HAC estimator of the variance of the OLS estimator may not be available when implementing a Hausman test. Indeed the poor performance of OLS-HAC is the theme of this paper.
- 2. As regards consistent/efficient estimation, it will be clear from the simulation results in section 4 below that the MSE cost of using DURBIN when a more efficient estimator is available (i.e., when BD or at least GEXOG holds) is generally small, whereas the MSE cost of not using DURBIN can be very large when neither BD nor GEXOG holds.
- 3. As regards consistent inference, it will also be clear from the simulation results in section 4 below that DURBIN-based inference performs well in all circumstances that we investigate, both in terms of test size and power, in contrast to all other methods that we consider, where inference often fails.

We will shortly turn to the extensive simulation results alluded to in points 2 and 3 above, but first we briefly consider DURBIN vs other estimation approaches in the important context of predictive inference.

3.4 Predictive Inference

As is clear from Table 1, OLS is rarely consistent in time-series situations of interest. One case where OLS *is* consistent and simultaneously FGLS is inconsistent involves multi-step

forecast evaluation, where one tests whether a forecast x_t is unbiased for y_{t+k} . That is, one tests whether

$$E(y_{t+k}|x_t) = x_t,$$

for $k \geq 1$.

One of the earliest analyses of this problem was by Hansen and Hodrick (1980), where y_{t+k} represented the k-period-ahead spot exchange rate and x_t represented the current k-period forward rate. The null hypothesis of $\beta = 1$ implies moving-average disturbances, producing a violation of strong exogeneity while nevertheless satisfying weak exogeneity. Hansen and Hodrick (1980) recognized that FGLS can be inconsistent in such a situation, whereas OLS remains consistent, albeit inefficient. They recognized, moreover, that the OLS standard error was inconsistent and therefore required a "correction" – and OLS-HAC was born.

Note however, that DURBIN is also perfectly applicable in the Hansen-Hodrick environment, delivering not only consistent standard errors, but also efficient as opposed to merely consistent parameter estimates.¹⁰ In particular, under the null of unbiasedness, the error term,

$$u_{t+k} = y_{t+k} - x_t,$$

satisfies $Cov(u_{t+j}u_t) = 0$ for j > k, which implies that u_{t+k} can be represented by an MA(k-1) process. Hence we can write

$$y_{t+k} = x_t \beta + \theta(L)\varepsilon_t,\tag{9}$$

where ε_t is a white noise process and $\theta(L)$ is a polynomial in the lag operator of order k-1.

Conceptually, equation (9) is merely a restricted DURBIN model, because on using the filter $\theta(L)^{-1}$ we obtain

$$\left\{\theta(L)^{-1}y_{t+k}\right\} = \beta \left\{\theta(L)^{-1}x_t\right\} + \varepsilon_{t+k}.$$
(10)

The filtered explanatory variable is uncorrelated with current and future innovations, ε_{t+k} , so that estimation of equation (10) by OLS will produce consistent and asymptotically efficient estimates of the regression parameters. In practice it is convenient to use the approximation $\theta(L)^{-1} \approx \pi(L)$, where $\pi(L) = (1 - \pi_1 L - ... - \pi_p L^p)$ is a *p*th-order lag-operator polynomial

¹⁰For a full empirical analysis, see Baillie et al. (2023).

with all roots outside the unit circle. DURBIN will then be

$$\pi(L)y_{t+k} = \beta \pi(L)x_t + \varepsilon_{t+k},\tag{11}$$

which is a restricted version of the generalized DGP (8) and can also be estimated by restricted OLS.

4 Simulation Evidence on Estimation and Testing

In this section we examine, via simulation, the sampling properties of the various estimators, the properties of forecasts that use those estimated parameters, and crucially, the size and power of associated hypothesis tests.

4.1 Simulation Design

The main simulation results will comprise four data generation processes that impose different assumptions on the generalized DGP given by (8) and (3):

1. Autoregressive Disturbances, AR(1) (NDY + BD)

$$y_{t} = \beta x_{t} + u_{t}$$

$$\begin{pmatrix} x_{t} \\ u_{t} \end{pmatrix} = \begin{pmatrix} 0.7 & 0 \\ 0 & \rho \end{pmatrix} \begin{pmatrix} x_{t-1} \\ u_{t-1} \end{pmatrix} + \begin{pmatrix} \varepsilon_{x,t} \\ \varepsilon_{u,t} \end{pmatrix}$$
(12)

2. Triangular vector autoregression (VAR) on (3) (NDY + GEXOG)

$$y_{t} = \beta x_{t} + u_{t}$$

$$\begin{pmatrix} x_{t} \\ u_{t} \end{pmatrix} = \begin{pmatrix} \psi_{11} & \psi_{12} \\ 0 & \psi_{22} \end{pmatrix} \begin{pmatrix} x_{t-1} \\ u_{t-1} \end{pmatrix} + \begin{pmatrix} \varepsilon_{x,t} \\ \varepsilon_{u,t} \end{pmatrix}$$
(13)

3. Unrestricted VAR on (3) (NDY + EBD)

$$y_{t} = \beta x_{t} + u_{t}$$

$$\begin{pmatrix} x_{t} \\ u_{t} \end{pmatrix} = \begin{pmatrix} \psi_{11} & \psi_{12} \\ \psi_{21} & \psi_{22} \end{pmatrix} \begin{pmatrix} x_{t-1} \\ u_{t-1} \end{pmatrix} + \begin{pmatrix} \varepsilon_{x,t} \\ \varepsilon_{u,t} \end{pmatrix}$$
(14)

4. Dynamic Regression (EBD)

$$y_t = \beta x_t + \rho y_{t-1} - 0.5 x_{t-1} + u_t$$
$$\begin{pmatrix} x_t \\ u_t \end{pmatrix} = \begin{pmatrix} 0.7 & 0 \\ 0 & 0 \end{pmatrix} \begin{pmatrix} x_{t-1} \\ u_{t-1} \end{pmatrix} + \begin{pmatrix} \varepsilon_{x,t} \\ \varepsilon_{u,t} \end{pmatrix}.$$
(15)

In all cases, $(\varepsilon_{x,t}, \varepsilon_{u,t})' \sim iidN(0, I)$ with t = 1, ..., T. We explore $T \in \{50, 200, 600, 2500\}$, which also spans the relevant range for macroeconomics, where structural change and other considerations tend to keep sample spans to roughly "the most recent fifty years"; that is, sample sizes of 50 years, 200 quarters, 600 months, or approximately 2500 weeks. Including T = 2500 also lets us check our Monte Carlo results against known large-sample results.

The autoregressive DGP in (12) matches the design in Lazarus et al. (2018). We explore $\rho \in \{0, .3, .5, .7, .9, .95, .99\}$, which spans the relevant range for economics. All ρ values are positive, as economic time series are generally positively serially correlated, and they range from white noise to the very strong serial correlation often of relevance in macroeconomic series. Including the white noise case ($\rho = 0$) allows us to check our Monte Carlo results against known results for the iid case.

In the simulations for the triangular VAR DGP in (13), we consider the following values for the matrix Ψ :

$$\Psi_1 = \begin{pmatrix} 0.4 & 0.7 \\ 0 & 0.5 \end{pmatrix} \qquad \Psi_1^* = \begin{pmatrix} 0.4 & 0.7 \\ 0 & 0.6 \end{pmatrix}$$

 Ψ_1^* has a larger leading eigenvalue than Ψ_1 (0.6 versus 0.5) and hence exhibits stronger autoregressive features.

For the unrestricted VAR DGP in (14), we consider the following values:

$$\Psi_2 = \begin{pmatrix} 0.4 & 0.7 \\ 0.3 & 0.5 \end{pmatrix} \qquad \Psi_2^* = \begin{pmatrix} 0.4 & 0.7 \\ 0.3 & 0.6 \end{pmatrix}$$

As before, Ψ_2^* was selected to be similar to Ψ_2 but with a larger leading eigenvalue (0.97 for Ψ_2^* and 0.91 for Ψ_2).

For the dynamic regression DGP in (15), we consider various parameter values for the the coefficient on y_{t-1} , namely $\rho \in \{0, 0.5, 0.7, 0.95\}$. When $\rho = 0.5$, the common factor restriction introduced in footnote 9 holds, in which case we expect FGLS and FGLS-D to perform well.

For all DGPs in our simulations we perform 10,000 Monte Carlo replications. We simulate

exact realizations of x and u by drawing x_0 and u_0 from their stationary distribution at each Monte Carlo replication, and we use common random numbers whenever appropriate.

4.2 **Operational Considerations**

Next, we detail operational matters relating to our implementation of the various estimators we use in our simulations.

4.2.1 OLS-HAC

OLS-HAC estimation proceeds from the approach previously outlined in section 2.2; namely

$$T^{1/2}(\hat{\beta}_{OLS} - \beta) \to N(0, V),$$

where $V = Q^{-1}\Omega Q^{-1}$ and

$$\Omega = \sum_{\tau = -\infty}^{\infty} \Gamma(\tau)$$

where $\Gamma(\tau) = cov(x_t u_t, x_{t-\tau} u_{t-\tau})$, and $\tau = 0, \pm 1, \dots$

The key object in V is Ω , the spectrum of xu at frequency zero. The OLS-HAC approach uses

$$\widehat{V} = Q^{-1}\widehat{\Omega}Q^{-1}$$

where $\widehat{\Omega}$ is a consistent estimator of Ω and hence \widehat{V} delivers a consistent estimator of V.

A large literature on consistent estimation of Ω can be traced back to at least Hansen and Hodrick (1980). The most popular approach is due to Newey and West (1987), who propose lag-window estimation with linearly-decreasing (Bartlett) lag window:

$$\widehat{\Omega} = \left(\frac{1}{T}\sum_{t=1}^{T} (x_t x_t') \hat{u}_t^2 + \sum_{\tau=1}^{h} \left(1 - \frac{\tau}{h+1}\right) (\widehat{\Gamma}_{\tau} + \widehat{\Gamma}_{-\tau})\right),\tag{16}$$

where

$$\widehat{\Gamma}_{\tau} = \frac{1}{T} \sum_{t=1}^{T} \hat{u}_t x_t x'_{t-\tau} \hat{u}_{t-\tau},$$

the \hat{u}_t are OLS regression residuals, and T is sample size. Indeed, many leading HAC estimators are of the form (16), distinguished only by their choice of truncation lag h.

We will explore several leading truncation lag choices, including:

- 1. NW: Newey-West (16) with $h = \lceil (T/100)^{2/9} \rceil$. This h choice is a standard textbook recommendation (e.g., Wooldridge (2015)).
- 2. NW-A: Newey-West (16) with $h = \lceil 0.75T^{1/3} \rceil$. This h choice is also standard, arising when a formula in Andrews (1991) is specialized to the case of a first-order autoregression with coefficient 0.25.
- 3. NW-LLSW: Newey-West (16) with $h = \lceil 1.3T^{1/2} \rceil$, as proposed by Lazarus et al. (2018). Its use of $T^{1/2}$ rather than $T^{2/9}$ or $T^{1/3}$ as in NW or NW-A, respectively, produces higher truncation lags. For example, if T = 200, then NW selects h = 5 but NW-LLSW selects h = 19.
- 4. NW-KV: Newey-West (16) with h = T, as proposed by Kiefer and Vogelsang (2002), which builds on Kiefer et al. (2000). Setting h = T is of course the maximum possible truncation lag.

We will also explore the Müller (2014) HAC estimator (we denote it by M), which is not in the Newey-West family. Instead, it is an orthogonal series estimator, that uses a type-II discrete cosine transform to produce an equally-weighted average of projections on cosines. The M estimator is:

$$\widehat{\Omega} = \frac{1}{\nu} \sum_{j=1}^{\nu} \widehat{\Lambda}_j \widehat{\Lambda}'_j,$$

where

$$\widehat{\Lambda}_j = \sqrt{\frac{2}{T}} \sum_{t=1}^T (x_t \widehat{u}_t) \cos\left(\pi j \left(\frac{t-1/2}{T}\right)\right)$$

The M truncation parameter, ν , is the total number of cosines included in the average projection. Lazarus et al. (2018) suggest setting $\nu = \lfloor 0.4T^{2/3} \rfloor$, producing the M-LLSW estimator.

4.2.2 FGLS and FGLS-D

If the data follow the DGP in (1), namely $y_t = x_t\beta + u_t$, and there exists a known lag operator polynomial (filter) $\Phi(L)$ that reduces u_t to white noise ε_t (i.e., $\Phi(L)u_t = \varepsilon_t$), then GLS estimation of β is appropriate, and it amounts to running an OLS regression on transformed data. Specifically, one regresses \tilde{y}_t on \tilde{x}_t , where $\tilde{y}_t = \Phi(L)y_t$ and $\tilde{x}_t = \Phi(L)x_t$.

In practice, however, $\Phi(L)$ is unknown and needs to be approximated. The FGLS estimator uses $\phi(L) = 1 - \phi_1 L - \phi_2 L^2 - \dots - \phi_p L^p$ and proceeds as follows:

- 1. Run an OLS regression of y_t on x_t , and obtain the residuals \hat{u}_t .
- 2. Fit an AR(p) model to \hat{u}_t (in particular, run an OLS regression of \hat{u}_t on $\hat{u}_{t-1}, ..., \hat{u}_{t-p}$, with p selected by AIC or BIC), and obtain the coefficients $\hat{\phi}_1, ..., \hat{\phi}_p$.
- 3. Construct the transformed data,

$$\tilde{x}_{t} = x_{t} - \hat{\phi}_{1} x_{t-1} - \dots - \hat{\phi}_{p} x_{t-p}$$
$$\tilde{y}_{t} = y_{t} - \hat{\phi}_{1} y_{t-1} - \dots - \hat{\phi}_{p} y_{t-p}.$$

4. Run an OLS regression of \tilde{y}_t on \tilde{x}_t to obtain the FGLS estimator of β .

The FGLS-D estimator relies on a different first-stage procedure, replacing the regressions in steps 1 and 2 above with a single DURBIN regression, proceeding as follows:

1. Run the OLS DURBIN regression (with p selected by AIC or BIC),

$$y_{t} = \sum_{j=1}^{p} \varphi_{j} y_{t-j} + \sum_{i=1}^{k} \beta_{i} x_{i,t} + \sum_{j=1}^{p} \sum_{i=1}^{k} \gamma_{i,j} x_{i,t-j} + \varepsilon_{t}$$

2. Use the estimated coefficients on the lags of y_t , $\hat{\varphi}_1, ..., \hat{\varphi}_p$, to construct the transformed data,

$$\tilde{x}_t = x_t - \hat{\varphi}_1 x_{t-1} - \dots - \hat{\varphi}_p x_{t-p}$$
$$\tilde{y}_t = y_t - \hat{\varphi}_1 y_{t-1} - \dots - \hat{\varphi}_p y_{t-p}.$$

3. Run the OLS regression of \tilde{y}_t on \tilde{x}_t to obtain the FGLS-D estimator of β .

4.2.3 DURBIN

As previously noted, the DURBIN regression augments regression (1) with lags of y and x to capture dynamics, very much in the spirit of an arbitrary equation in a vector autoregression, as suggested by Durbin (1970).¹¹ The p^{th} -order DURBIN regression is

$$y_{t} = \sum_{j=1}^{p} \phi_{j} y_{t-j} + \sum_{i=1}^{k} \beta_{i} x_{i,t} + \sum_{j=1}^{p} \sum_{i=1}^{k} \gamma_{i,j} x_{i,t-j} + \varepsilon_{t}, \qquad (17)$$

 $^{^{11}}$ Also related is the important recent work of Montiel Olea and Plagborg-Møller (2021), who study lagaugmented local projection estimators of impulse-response functions in vector autoregressions.

which has p + k + kp parameters.

If u_t in equation (1) is a finite-ordered AR(p) process with p known, then DURBIN holds exactly. In particular, we have¹²

$$y_{t} = \sum_{j=1}^{p} \phi_{j} y_{t-j} + \sum_{i=1}^{k} \beta_{i} x_{i,t} + \sum_{j=1}^{p} \sum_{i=1}^{k} \beta_{i} \phi_{j} x_{i,t-j} + \varepsilon_{t}$$
(18)
$$= \sum_{j=1}^{p} \phi_{j} y_{t-j} + \sum_{i=1}^{k} \beta_{i} x_{i,t} + \sum_{j=1}^{p} \sum_{i=1}^{k} \gamma_{i,j} x_{i,t-j} + \varepsilon_{t}.$$

Hence the usual asymptotic inference is immediately available:

$$T^{1/2}(\widehat{\vartheta}_{OLS} - \vartheta) \to N(0, Q^{-1}),$$
 (19)

where ϑ_{OLS} is the vector of DURBIN parameters,

$$Q = plim\left(T^{-1}\sum_{t=1}^{T} z_t z_t'\right),\tag{20}$$

and $z'_t = (y_{t-1}, ..., y_{t-p}, x_{1,t}, ..., x_{k,t}, x_{1,t-1}, ..., x_{k,t-1}, ..., x_{1,t-p}, ..., x_{k,t-p}).$

In the more compelling case where p is unknown and must be selected (implemented in our Monte Carlo below), the DURBIN regression (17) is approximate rather than exact. However, the limiting distribution (19) remains valid if p is selected suitably (Grenander, 1981; Hannan and Deistler, 1988), as achieved by standard criteria with well-known optimality properties.¹³ In particular, if a p_{max} is known such that $p \leq p_{max}$, then a consistent selection criterion (in the model selection sense) like BIC is a natural choice. Alternatively, in the absence of a p_{max} , an efficient selection criterion (in the model selection sense) like AIC is a natural choice.¹⁴

¹²Note that DURBIN does *not* impose the common factor restriction embedded in (18), namely that $\gamma_{i,j} = \beta_i \phi_j \,\forall i, j$, in which case DURBIN coincides with FGLS. See Sargan (1964) and Hendry and Mizon (1978).

¹³OLS-HAC regression, in contrast, typically relies on one or another of various "rules of thumb" for bandwidth (truncation, h or ν) selection. "Automatic" bandwidth selection has, however, been considered in Andrews-Newey-West environments by Andrews (1991), Andrews and Monahan (1992), and Newey and West (1994), among others.

¹⁴In the Gaussian case, we have BIC = $T \log(SSE) + \log(T)(p+k+kp)$ and AIC = $T \log(SSE) + 2(p+k+kp)$, where SSE is the DURBIN regression sum of squared errors.

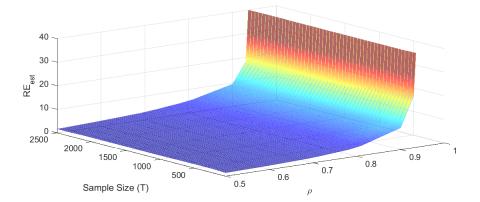


Figure 1: Efficiency of DURBIN Relative to OLS DGP: Autoregressive Disturbances, NDY + BD

Notes: All shocks are N(0,1) white noise. We select DURBIN lag order using BIC. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. We do not plot values for $\rho = 0.99$, due to their extreme magnitude as shown in Table 2. See text for details.

4.3 Estimation Accuracy

We first examine the accuracy of our four estimators (OLS, FGLS, FGLS-D, and DURBIN) under our four DGPs (NDY+BD, NDY+GEXOG, NDY+EBD, BD). The key object of interest is RE_{est}, the efficiency of DURBIN relative to OLS, FGLS or FGLS-D. For example:

$$RE_{est}(OLS) = \frac{MSE(OLS)}{MSE(DURBIN)}.$$

We also show MSE and bias.¹⁵

Autoregressive Disturbances DGP (NDY + BD). Results appear in Table 2. Let us begin directly with the RE_{est} results for DURBIN relative to OLS. For any fixed sample size T, RE_{est} is increasing in serial correlation strength ρ . Consider, for example, a leading case like T = 200 corresponding, to fifty years of quarterly data. For $\rho = 0$, RE_{est} is close to 1, as it should be since there is no serial correlation. RE_{est} grows quickly as ρ increases, however, reaching 2.9 when $\rho = 0.7$ and 36.3 when $\rho = 0.95$.

In contrast, for any fixed serial correlation strength ρ , RE_{est} stabilizes quickly in sample size T and remains approximately constant. Consider, for example, a realistic case like $\rho =$

¹⁵Note that all OLS-HAC estimators simply use the OLS estimator of β . Particular HAC estimators will have particular effects on the *standard errors* of $\hat{\beta}$, but not on $\hat{\beta}$ itself, which always remains just $\hat{\beta}_{OLS}$.

Table 2: Bias, MSE, and Relative Efficiency Estimators: OLS, FGLS, FGLS-D, DURBIN DGP: Autoregressive Disturbances, NDY + BD

				T=50				
		$\rho = 0$	$\rho = 0.3$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$	$\rho = 0.99$
	OLS	0.0006	-0.0021	-0.0008	0.0025	0.0093	0.0098	-0.0270
D:	FGLS	0.0006	-0.0015	-0.0002	0.0000	0.0030	-0.0002	-0.0068
Bias	FGLS-D	0.0007	-0.0016	-0.0002	0.0006	0.0021	-0.0002	0.0014
	DURBIN	0.0006	-0.0010	0.0006	0.0001	0.0034	-0.0006	0.0006
	OLS	0.0112	0.0180	0.0289	0.0599	0.3013	1.3368	80.0070
MOR	FGLS	0.0121	0.0174	0.0216	0.0237	0.0251	0.0304	0.2953
MSE	FGLS-D	0.0114	0.0179	0.0222	0.0231	0.0207	0.0198	0.0183
	DURBIN	0.0131	0.0201	0.0237	0.0229	0.0226	0.0234	0.0227
	OLS	0.8597	0.8952	1.2189	2.6140	13.3211	57.1114	3530.5932
RE_{est}	FGLS	0.9261	0.8666	0.9116	1.0356	1.1115	1.2986	13.0298
	FGLS-D	0.8685	0.8869	0.9370	1.0063	0.9142	0.8476	0.8092
				T=200)			
		$\rho = 0$	$\rho = 0.3$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$	$\rho = 0.99$
	OLS	-0.0003	-0.0006	-0.0007	-0.0012	0.0029	-0.0082	-0.0441
D:	FGLS	-0.0003	-0.0008	-0.0004	-0.0009	-0.0005	-0.0008	0.0001
Bias	FGLS-D	-0.0003	-0.0008	-0.0004	-0.0008	-0.0005	-0.0005	0.0000
	DURBIN	-0.0002	-0.0009	-0.0003	-0.0009	-0.0002	-0.0004	-0.0003
	OLS	0.0026	0.0043	0.0072	0.0147	0.0635	0.1884	8.9415
	FGLS	0.0027	0.0039	0.0048	0.0051	0.0048	0.0046	0.0048
MSE	FGLS-D	0.0026	0.0040	0.0048	0.0051	0.0048	0.0045	0.0044
	DURBIN	0.0027	0.0051	0.0052	0.0051	0.0052	0.0052	0.0051
	OLS	0.9611	0.8526	1.3750	2.8763	12.3138	36.3636	1753.3931
RE_{est}	FGLS	0.9761	0.0020 0.7730	0.9319	1.0083	0.9296	0.8909	0.9385
rubest	FGLS-D	0.9614	0.7801	0.9306	1.0003 1.0024	0.9230 0.9221	0.8767	0.9563 0.8567
				_	_			
		a = 0	a = 0.3	T = 600		a = 0.9	a = 0.95	a = 0.90
		$\rho = 0$	$\rho = 0.3$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$	/
	OLS	0.0001	0.0001	$\rho = 0.5$ -0.0008	$ \rho = 0.7 $ 0.0009	0.0005	0.0007	0.0119
Bias	FGLS	$0.0001 \\ 0.0001$	$0.0001 \\ 0.0000$	$ \rho = 0.5 $ -0.0008 -0.0006	$ \rho = 0.7 $ 0.0009 0.0001	$0.0005 \\ 0.0002$	0.0007 0.0002	0.0119
Bias	FGLS FGLS-D	$\begin{array}{c} 0.0001 \\ 0.0001 \\ 0.0001 \end{array}$	$\begin{array}{c} 0.0001 \\ 0.0000 \\ 0.0000 \end{array}$	$\rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0006$	$\rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001$	$\begin{array}{c} 0.0005 \\ 0.0002 \\ 0.0002 \end{array}$	0.0007 0.0002 0.0002	0.0119 -0.0006 -0.0006
Bias	FGLS FGLS-D DURBIN	$\begin{array}{c} 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \end{array}$	0.0001 0.0000 0.0000 0.0001	$\rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0006 \\ -0.0005$	$\rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001$	0.0005 0.0002 0.0002 0.0003	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\end{array}$	0.0119 -0.0006 -0.0006 -0.0006
Bias	FGLS FGLS-D DURBIN OLS	0.0001 0.0001 0.0001 0.0001 0.0009	0.0001 0.0000 0.0000 0.0001 0.0015	$\rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0006 \\ -0.0005 \\ 0.0024$	$\begin{aligned} \rho &= 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \end{aligned}$	0.0005 0.0002 0.0002 0.0003 0.0203	0.0007 0.0002 0.0002 0.0004 0.00493	0.0119 -0.0006 -0.0006 -0.0006 1.1932
	FGLS FGLS-D DURBIN OLS FGLS	$\begin{array}{c} 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0009 \\ 0.0009 \end{array}$	$\begin{array}{c} 0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ 0.0015 \\ 0.0013 \end{array}$	$\begin{array}{l} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \end{array}$	$\begin{aligned} \rho &= 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \\ 0.0017 \end{aligned}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015 \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0493\\ 0.0015 \end{array}$	0.0119 -0.0006 -0.0006 -0.0006 1.1932 0.0015
Bias	FGLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0009 \\ 0.0009 \\ 0.0009 \\ 0.0009 \end{array}$	$\begin{array}{c} 0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ \hline 0.0015 \\ 0.0013 \\ 0.0013 \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \\ 0.0017 \\ 0.0017 \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ \hline \end{array}$	0.0119 -0.0006 -0.0006 1.1932 0.0015 0.0014
	FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0009 \\ 0.0009 \\ 0.0009 \\ 0.0009 \\ 0.0009 \\ 0.0009 \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ \hline 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \\ 0.0017 \\ 0.0017 \\ 0.0017 \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ \end{array}$	0.0119 -0.0006 -0.0006 1.1932 0.0015 0.0014 0.0017
MSE	FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS	0.0001 0.0001 0.0001 0.0009 0.0009 0.0009 0.0009 0.0009 0.9900	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551 \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 2.8902 \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793 \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 29.5992 \end{array}$	0.0119 -0.0006 -0.0006 -0.0006 1.1932 0.0015 0.0014 0.0017 705.7406
	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS	0.0001 0.0001 0.0001 0.0009 0.0009 0.0009 0.0009 0.0009 0.9900 0.9959	$\begin{array}{c} 0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ \hline 0.0015 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ \hline 0.8551 \\ 0.7625 \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 2.8902 \\ 1.0027 \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 29.5992\\ 0.8918\\ \end{array}$	0.0119 -0.0006 -0.0006 -0.0006 1.1932 0.0015 0.0014 0.0017 705.7406 0.8731
MSE	FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS	0.0001 0.0001 0.0001 0.0009 0.0009 0.0009 0.0009 0.0009 0.9900	0.0001 0.0000 0.0000 0.0001 0.0015 0.0013 0.0013 0.0017 0.8551	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 2.8902 \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793 \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 29.5992 \end{array}$	$\begin{array}{c} \rho = 0.99\\ 0.0119\\ -0.0006\\ -0.0006\\ 1.1932\\ 0.0015\\ 0.0014\\ 0.0017\\ 705.7406\\ 0.8731\\ 0.8464\end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 2.8902 \\ 1.0027 \\ 1.0026 \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 29.5992\\ 0.8918\\ 0.8912\\ \end{array}$	0.0119 -0.0006 -0.0006 1.1932 0.0015 0.0014 0.0017 705.7406 0.8731 0.8464
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS FGLS-D	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9959\\ 0.9959\\ 0.9899\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7622\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \hline \mathbf{T=250} \\ \rho = 0.5 \end{array}$	$\begin{tabular}{ c c c c c }\hline $\rho = 0.7$\\\hline 0.0009\\\hline 0.0001\\\hline 0.0001\\\hline 0.0001\\\hline 0.00017\\\hline 0.0017\\\hline 0.0017\\\hline 0.0017\\\hline 2.8902\\\hline 1.0027\\\hline 1.0026\\\hline 0\\\hline $\rho = 0.7$\\\hline \end{tabular}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ 29.5992\\ 0.8918\\ 0.8912\\ \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 1.1932\\ 0.0015\\ 0.0014\\ 0.0017\\ \hline 705.7406\\ 0.8731\\ 0.8464\\ \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \rho=0\\ 0.0000\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \mathbf{T=250} \\ \rho = 0.5 \\ -0.0001 \end{array}$	$\begin{array}{c} \rho = 0.7 \\ \hline 0.0009 \\ 0.0001 \\ 0.0001 \\ \hline 0.0001 \\ 0.0001 \\ \hline 0.00017 \\ 0.0017 \\ \hline 0.0017 \\ \hline 2.8902 \\ 1.0027 \\ 1.0026 \\ \hline 0 \\ \hline \rho = 0.7 \\ \hline 0.0001 \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ 29.5992\\ 0.8918\\ 0.8912\\ \end{array}$ $\rho=0.95\\ 0.0008 \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 1.1932\\ 0.0015\\ 0.0014\\ 0.0017\\ 705.7406\\ 0.8731\\ 0.8464\\ \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D CLS FGLS	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \rho=0\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \textbf{T=250} \\ \rho = 0.5 \\ -0.0001 \\ 0.0000 \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 1.0027 \\ 1.0026 \\ \hline 0 \\ \hline \rho = 0.7 \\ 0.0001 \\ 0.0001 \\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ 29.5992\\ 0.8918\\ 0.8912\\ \hline \rho = 0.95\\ 0.0008\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 1.1932\\ 0.0015\\ 0.0014\\ 0.0017\\ \hline 705.7406\\ 0.8731\\ 0.8464\\ \hline \\ \rho = 0.99\\ -0.0016\\ -0.0001\\ -0.0001\\ \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D OLS FGLS FGLS FGLS	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \rho=0\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \hline\end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \textbf{T=250} \\ \rho = 0.5 \\ -0.0001 \\ 0.0000 \\ 0.0000 \\ \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 1.0027 \\ 1.0026 \\ \hline \\ \textbf{0} \\ \hline \\ \rho = 0.7 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ \hline \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ 0.0002\\ 0.0002\\ \hline\end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ 29.5992\\ 0.8918\\ 0.8912\\ \hline \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 1.1932\\ 0.0015\\ 0.0014\\ 0.0017\\ \hline 705.7406\\ 0.8731\\ 0.8464\\ \hline \\ \hline \\ \rho = 0.99\\ -0.0016\\ -0.0001\\ -0.0001\\ -0.0001\\ \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D CLS FGLS	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \rho=0\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \textbf{T=250} \\ \rho = 0.5 \\ -0.0001 \\ 0.0000 \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0048 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 1.0027 \\ 1.0026 \\ \hline 0 \\ \hline \rho = 0.7 \\ 0.0001 \\ 0.0001 \\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ 29.5992\\ 0.8918\\ 0.8912\\ \hline \rho = 0.95\\ 0.0008\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 1.1932\\ 0.0015\\ 0.0014\\ 0.0017\\ \hline 705.7406\\ 0.8731\\ 0.8464\\ \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D OLS FGLS FGLS FGLS	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \rho=0\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \hline\end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \textbf{T=250} \\ \rho = 0.5 \\ -0.0001 \\ 0.0000 \\ 0.0000 \\ \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 1.0027 \\ 1.0026 \\ \hline \\ \textbf{0} \\ \hline \\ \rho = 0.7 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ \hline \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ 0.0002\\ 0.0002\\ \hline\end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ 29.5992\\ 0.8918\\ 0.8912\\ \hline \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 1.1932\\ 0.0011\\ 0.0014\\ 0.0017\\ \hline 705.7406\\ 0.8731\\ 0.8464\\ \hline \\ \hline \\ \rho = 0.99\\ -0.0016\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ \hline \end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D CLS FGLS FGLS FGLS FGLS-D DURBIN	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \rho=0\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \hline\end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \textbf{T=250} \\ \textbf{P} = 0.5 \\ -0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 1.0027 \\ 1.0026 \\ \hline \\ \textbf{0} \\ \hline \\ \rho = 0.7 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ \hline \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ 0.0002\\ 0.0002\\ 0.0001\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0493\\ 0.0015\\ 0.0015\\ 0.0017\\ 29.5992\\ 0.8918\\ 0.8912\\ \hline \end{array}$ $\begin{array}{c} \rho = 0.95\\ 0.0008\\ 0.0002\\ 0.0002\\ 0.0003\\ \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 1.1932\\ 0.0014\\ 0.0017\\ \hline \\ 705.7406\\ 0.8731\\ 0.8464\\ \hline \\ \rho = 0.99\\ -0.0016\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0006\\ \hline \\ 0.1116\\ \hline \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D OLS FGLS FGLS-D DURBIN OLS	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \rho=0\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \hline \mathbf{T=250} \\ \rho = 0.5 \\ -0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ 0.0006 \\ \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 2.8902 \\ 1.0027 \\ 1.0026 \\ \hline {\bf 0} \\ \hline {\bf \rho} = 0.7 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ \hline 0.0011 \\ \hline \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ 0.0048\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ 0.0015\\ \hline 0.0017\\ 29.5992\\ 0.8918\\ 0.8912\\ \hline \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 0.0012\\ 0.0012\\ 0.0017\\ \hline 0.0017\\ \hline 705.7406\\ 0.8731\\ 0.8464\\ \hline \\ \rho = 0.99\\ -0.0010\\ -0.0001\\ -0.0001\\ 0.0000\\ \hline 0.1116\\ 0.0004\\ \hline \end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D CLS FGLS FGLS-D DURBIN OLS FGLS	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \hline\\ \rho = 0\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ 0.0002\\ 0.0002\\ \hline\end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \hline \mathbf{T=250} \\ \rho = 0.5 \\ -0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ \hline 0.0006 \\ 0.0004 \\ \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 2.8902 \\ 1.0027 \\ 1.0026 \\ \hline \\ \textbf{0} \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ \hline \\ \textbf{0} \\ \textbf{0} \\ \textbf{0} \\ \hline \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ \hline\\ 0.0048\\ 0.0004\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 29.5992\\ 0.8918\\ 0.8912\\ \hline \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 0.00012\\ 0.0012\\ 0.0017\\ \hline 0.0017\\ \hline 0.0017\\ \hline 0.0017\\ \hline 0.0017\\ \hline 0.8731\\ 0.8464\\ \hline \\ \rho = 0.99\\ -0.0010\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ \hline 0.1116\\ 0.0004\\ \hline 0.0004\\ \hline \end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D FGLS FGLS-D DURBIN OLS FGLS FGLS FGLS-D DURBIN	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \hline\\ \rho = 0\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ \hline\end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \hline\\ \rho=0.3\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0004\\ \hline\end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \hline \mathbf{T=250} \\ \rho = 0.5 \\ -0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ 0.0006 \\ 0.0004 \\ 0.0004 \\ 0.0004 \\ 0.0004 \\ \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 2.8902 \\ 1.0027 \\ 1.0026 \\ \hline \\ \hline \\ \rho = 0.7 \\ \hline \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0004 \\ 0.0004 \\ 0.0004 \\ 0.0004 \\ \hline \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ \hline\\ 0.0048\\ 0.0004\\ 0.0004\\ 0.0004\\ \hline\end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 29.5992\\ 0.8918\\ 0.8912\\ \hline \end{array}$ $\rho=0.95\\ 0.0008\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0003\\ \hline 0.0106\\ 0.0004\\ 0.0004\\ 0.0004\\ \hline 0.0004\\ \hline \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 0.0015\\ 0.0014\\ 0.0017\\ \hline 705.7406\\ 0.8731\\ 0.8464\\ \hline \\ \rho = 0.99\\ -0.0010\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ 0.1116\\ 0.0004\\ 0.0004\\ 0.0004\\ \hline \end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS FGLS	$\begin{array}{c} 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9900\\ 0.9959\\ 0.9899\\ \hline\\ \hline\\ \rho = 0\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ \hline\end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0015\\ 0.0013\\ 0.0013\\ 0.0013\\ 0.0017\\ 0.8551\\ 0.7625\\ 0.7622\\ \end{array}$	$\begin{array}{c} \rho = 0.5 \\ -0.0008 \\ -0.0006 \\ -0.0005 \\ 0.0024 \\ 0.0016 \\ 0.0016 \\ 0.0017 \\ 1.3794 \\ 0.9287 \\ 0.9278 \\ \hline \mathbf{T=250} \\ \mathbf{\rho} = 0.5 \\ -0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ \hline 0.0006 \\ 0.0004 \\ 0.0004 \\ \hline \end{array}$	$\begin{array}{c} \rho = 0.7 \\ 0.0009 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0017 \\ 0.0017 \\ 0.0017 \\ 2.8902 \\ 1.0027 \\ 1.0026 \\ \hline \\ \hline \rho = 0.7 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0001 \\ 0.0004 \\ 0.0004 \\ 0.0004 \\ \hline \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0203\\ 0.0015\\ 0.0015\\ 0.0016\\ 12.4793\\ 0.9257\\ 0.9250\\ \hline\\ \rho=0.9\\ -0.0008\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ \hline\\ 0.0048\\ 0.0004\\ 0.0004\\ \hline\end{array}$	$\begin{array}{c} 0.0007\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline 0.0493\\ 0.0015\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 29.5992\\ 0.8918\\ 0.8912\\ \hline \end{array}$	$\begin{array}{c} 0.0119\\ -0.0006\\ -0.0006\\ -0.0006\\ 0.00012\\ 0.0012\\ 0.0017\\ \hline 0.0017\\ \hline 0.0017\\ \hline 0.0017\\ \hline 0.0017\\ \hline 0.8731\\ 0.8464\\ \hline \\ \rho = 0.99\\ -0.0010\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ \hline 0.1116\\ 0.0004\\ \hline 0.0004\\ \hline \end{array}$

Notes: All shocks are N(0,1) white noise. We select FGLS, FGLS-D, and DURBIN lag orders using BIC. RE_{est} denotes the relative estimation efficiency of DURBIN. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

0.9. RE_{est} remains at approximately RE_{est} = 12 for all sample sizes $T \in \{50, 200, 600, 2500\}$. Hence RE_{est} is clearly driven by serial correlation strength and not by sample size.

In Figure 1 we provide a visual representation of the RE_{est} of DURBIN relative to OLS presented in Table 2. It reveals clearly that RE_{est} is driven entirely by the degree of serial correlation and not by sample size.

Now consider separately the MSEs for OLS and DURBIN that underlie RE_{est} . For any fixed sample size T, the MSE of OLS is strongly increasing in serial correlation strength ρ (because the OLS estimator ignores serial correlation), whereas the MSE from DURBIN is invariant to serial correlation strength (because the DURBIN estimator controls for serial correlation). That is why the RE_{est} ratio is also strongly increasing in ρ , as documented earlier. In contrast, for any fixed serial correlation strength ρ , the MSEs for *both* OLS and DURBIN decrease with sample size T (as they must, since both OLS and DURBIN are consistent), but they decrease proportionately, so that the RE_{est} ratio is invariant to T, as documented earlier.

Next, let us examine the bias and variance components that underlie the MSEs. First consider bias. Both the OLS and DURBIN estimators are theoretically unbiased for any serial correlation strength and sample size, and the Monte Carlo confirms the theory: the estimated biases are always negligible and invariant to ρ .¹⁶ Moreover, given the scale of the bias, the patterns mentioned above for MSE will correspond to patterns in variance: OLS variance increases sharply with serial correlation strength (because OLS ignores serial correlation), whereas DURBIN variance does not (because DURBIN controls for serial correlation), and both variances decrease with sample size (by consistency), but they do so proportionately. That is, the MSE patterns between OLS and DURBIN, and hence the corresponding RE_{est} patterns, are driven entirely by variance.

Triangular and Unrestricted VAR DGPs (NDY+GEXOG, NDY+EBD). Results appear in Table 3. Ψ_1 and Ψ_1^* correspond to different parameterizations of the NDY + GEXOG DGP, and Ψ_2 and Ψ_2^* correspond to different parameterizations of the NDY+EBDDGP.¹⁷ For all sample sizes, OLS and FGLS exhibit large bias and MSE, which is expected since they are indeed inconsistent under both NDY + GEXOG and NDY + EBD. As a result, the RE_{est}'s for DURBIN relative to OLS and FGLS in Table 3 are very large: DURBIN dominates both.

 $^{^{16}\}mathrm{Moreover}$ the estimated biases decrease with T, as expected, by consistency.

¹⁷Recall that Ψ_1^* has a larger leading eigenvalue than does Ψ_1 , and Ψ_2^* has a larger leading eigenvalue than Ψ_2 .

Dynamic Regression DGP (*EBD*). Results appear in Table 4. In the *EBD* case, OLS, FGLS and FGLS-D are in general inconsistent, whereas DURBIN remains consistent. This is reflected in the large biases and MSEs of the other estimators compared to DURBIN, and hence the high efficiency of DURBIN relative to OLS and FGLS.

A notable exception is when $\rho = 0.5$, in which case the common factor restriction holds, so that it is possible to write the dynamic regression as a single-regressor equation (with just x_t) and a disturbance with AR(1) serial correlation. Put differently, in this case the DGP in (15) can be rewritten in the form of (12), so that FGLS and FGLS-D are consistent and efficient and should have lower MSE than Durbin. Table 4 shows that this is the case for all sample sizes. This result highlights the role that the common factor restriction plays; if it holds, it guarantees that all dynamics enter through the disturbance term, so that FGLS and FGLS-D dominate DURBIN, but if it does not hold (and there is no reason why it should hold), DURBIN dominates.

4.4 Prediction Accuracy

One of the primary uses of regression and dynamic regression is for ex ante prediction. There is substantial previous literature related to the task of prediction. In particular, Baillie (1979) has considered the situation of predictions from the regression model with AR(p) errors and the properties of prediction from static regressions and also with optimal multi-step predictions in the sense of minimum MSE predictions. Baillie (1979) also derived results on the efficiency of these predictors with and without estimated parameters. One conclusion concerns the importance of including the full effects of dynamics from the AR(p) regression model in the predictor. In this case, the complete structural dynamic predictor generally has substantial asymptotic and small sample efficiency gains over predictors from static regressions. Similar effects and properties are found in more complicated dynamic models such as the DGP considered in section 3 of this paper.

We now consider one-step-ahead predictions relying on the OLS and DURBIN estimation strategies. The results reflect that an explicit modeling of autocorrelation can be used for improved prediction. OLS estimators neglect this and therefore produce suboptimal predictions. To see this, first consider the case of a DGP with autoregressive disturbances

Table 3: Bias, MSE, and Relative Efficiency Estimators: OLS, FGLS, FGLS-D, DURBIN DGPs: (1) Triangular VAR, NDY + GEXOG, (2) Unrestricted VAR, NDY + EBD

		т	=50		
		 Ψ ₁	<u></u> Ψ ₁ *	Ψ_2	Ψ_2^*
	OLS	0.2376	0.3054	0.5286	0.6828
-	FGLS	0.1083	0.1484	0.4622	0.6367
Bias	FGLS-D	0.0708	0.0520	0.1889	0.2902
	DURBIN	0.0637	0.0386	0.0268	0.0074
	OLS	0.0705	0.1082	0.2989	0.4834
	FGLS	0.0705 0.0286	0.1082	0.2389 0.2494	0.4334 0.4385
MSE	FGLS-D	0.0280 0.0384	0.0400 0.0352	0.2494 0.0980	0.4383 0.1672
	DURBIN				
		0.0408	0.0374	0.0409	0.0300
DD	OLS	1.7284	2.8912	7.3025	16.1337
$\mathrm{RE}_{\mathrm{est}}$	FGLS	0.7021	1.0693	6.0917	14.6353
	FGLS-D	0.9430	0.9393	2.3938	5.5796
		T	=200		
		Ψ_1	Ψ_1^*	Ψ_2	Ψ_2^*
_	OLS	0.2445	0.3174	0.5621	$0.725\overline{2}$
Bias	FGLS	0.1001	0.1413	0.5037	0.6986
	FGLS-D	0.0033	0.0034	0.1947	0.3410
	DURBIN	0.0009	-0.0007	-0.0003	0.0002
	OLS	0.0632	0.1045	0.3206	0.5291
	FGLS	0.0141	0.0246	0.2644	0.4944
MSE	FGLS-D	0.0052	0.0051	0.0557	0.1011 0.1451
	DURBIN	0.0052 0.0052	0.0051 0.0051	0.0051	0.0052
	OLS	12.0344	20.6612	62.1667	
DE					101.5652
RE_{est}	FGLS	2.6880	4.8570	51.2578	94.9083
	FGLS-D	0.9968	1.0006	10.8053	27.8557
			=600		
		Ψ_1	Ψ_1^*	Ψ_2	Ψ_2^*
	OLS	0.2460	0.3218	0.5721	0.7378
Bias	FGLS	0.0980	0.1409	0.5045	0.7176
Dias	FGLS-D	0.0000	0.0012	0.2007	0.3667
	DURBIN	-0.0008	-0.0002	0.0001	0.0008
	OLS	0.0617	0.1048	0.3288	0.5454
MOD	FGLS	0.0110	0.0214	0.2592	0.5169
MSE	FGLS-D	0.0017	0.0017	0.0464	0.1454
	DURBIN	0.0017	0.0017	0.0017	0.0017
	OLS	37.0807	61.9455	199.1306	329.6430
RE_{est}	FGLS	6.6214	12.6578	156.9929	312.4485
- •est	FGLS-D	1.0163	1.0083	28.1260	87.8873
		$\frac{T}{\Psi_1}$	$\frac{=2500}{\Psi_{1}^{*}}$	Ψ_2	Ψ_2^*
	OIS		1		4
	OLS	0.2472	0.3220	0.5756	0.7438
Bias	FGLS	0.0984	0.1400	0.4654	0.7213
	FGLS-D	0.0004	0.0001	0.2034	0.3763
	DURBIN	0.0002	-0.0003	0.0001	-0.0001
	OLS	0.0614	0.1040	0.3316	0.5534
MSE	FGLS	0.0100	0.0200	0.2179	0.5209
MOL	FGLS-D	0.0004	0.0004	0.0430	0.1444
	DURBIN	0.0004	0.0004	0.0004	0.0004
	OLS	153.9376	258.1795	830.3128	1370.2607
RE _{est}	FGLS	25.1163	49.6206	545.5996	1289.7121
	FGLS-D	1.0261	1.0147	107.5807	357.5905
	1.010-0	1.0201	1.0141	101.0001	001.0000

Notes: All shocks are N(0, 1) white noise. We select FGLS, FGLS-D, and DURBIN lag orders using BIC. RE_{est} denotes the relative estimation efficiency of DURBIN. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

Table 4: Bias, MSE, and Relative Efficiency
Estimators: OLS, FGLS, FGLS-D, DURBIN
DGP: Dynamic Regression, EBD

			T=50)		
		$\rho = 0$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$
	OLS	-0.3366	-0.0003	0.2531	0.6886	0.8700
D '	FGLS	-0.3369	-0.0002	0.0329	-0.1000	-0.1536
Bias	FGLS-D	-0.3336	-0.0004	0.0170	-0.1317	-0.1891
	DURBIN	-0.0484	-0.0001	-0.0009	0.0000	-0.0004
	OLS	0.1275	0.0292	0.1305	0.9036	1.9497
MOD	FGLS	0.1297	0.0215	0.0303	0.0423	0.0597
MSE	FGLS-D	0.1275	0.0220	0.0267	0.0400	0.0570
	DURBIN	0.0435	0.0234	0.0224	0.0231	0.0234
	OLS	2.9300	1.2443	5.8337	39.1776	83.4520
RE_{est}	FGLS	2.9827	0.9161	1.3561	1.8348	2.5563
	FGLS-D	2.9310	0.9401	1.1944	1.7358	2.4410
			T=20	0		
		$\rho = 0$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$
	OLS	-0.3462	-0.0004	0.2678	0.7371	0.9235
Ъ .	FGLS	-0.3464	-0.0004	0.0082	-0.1369	-0.1895
Bias	FGLS-D	-0.3457	-0.0004	0.0049	-0.1422	-0.1946
	DURBIN	0.0000	-0.0003	0.0004	0.0005	0.0005
	OLS	0.1231	0.0071	0.0879	0.6648	1.1970
MOD	FGLS	0.1236	0.0047	0.0061	0.0242	0.0408
MSE	FGLS-D	0.1231	0.0047	0.0060	0.0254	0.0425
	DURBIN	0.0051	0.0050	0.0051	0.0053	0.0051
	OLS	24.1127	1.4081	17.2231	124.8315	232.6470
$\mathrm{RE}_{\mathrm{est}}$	FGLS	24.1985	0.9384	1.2010	4.5375	7.9253
111/est						
ruest	FGLS-D	24.0998	0.9342	1.1725	4.7644	8.2576
ru⊔est			0.9342	1.1725	4.7644	8.2576
rubest				1.1725	4.7644 $\rho = 0.9$	8.2576 $\rho = 0.95$
rubest		24.0998	0.9342 T=60	1.1725 D		
	FGLS-D OLS FGLS	24.0998 $\rho = 0$	0.9342 T=60 $\rho = 0.5$	1.1725 0 $\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$
Bias	FGLS-D OLS	24.0998 $\rho = 0$ -0.3489	0.9342 T=60 $\rho = 0.5$ 0.0005	$ \begin{array}{r} 1.1725 \\ \hline 0 \\ \rho = 0.7 \\ \hline 0.2734 \end{array} $	$ \rho = 0.9 $ 0.7502	$ \rho = 0.95 $ 0.9393
	FGLS-D OLS FGLS	24.0998 $\rho = 0$ -0.3489 -0.3488	0.9342 T=600 $\rho = 0.5$ 0.0005 0.0002	$ \begin{array}{r} 1.1725 \\ \hline 0 \\ \rho = 0.7 \\ 0.2734 \\ 0.0036 \\ \end{array} $	$\rho = 0.9 \\ 0.7502 \\ -0.1431$	$ \rho = 0.95 $ 0.9393 -0.1938
	FGLS-D OLS FGLS FGLS-D	$\frac{\rho = 0}{-0.3489}$ -0.3488 -0.3486	0.9342 T=600 $\rho = 0.5$ 0.0005 0.0002 0.0002	$\begin{array}{c} 1.1725\\ \hline \\ \hline \\ \rho = 0.7\\ \hline \\ 0.2734\\ 0.0036\\ 0.0026 \end{array}$	$\rho = 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447$	$\rho = 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952$
Bias	FGLS-D OLS FGLS FGLS-D DURBIN	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002 \end{array}$	0.9342 T=60 $\rho = 0.5$ 0.0005 0.0002 0.0002 0.0002	$\begin{array}{c} 1.1725\\ \hline \\ \hline \\ \rho = 0.7\\ \hline \\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009 \end{array}$	$\rho = 0.9$ 0.7502 -0.1431 -0.1447 -0.0001	$\rho = 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010$
	FGLS-D OLS FGLS FGLS-D DURBIN OLS	$\begin{array}{c} 24.0998\\ \hline \rho = 0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ \hline 0.1228 \end{array}$	0.9342 $T=600$ $\rho = 0.5$ 0.0005 0.0002 0.0002 0.0002 0.0002 0.0002	$\begin{array}{c} 1.1725\\ \hline 0\\ \hline \rho = 0.7\\ \hline 0.2734\\ 0.0036\\ 0.0026\\ \hline 0.0009\\ \hline 0.0803 \end{array}$	$\rho = 0.9$ 0.7502 -0.1431 -0.1447 -0.0001 0.6050	$\rho = 0.95$ 0.9393 -0.1938 -0.1952 0.0010 0.9995
Bias	FGLS-D OLS FGLS FGLS-D DURBIN OLS FGLS	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ \hline\\ 0.1228\\ 0.1229\\ \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0024\\ 0.0015 \end{array}$	$\begin{array}{c} 1.1725\\ \hline 0\\ \hline \rho = 0.7\\ \hline 0.2734\\ 0.0036\\ 0.0026\\ \hline 0.0009\\ \hline 0.0803\\ 0.0020\\ \end{array}$	$\rho = 0.9$ 0.7502 -0.1431 -0.1447 -0.0001 0.6050 0.0221	$\rho = 0.95$ 0.9393 -0.1938 -0.1952 0.0010 0.9995 0.0391
Bias	FGLS-D OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ \hline\\ 0.1228\\ 0.1229\\ 0.1227\\ \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0024\\ 0.0015\\ 0.0015\end{array}$	$\begin{array}{c} 1.1725\\ \hline 0\\ \hline \rho = 0.7\\ \hline 0.2734\\ 0.0036\\ 0.0026\\ \hline 0.0009\\ \hline 0.0803\\ 0.0020\\ \hline 0.0020\\ \hline 0.0020\\ \end{array}$	$\rho = 0.9$ 0.7502 -0.1431 -0.1447 -0.0001 0.6050 0.0221 0.0226	$\rho = 0.95$ 0.9393 -0.1938 -0.1952 0.0010 0.9995 0.0391 0.0396
Bias	FGLS-D OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ \hline\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ \end{array}$	$\begin{array}{c} 0.9342 \\ \hline \mathbf{T=600} \\ \rho=0.5 \\ 0.0005 \\ 0.0002 \\ 0.0002 \\ 0.0002 \\ 0.0002 \\ 0.0024 \\ 0.0015 \\ 0.0015 \\ 0.0017 \end{array}$	$\begin{array}{c} 1.1725\\ \hline 0\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ \hline 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ \end{array}$	$\rho = 0.9$ 0.7502 -0.1431 -0.1447 -0.0001 0.6050 0.0221 0.0226 0.0017	$\rho = 0.95$ 0.9393 -0.1938 -0.1952 0.0010 0.9995 0.0391 0.0396 0.0017
Bias	FGLS-D OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ \hline\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851 \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0024\\ 0.0015\\ 0.0015\\ 0.0017\\ 1.4430\\ \end{array}$	$\begin{array}{c} 1.1725\\ \hline 0\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ \hline 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ \hline 46.0534 \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \end{split}$
Bias	FGLS-D OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ \hline\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851\\ 73.8221 \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0024\\ 0.0015\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363 \end{array}$	$\begin{array}{c} 1.1725\\ \hline \\ \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602 \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \end{split}$
Bias	FGLS-D OLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS FGLS-D	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ 73.7851\\ 73.7851\\ 73.7053\\ \hline\\ \rho=0 \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0015\\ 0.0015\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5 \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7 \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \rho &= 0.95 \end{split}$
Bias	FGLS-D OLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D FGLS-D	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ \hline\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851\\ \hline\\ 73.7851\\ \hline\\ 73.7053\\ \hline\\ \rho=0\\ -0.3495\\ \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ 0.0015\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5\\ 0.0001\\ \end{array}$	$\begin{array}{c} 1.1725\\ \hline \\ \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ \hline 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ \hline 46.0534\\ 1.1720\\ 1.1602\\ \hline \\ 0\\ \hline \rho = 0.7\\ \hline 0.2740\\ \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \hline \rho &= 0.95 \\ 0.9374 \end{split}$
Bias MSE RE _{est}	FGLS-D OLS FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ 73.7851\\ 73.7053\\ \hline\\ \rho=0\\ -0.3495\\ -0.3494\\ \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.00015\\ 0.0015\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5\\ 0.0001\\ 0.0002\\ \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7\\ \hline 0.2740\\ 0.0007\\ \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \hline \rho &= 0.95 \\ 0.9374 \\ -0.1959 \end{split}$
Bias	FGLS-D OLS FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D OLS FGLS-D	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ 73.7851\\ 73.7053\\ \hline\\ \rho=0\\ -0.3495\\ -0.3494\\ -0.3494\\ \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.00015\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5\\ 0.0001\\ 0.0002\\ 0.0002\\ \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7\\ 0.2740\\ 0.0007\\ 0.0005\\ \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \hline \rho &= 0.95 \\ 0.9374 \\ -0.1959 \\ -0.1962 \end{split}$
Bias MSE RE _{est}	FGLS-D OLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D OLS FGLS-D FGLS FGLS FGLS	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851\\ \hline\\ 73.7053\\ \hline\\ \rho=0\\ -0.3495\\ -0.3494\\ -0.3494\\ 0.0003\\ \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.00015\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \mathbf{P=0.5}\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7\\ 0.2740\\ 0.0007\\ 0.0005\\ 0.0000\\ \hline \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \hline \rho &= 0.95 \\ 0.9374 \\ -0.1959 \\ -0.1962 \\ 0.0002 \\ \end{split}$
Bias MSE RE _{est}	FGLS-D OLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D CLS FGLS-D DURBIN OLS	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851\\ \hline\\ 73.7053\\ \hline\\ \rho=0\\ -0.3495\\ -0.3494\\ -0.3494\\ 0.0003\\ \hline\\ 0.1224\\ \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.00015\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5\\ 0.0001\\ 0.0002\\ 0.0002\\ \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7\\ 0.2740\\ 0.0007\\ 0.0005\\ \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \hline \rho &= 0.95 \\ 0.9374 \\ -0.1959 \\ -0.1962 \end{split}$
Bias MSE RE _{est} Bias	FGLS-D OLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D FGLS-D CLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851\\ 73.8221\\ \hline\\ 73.7053\\ \hline\\ \rho=0\\ -0.3495\\ -0.3494\\ -0.3494\\ 0.0003\\ \hline\\ 0.1224\\ 0.1224\\ \hline\end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0006\\ 0.0004\\ \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7\\ 0.2740\\ 0.0007\\ 0.0005\\ 0.0000\\ 0.0764\\ 0.0005\\ \hline \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \end{split}$
Bias MSE RE _{est}	FGLS-D OLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D CLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851\\ \hline\\ 73.8221\\ \hline\\ 73.7053\\ \hline\\ \rho=0\\ -0.3495\\ -0.3494\\ -0.3494\\ 0.0003\\ \hline\\ 0.1224\\ 0.1223\\ \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0004\\ \hline \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7\\ 0.2740\\ 0.0007\\ 0.0005\\ 0.0000\\ \hline 0.0764\\ 0.0005\\ 0.0004\\ \hline \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \end{split}$
Bias MSE RE _{est} Bias	FGLS-D OLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D FGLS-D CLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851\\ 73.8221\\ \hline\\ 73.7053\\ \hline\\ \rho=0\\ -0.3495\\ -0.3494\\ -0.3494\\ 0.0003\\ \hline\\ 0.1224\\ 0.1224\\ \hline\end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0006\\ 0.0004\\ \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7\\ 0.2740\\ 0.0007\\ 0.0005\\ 0.0000\\ 0.0764\\ 0.0005\\ \hline \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \end{split}$
Bias MSE RE _{est} Bias	FGLS-D OLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D CLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851\\ \hline\\ 73.8221\\ \hline\\ 73.7053\\ \hline\\ \rho=0\\ -0.3495\\ -0.3494\\ -0.3494\\ 0.0003\\ \hline\\ 0.1224\\ 0.1223\\ \end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0004\\ \hline \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7\\ 0.2740\\ 0.0007\\ 0.0005\\ 0.0000\\ \hline 0.0764\\ 0.0005\\ 0.0004\\ \hline \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \end{split}$
Bias MSE RE _{est} Bias	FGLS-D OLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} 24.0998\\ \hline\\ \rho=0\\ -0.3489\\ -0.3488\\ -0.3486\\ -0.0002\\ 0.1228\\ 0.1229\\ 0.1227\\ 0.0017\\ \hline\\ 73.7851\\ \hline\\ 73.8221\\ \hline\\ 73.7053\\ \hline\\ \rho=0\\ -0.3494\\ -0.3494\\ -0.3494\\ 0.0003\\ \hline\\ 0.1224\\ 0.1223\\ 0.0004\\ \hline\end{array}$	$\begin{array}{c} 0.9342\\ \hline \mathbf{T=600}\\ \rho=0.5\\ 0.0005\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0015\\ 0.0015\\ 0.0017\\ 1.4430\\ 0.9363\\ 0.9356\\ \hline \mathbf{T=250}\\ \rho=0.5\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ 0.0004\\ 0.0004\\ 0.0004\\ \hline \end{array}$	$\begin{array}{c} 1.1725\\ \hline \rho = 0.7\\ 0.2734\\ 0.0036\\ 0.0026\\ 0.0009\\ 0.0803\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0020\\ 0.0017\\ \hline 46.0534\\ 1.1720\\ 1.1602\\ \hline \rho = 0.7\\ 0.2740\\ 0.0007\\ 0.0005\\ 0.0000\\ \hline 0.0764\\ 0.0005\\ 0.0004\\ 0.0004\\ \hline \end{array}$	$\begin{split} \rho &= 0.9 \\ 0.7502 \\ -0.1431 \\ -0.1447 \\ -0.0001 \\ 0.6050 \\ 0.0221 \\ 0.0226 \\ 0.0017 \\ 364.0187 \\ 13.3167 \\ 13.3167 \\ 13.5727 \\ \end{split}$	$\begin{split} \rho &= 0.95 \\ 0.9393 \\ -0.1938 \\ -0.1952 \\ 0.0010 \\ 0.9995 \\ 0.0391 \\ 0.0396 \\ 0.0017 \\ 596.3733 \\ 23.3308 \\ 23.6306 \\ \end{split}$

Notes: All shocks are N(0,1) white noise. We select FGLS, FGLS-D, and DURBIN lag orders using BIC. RE_{est} denotes the relative estimation efficiency of DURBIN. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details. 24

and known parameter $\beta = 1.^{18}$ Specifically consider the DGP given by

$$y_t = x_t + u_t$$
$$x_t = \rho x_{t-1} + \epsilon_{x,t}$$
$$u_t = \rho u_{t-1} + \epsilon_{u,t},$$

with all shocks N(0,1) and orthogonal at all leads and lags. For this DGP, the optimal prediction accounting for serial correlation in u is

$$y_{t+1,t}^{opt} = x_{t+1,t} + u_{t+1,t}$$

= $\rho x_t + \rho u_t$, (21)

and the corresponding prediction error is $e_{t+1}^{opt} = \varepsilon_{x,t+1} + \varepsilon_{u,t+1}$, with variance $\sigma_{opt}^2 = 2$.

The suboptimal prediction, failing to account for serial correlation in u, is just the first term in (21),

$$y_{t+1,t}^{subopt} = \rho x_t$$

with corresponding prediction error $e_{t+1}^{subopt} = \varepsilon_{x,t+1} + u_{t+1}$, and variance $\sigma_{subopt}^2 = 1 + \frac{1}{1-\rho^2}$.

Both predictions are unbiased, so the prediction efficiency of DURBIN relative to OLS (RE_{pred}) is just the relative variance, which is

$$RE_{pred} = \frac{\sigma_{subopt}^2}{\sigma_{opt}^2} = \frac{1}{2} + \frac{1}{2(1-\rho^2)}.$$
(22)

 RE_{pred} is bounded below by 1, which occurs when $\rho=0$, and $\text{RE}_{\text{pred}}\rightarrow\infty$ monotonically as $\rho\rightarrow1$.

Now we consider the case of estimated parameters, which is more complicated. In Table 5 we show RE_{pred} estimated by Monte Carlo, accounting for parameter estimation uncertainty. For all but the most extreme cases (e.g., T = 50 with $\rho = 0.99$) the Monte Carlo results are almost identical to the analytic result (22) that ignores parameter estimation uncertainty.¹⁹ Hence RE_{pred} depends strongly on ρ but not on T. More precisely, for any T we of course obtain RE_{pred} = 1 in the white noise case ($\rho = 0$), but then RE_{pred} grows quickly in ρ , and for any ρ , RE_{pred} stabilizes extremely quickly in T and is basically constant.

¹⁸We start with the case of known parameter β , as it can easily be solved analytically.

¹⁹This is because the effects of parameter estimation uncertainty on MSPE vanish quickly (like 1/T rather than $1/\sqrt{T}$), as is well known. Hence the earlier-documented poor estimation efficiency of OLS relative to DURBIN, although a large problem for some purposes, is not an important problem for prediction.

	Relative Prediction Efficiency (RE_{pred})										
Т	$\rho = 0$	$\rho = 0.3$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$	$\rho = 0.99$				
50	0.989	1.042	1.160	1.452	3.033	5.865	391.908				
200	0.997	1.051	1.168	1.476	3.121	5.698	47.361				
600	1.000	1.047	1.152	1.505	3.214	5.605	25.569				
2500	1.000	1.049	1.163	1.469	3.101	5.656	25.648				

Table 5: Prediction Efficiency of DURBIN Relative to OLS DGP: Autoregressive Disturbances, NDY + EBD

Notes: All shocks are N(0,1) white noise. RE_{pred} is the relative predictive efficiency of DURBIN, RE_{pred}=MSPE(OLS)/MSPE(DURBIN), where MSPE is 1-step-ahead mean squared prediction error. We select the DURBIN lag order using BIC. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

4.5 Inference

Now we consider the finite-sample properties of hypothesis tests associated with the various estimation procedures. We first consider test sizes, after which we consider rejection frequencies. In all tables in this section we consider the following estimators: OLS with unadjusted standard errors, five OLS-HAC estimators (NW, NW-A, NW-LLSW, NW-KV, and M-LLSW), FGLS, FGLS-D, and two implementations of DURBIN, one using BIC for lag order selection and the other using AIC. Additionally, we have included two Hausman tests; the first null hypothesis is that FGLS is efficient relative to OLS, and the second is that FGLS-D is efficient relative to DURBIN.

4.5.1 Size

Table 6 contains results for the autoregressive disturbances DGP, NDY + BD. First, tests based on OLS are incorrectly sized for all (ρ, T) combinations, except when $\rho = 0$, and the size distortions become huge as ρ grows. Second, the various NW HAC corrections reduce but do not eliminate the size distortion. In particular, distortion generally remains in the economically crucial region of $\rho \in [0.5, 0.99]$, depending on the sample size and the precise NW version used. NW and NW-A are worst, NW-LLSW are better, and NW-KV is the best. The M-LLSW HAC correction is different in that it exhibits an approximately correct size across (ρ, T) combinations. Finally, tests based on FGLS, FGLS-D and DURBIN, in contrast, are correctly sized for all (ρ, T) combinations, even with extremely strong autocorrelation. This holds regardless of whether DURBIN lag order selection is done with BIC or AIC.

			T=5	0				
	Truncation	$\rho = 0$	$\rho = 0.3$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$	$\rho = 0.99$
OLS	_	0.051	0.106	0.167	0.245	0.346	0.380	0.407
NW	$h = \left[4(T/100)^{2/9}\right]$	0.066	0.088	0.113	0.141	0.200	0.227	0.263
NW-A	$h = [0.75T^{1/3}]$	0.064	0.093	0.121	0.160	0.230	0.264	0.294
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	0.064	0.078	0.091	0.110	0.123	0.137	0.196
NW-KV	h = T	0.061	0.075	0.081	0.097	0.091	0.090	0.155
M-LLSW	$\nu = 4(T/100)^{2/9} $	0.065	0.069	0.077	0.087	0.086	0.102	0.167
FGLS	BIC	0.066	0.076	0.082	0.076	0.076	0.084	0.054
FGLS-D	BIC	0.054	0.095	0.090	0.069	0.057	0.059	0.052
DURBIN	BIC	0.060	0.099	0.082	0.058	0.053	0.058	0.051
DURBIN	AIC	0.086	0.093	0.088	0.078	0.076	0.080	0.076
Hausman 1	OLS vs FGLS		0.738	0.632	0.446	0.253	0.239	0.274
Hausman 2	DURBIN vs FGLS-D		0.052	0.091	0.121	0.119	0.118	0.100
iiaasiiiaii 2	DOILDIN VS I GLO D		T=20		0.121	0.110	0.110	0.100
	Truncation	$\rho = 0$	$\rho = 0.3$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$	$\rho = 0.99$
OLS	_	0.051	0.110	0.174	0.252	0.352	0.386	0.413
NW	$h = \lceil 4(T/100)^{2/9} \rceil$	0.059	0.067	0.085	0.107	0.142	0.157	0.174
NW-A	$h = \left[0.75T^{1/3}\right]$	0.059	0.067	0.085	0.107	0.142	0.157	0.174
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	0.059	0.060	0.068	0.072	0.080	0.076	0.084
NW-KV	h = T	0.053	0.056	0.061	0.060	0.061	0.049	0.032
M-LLSW	$\nu = 4(T/100)^{2/9} $	0.060	0.059	0.063	0.063	0.066	0.063	0.076
FGLS	$\mathcal{D} = \left[4(1/100)^{-1} \right]$ BIC	0.055	0.053 0.054	0.005 0.056	0.005 0.055	0.050	0.003	0.048
FGLS-D	BIC	0.050 0.051	0.061	0.054	0.054	0.052 0.053	0.051	0.050
DURBIN	BIC	0.051 0.053	0.061	0.049	0.054 0.052	0.055 0.051	0.051	0.049
DURBIN	AIC	0.055 0.066	0.054	0.049 0.053	0.052 0.056	0.051 0.056	$0.055 \\ 0.057$	0.049 0.052
Hausman 1	OLS vs FGLS	0.000	0.622	0.055	0.030	0.126	0.007	0.032
Hausman 2	DURBIN vs FGLS-D		0.022	0.433 0.067	0.212	0.120 0.074	0.066	0.125
mausinan 2	DOILDIN VS FOLD-D		T=60		0.035	0.014	0.000	0.002
	Truncation	$\rho = 0$	$\rho = 0.3$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$	$\rho = 0.99$
OLS	_	0.049	0.117	0.175	0.249	0.351	0.379	0.408
NW	$h = \lceil 4(T/100)^{2/9} \rceil$	0.049	0.065	0.070	0.086	0.114	0.120	0.134
NW-A	$h = [0.75T^{1/3}]$	0.049	0.064	0.068	0.082	0.104	0.109	0.121
NW-LLSW	$h = \begin{bmatrix} 0.75T^{1/3} \\ h = \begin{bmatrix} 1.3T^{1/2} \end{bmatrix}$	0.051	0.057	0.057	0.057	0.065	0.058	0.050
NW-KV				0.053	0.053	0.050	0.042	
	h = 1	0.049	0 0.50					0.017
	h = T $\mu = A(T/100)^{2/9} $	0.049 0.051	0.050					0.017 0.052
M-LLSW	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$	0.051	0.054	0.054	0.055	0.057	0.051	0.052
M-LLSW FGLS	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC	$\begin{array}{c} 0.051 \\ 0.050 \end{array}$	$0.054 \\ 0.055$	$\begin{array}{c} 0.054 \\ 0.051 \end{array}$	$0.055 \\ 0.049$	$0.057 \\ 0.047$	$\begin{array}{c} 0.051 \\ 0.051 \end{array}$	$0.052 \\ 0.051$
M-LLSW FGLS FGLS-D	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \end{array}$	$\begin{array}{c} 0.054 \\ 0.055 \\ 0.055 \end{array}$	$\begin{array}{c} 0.054 \\ 0.051 \\ 0.050 \end{array}$	$\begin{array}{c} 0.055 \\ 0.049 \\ 0.049 \end{array}$	$\begin{array}{c} 0.057 \\ 0.047 \\ 0.047 \end{array}$	$\begin{array}{c} 0.051 \\ 0.051 \\ 0.051 \end{array}$	$\begin{array}{c} 0.052 \\ 0.051 \\ 0.051 \end{array}$
M-LLSW FGLS FGLS-D DURBIN	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.049 \end{array}$	$\begin{array}{c} 0.054 \\ 0.055 \\ 0.055 \\ 0.055 \end{array}$	$\begin{array}{c} 0.054 \\ 0.051 \\ 0.050 \\ 0.049 \end{array}$	$0.055 \\ 0.049 \\ 0.049 \\ 0.049$	$0.057 \\ 0.047 \\ 0.047 \\ 0.045$	$\begin{array}{c} 0.051 \\ 0.051 \\ 0.051 \\ 0.048 \end{array}$	$0.052 \\ 0.051 \\ 0.051 \\ 0.049$
M-LLSW FGLS FGLS-D DURBIN DURBIN	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \end{array}$	$\begin{array}{c} 0.054 \\ 0.055 \\ 0.055 \\ 0.055 \\ 0.055 \\ 0.056 \end{array}$	$\begin{array}{c} 0.054 \\ 0.051 \\ 0.050 \\ 0.049 \\ 0.050 \end{array}$	$\begin{array}{c} 0.055 \\ 0.049 \\ 0.049 \\ 0.049 \\ 0.049 \\ 0.050 \end{array}$	$0.057 \\ 0.047 \\ 0.047 \\ 0.045 \\ 0.046$	$\begin{array}{c} 0.051 \\ 0.051 \\ 0.051 \\ 0.048 \\ 0.048 \end{array}$	$0.052 \\ 0.051 \\ 0.051 \\ 0.049 \\ 0.051$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC OLS vs FGLS	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.049 \end{array}$	$\begin{array}{c} 0.054 \\ 0.055 \\ 0.055 \\ 0.055 \\ 0.056 \\ \hline 0.533 \end{array}$	$\begin{array}{c} 0.054 \\ 0.051 \\ 0.050 \\ 0.049 \\ 0.050 \\ \hline 0.296 \end{array}$	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.049\\ 0.050\\ \hline 0.115 \end{array}$	$\begin{array}{r} 0.057 \\ 0.047 \\ 0.047 \\ 0.045 \\ 0.046 \\ \hline 0.088 \end{array}$	$\begin{array}{r} 0.051 \\ 0.051 \\ 0.051 \\ 0.048 \\ 0.048 \\ \hline 0.077 \end{array}$	$\begin{array}{c} 0.052 \\ 0.051 \\ 0.051 \\ 0.049 \\ 0.051 \\ \hline 0.069 \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.049 \end{array}$	$\begin{array}{c} 0.054 \\ 0.055 \\ 0.055 \\ 0.055 \\ 0.056 \\ 0.533 \\ 0.052 \end{array}$	$\begin{array}{c} 0.054 \\ 0.051 \\ 0.050 \\ 0.049 \\ 0.050 \\ \hline 0.296 \\ 0.052 \end{array}$	0.055 0.049 0.049 0.049 0.049 0.050	$0.057 \\ 0.047 \\ 0.047 \\ 0.045 \\ 0.046$	$\begin{array}{c} 0.051 \\ 0.051 \\ 0.051 \\ 0.048 \\ 0.048 \end{array}$	$0.052 \\ 0.051 \\ 0.051 \\ 0.049 \\ 0.051$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.049 \\ 0.063 \end{array}$	0.054 0.055 0.055 0.055 0.056 0.533 0.052 T=25	0.054 0.051 0.050 0.049 0.050 0.296 0.052 00	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.049\\ 0.050\\ \hline 0.115\\ 0.089\\ \end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ \hline 0.088\\ 0.059\\ \end{array}$	$\begin{array}{c} 0.051 \\ 0.051 \\ 0.051 \\ 0.048 \\ 0.048 \\ \hline 0.077 \\ 0.051 \end{array}$	$\begin{array}{c} 0.052 \\ 0.051 \\ 0.051 \\ 0.049 \\ 0.051 \\ 0.069 \\ 0.054 \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC OLS vs FGLS	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.063 \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ 0.533\\ 0.052\\ \textbf{T=25}\\ \rho=0.3 \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline 0.296\\ 0.052\\ \hline \textbf{00}\\ \hline \rho=0.5\\ \end{array}$	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.049\\ 0.050\\ 0.115\\ 0.089\\ \end{array}$ $\rho=0.7$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ 0.088\\ 0.059\\ \end{array}$ $\rho=0.9$	$\begin{array}{c} 0.051 \\ 0.051 \\ 0.051 \\ 0.048 \\ 0.048 \\ \hline 0.077 \\ 0.051 \\ \hline \rho = 0.95 \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ \hline 0.069\\ 0.054\\ \end{array}$ $\rho=0.99$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS	$\begin{split} \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ BIC \\ BIC \\ BIC \\ AIC \\ OLS vs FGLS \\ DURBIN vs FGLS-D \\ \hline \\ Truncation \\ - \end{split}$	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.063 \\ \end{array}$ $\begin{array}{c} \rho = 0 \\ 0.050 \\ 0.050 \\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.110\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.052\\ 0$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline 0.0296\\ 0.052\\ \hline \textbf{00}\\ \hline \rho = 0.5\\ 0.179\\ 0.051\\ \hline 0.0179\\ 0.051\\ \hline 0.0179\\ \hline 0.010\\ 0.010\\ \hline 0.010\\ \hline$	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.049\\ 0.050\\ \hline 0.115\\ 0.089\\ \hline \rho = 0.7\\ 0.246\\ \hline 0.246\\$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ 0.088\\ 0.059\\ \hline\\ \rho=0.9\\ 0.352\\ \end{array}$	$\begin{array}{c} 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.048\\ 0.077\\ 0.051\\ \hline\\ \rho=0.95\\ 0.376\\ 0.376\\ \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ 0.069\\ 0.054\\ \hline\\ \rho=0.99\\ 0.405\\ 0.405\\ \hline\end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation - h = [4(T/100)^{2/9}]	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.063 \\ \end{array}$ $\begin{array}{c} \rho = 0 \\ 0.050 \\ 0.050 \\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline 0.0296\\ 0.052\\ \hline \textbf{00}\\ \hline \rho = 0.5\\ \hline 0.179\\ 0.063\\ \hline \end{array}$	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ 0.115\\ 0.089\\ \hline\\ \rho=0.7\\ 0.246\\ 0.068\\ \end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ 0.088\\ 0.059\\ \hline\\ \rho=0.9\\ 0.352\\ 0.088\\ \end{array}$	$\begin{array}{c} 0.051 \\ 0.051 \\ 0.051 \\ 0.048 \\ 0.048 \\ \hline 0.077 \\ 0.051 \\ \hline \rho = 0.95 \\ \hline 0.376 \\ 0.093 \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ \hline 0.069\\ 0.054\\ \hline \rho = 0.99\\ 0.405\\ 0.093\\ \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A	$\begin{split} \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \hline \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ h &= \lceil 4(T/100)^{2/9} \rceil \\ h &= \lceil 0.75T^{1/3} \rceil \end{split}$	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.049 \\ 0.063 \end{array}$ $\begin{array}{c} \rho = 0 \\ 0.050 \\ 0.050 \\ 0.050 \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ \hline 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ 0.052\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline 0.052\\ \hline 00\\ \hline \rho = 0.5\\ \hline 0.179\\ 0.063\\ 0.060\\ \hline \end{array}$	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ 0.115\\ 0.089\\ \hline\\ \rho=0.7\\ 0.246\\ 0.068\\ 0.065\\ \end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ \hline 0.088\\ 0.059\\ \hline \rho=0.9\\ \hline 0.352\\ 0.088\\ 0.081\\ \end{array}$	$\begin{array}{c} 0.051 \\ 0.051 \\ 0.051 \\ 0.048 \\ 0.048 \\ \hline 0.077 \\ 0.051 \\ \hline \rho = 0.95 \\ \hline 0.376 \\ 0.093 \\ 0.085 \\ \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ \hline \\ 0.069\\ 0.054\\ \hline \\ \rho=0.99\\ 0.405\\ 0.093\\ 0.082\\ \end{array}$
M-LLSW FGLS FGLS-D DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-A NW-LLSW	$\begin{split} \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \hline \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ h &= \lceil 4(T/100)^{2/9} \rceil \\ h &= \lceil 0.75T^{1/3} \rceil \\ h &= \lceil 1.3T^{1/2} \rceil \end{split}$	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.063 \\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ \hline 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ 0.052\\ 0.048\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline \end{array} \\ \hline \begin{array}{c} 0.296\\ 0.052\\ \hline \end{array} \\ \hline \begin{array}{c} 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ $	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ \hline 0.115\\ 0.089\\ \hline \rho=0.7\\ \hline 0.246\\ 0.068\\ 0.065\\ 0.052\\ \end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ \hline 0.088\\ 0.059\\ \hline \rho=0.9\\ \hline 0.352\\ 0.088\\ 0.081\\ 0.057\\ \hline \end{array}$	$\begin{array}{c} 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.048\\ \hline 0.077\\ 0.051\\ \hline \end{array}$ $\begin{array}{c} \rho = 0.95\\ 0.376\\ 0.093\\ 0.085\\ 0.056\\ \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ \hline \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW NW-KV	$\begin{split} \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \hline \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ h &= \lceil 4(T/100)^{2/9} \rceil \\ h &= \lceil 0.75T^{1/3} \rceil \\ h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \end{split}$	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.063 \\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ \hline 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ 0.052\\ 0.048\\ 0.047\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline \end{array} \\ \hline \begin{array}{c} 0.296\\ 0.052\\ \hline \end{array} \\ \hline \begin{array}{c} 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ $	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ \hline 0.115\\ 0.089\\ \hline \rho=0.7\\ \hline 0.246\\ 0.068\\ 0.065\\ 0.052\\ 0.049\\ \hline \end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ 0.088\\ 0.059\\ \hline\\ \rho=0.9\\ 0.352\\ 0.088\\ 0.081\\ 0.057\\ 0.050\\ \end{array}$	$\begin{array}{c} 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.048\\ \hline 0.077\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ \hline \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW M-LLSW	$\begin{split} \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \hline \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ h &= \lceil 4(T/100)^{2/9} \rceil \\ h &= \lceil 0.75T^{1/3} \rceil \\ h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \end{split}$	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.063 \\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ \hline 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ 0.052\\ 0.048\\ 0.047\\ 0.047\\ \hline 0.047\\ \hline \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline \end{array} \\ \hline \begin{array}{c} 0.296\\ 0.052\\ \hline \end{array} \\ \hline \begin{array}{c} 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ $	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ \hline 0.115\\ 0.089\\ \hline \rho=0.7\\ 0.246\\ 0.068\\ 0.065\\ 0.052\\ 0.049\\ 0.051\\ \end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ \hline \end{array}$	$\begin{array}{c} 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.048\\ \hline 0.077\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ \hline \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW NW-KV M-LLSW FGLS	$\begin{split} \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \hline \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ h &= \lceil 4(T/100)^{2/9} \rceil \\ h &= \lceil 0.75T^{1/3} \rceil \\ h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \end{split}$	$\begin{array}{c} 0.051 \\ 0.050 \\ 0.049 \\ 0.063 \\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ \hline 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ 0.052\\ 0.048\\ 0.047\\ 0.047\\ 0.048\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline \end{array} \\ \hline \begin{array}{c} 0.296\\ 0.052\\ \hline \end{array} \\ \hline \begin{array}{c} 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ $	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ \hline \\ 0.115\\ 0.089\\ \hline \\ \rho=0.7\\ \hline \\ 0.246\\ 0.068\\ 0.065\\ 0.052\\ 0.052\\ 0.049\\ 0.051\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ \hline \end{array}$	$\begin{array}{c} 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.048\\ \hline 0.077\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ \hline \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D	$\begin{split} \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \hline \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ h &= \lceil 4(T/100)^{2/9} \rceil \\ h &= \lceil 0.75T^{1/3} \rceil \\ h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \hline \\ \end{bmatrix} \end{split}$	$\begin{array}{c} 0.051\\ 0.050\\ 0.049\\ 0.063\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ \hline 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ 0.052\\ 0.048\\ 0.047\\ 0.047\\ 0.048\\ 0.048\\ 0.048\\ \hline 0.055\\ \hline 0.055\\$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline \end{array}$ $\begin{array}{c} 0.296\\ 0.052\\ \hline \end{array}$ $\begin{array}{c} 0\\ \rho=0.5\\ 0.179\\ 0.063\\ 0.063\\ 0.060\\ 0.052\\ 0.050\\ 0.052\\ 0.051\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ 0.115\\ 0.089\\ \hline \rho=0.7\\ 0.246\\ 0.068\\ 0.065\\ 0.052\\ 0.049\\ 0.051\\ 0.050\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ 0.088\\ 0.059\\ \hline\\ \rho=0.9\\ 0.352\\ 0.088\\ 0.081\\ 0.057\\ 0.050\\ 0.053\\ 0.048\\ 0.048\\ 0.048\\ \end{array}$	$\begin{array}{c} 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.048\\ \hline 0.077\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ 0.069\\ 0.054\\ \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation $-$ $h = \lceil 4(T/100)^{2/9} \rceil$ $h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC	$\begin{array}{c} 0.051\\ 0.050\\ 0.049\\ 0.063\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ 0.052\\ 0.048\\ 0.047\\ 0.047\\ 0.048\\ 0.048\\ 0.048\\ 0.050\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline \end{array}$ $\begin{array}{c} 0.296\\ 0.052\\ \hline \end{array}$ $\begin{array}{c} 0\\ \rho = 0.5\\ 0.179\\ 0.063\\ 0.063\\ 0.063\\ 0.052\\ 0.050\\ 0.052\\ 0.051\\ 0.050\\ 0.050\\ 0.049\\ \end{array}$	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ 0.115\\ 0.089\\ \hline\\ \rho=0.7\\ 0.246\\ 0.068\\ 0.065\\ 0.052\\ 0.049\\ 0.051\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ \hline\end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ 0.088\\ 0.059\\ \hline\\ \rho=0.9\\ 0.352\\ 0.088\\ 0.081\\ 0.057\\ 0.050\\ 0.053\\ 0.048\\ 0.048\\ 0.048\\ 0.048\\ \hline\end{array}$	$\begin{array}{c} 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.048\\ 0.077\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ 0.069\\ 0.054\\ \hline\\ \rho=0.99\\ 0.405\\ 0.093\\ 0.042\\ 0.042\\ 0.042\\ 0.027\\ 0.042\\ 0.052\\ 0.053\\ 0.049\\ \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW FGLS FGLS-D DURBIN DURBIN	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation - $h = \lceil 4(T/100)^{2/9} \rceil$ $h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ h = T $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC	$\begin{array}{c} 0.051\\ 0.050\\ 0.049\\ 0.063\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ 0.052\\ 0.048\\ 0.047\\ 0.048\\ 0.047\\ 0.048\\ 0.048\\ 0.048\\ 0.050\\ 0.050\\ 0.050\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline \end{array}$ $\begin{array}{c} 0.296\\ 0.052\\ \hline \end{array}$ $\begin{array}{c} 0\\ 0\\ \hline \end{array}$ $\begin{array}{c} \rho = 0.5\\ 0.179\\ 0.063\\ 0.063\\ 0.060\\ 0.052\\ 0.051\\ 0.050\\ 0.051\\ 0.050\\ 0.049\\ 0.049\\ 0.049\\ \end{array}$	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ 0.115\\ 0.089\\ \hline\\ \rho=0.7\\ 0.246\\ 0.068\\ 0.065\\ 0.052\\ 0.049\\ 0.051\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ \hline\end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ 0.088\\ 0.059\\ \hline\\ \rho=0.9\\ 0.352\\ 0.088\\ 0.081\\ 0.057\\ 0.053\\ 0.053\\ 0.048\\ 0.048\\ 0.048\\ 0.048\\ 0.047\\ \hline\end{array}$	$\begin{array}{c} 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.048\\ 0.077\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ 0.069\\ 0.054\\ \hline\\ \hline\\ \rho=0.99\\ 0.405\\ 0.093\\ 0.042\\ 0.042\\ 0.042\\ 0.042\\ 0.052\\ 0.053\\ 0.049\\ 0.050\\ \end{array}$
M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation $-$ $h = \lceil 4(T/100)^{2/9} \rceil$ $h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC	$\begin{array}{c} 0.051\\ 0.050\\ 0.049\\ 0.063\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.055\\ 0.055\\ 0.055\\ 0.056\\ 0.533\\ 0.052\\ \hline \mathbf{T=25}\\ \rho=0.3\\ 0.110\\ 0.053\\ 0.052\\ 0.048\\ 0.047\\ 0.047\\ 0.048\\ 0.048\\ 0.048\\ 0.050\\ \end{array}$	$\begin{array}{c} 0.054\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline \end{array}$ $\begin{array}{c} 0.296\\ 0.052\\ \hline \end{array}$ $\begin{array}{c} 0\\ \rho = 0.5\\ 0.179\\ 0.063\\ 0.063\\ 0.063\\ 0.052\\ 0.050\\ 0.052\\ 0.051\\ 0.050\\ 0.050\\ 0.049\\ \end{array}$	$\begin{array}{c} 0.055\\ 0.049\\ 0.049\\ 0.050\\ 0.115\\ 0.089\\ \hline\\ \rho=0.7\\ 0.246\\ 0.068\\ 0.065\\ 0.052\\ 0.049\\ 0.051\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ \hline\end{array}$	$\begin{array}{c} 0.057\\ 0.047\\ 0.047\\ 0.045\\ 0.046\\ 0.088\\ 0.059\\ \hline\\ \rho=0.9\\ 0.352\\ 0.088\\ 0.081\\ 0.057\\ 0.050\\ 0.053\\ 0.048\\ 0.048\\ 0.048\\ 0.048\\ \hline\end{array}$	$\begin{array}{c} 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.048\\ 0.077\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.051\\ 0.051\\ 0.049\\ 0.051\\ 0.069\\ 0.054\\ \hline\\ \rho=0.99\\ 0.405\\ 0.093\\ 0.042\\ 0.042\\ 0.042\\ 0.027\\ 0.042\\ 0.052\\ 0.053\\ 0.049\\ \end{array}$

Table 6: Empirical Size of Nominal 5% t-test of $H_0: \beta = 1$ DGP: Autoregressive Disturbances, NDY + BD

	T=50	0			
	Truncation	Ψ_1	Ψ_1^*	Ψ_2	Ψ_2^*
OLS	_	0.613	0.787	0.969	0.992
NW	$h = \left[4(T/100)^{2/9}\right]$	0.558	0.730	0.954	0.989
NW-A	$h = [0.75T^{1/3}]$	0.568	0.743	0.959	0.990
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	0.507	0.676	0.928	0.980
NW-KV	h = T	0.438	0.586	0.874	0.958
M-LLSW	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$	0.447	0.607	0.899	0.970
FGLS	BIC	0.221	0.322	0.883	0.959
FGLS-D	BIC	0.309	0.248	0.505	0.627
DURBIN	BIC	0.276	0.200	0.124	0.070
DURBIN	AIC	0.133	0.099	0.087	0.078
Hausman 1	OLS vs FGLS	0.880	0.899	0.693	0.740
Hausman 2	DURBIN vs FGLS-D	0.006	0.009	0.427	0.640
	T=20	0			
	Truncation	Ψ_1	Ψ_1^*	Ψ_2	Ψ_2^*
OLS	_	0.990	0.999	1.000	1.000
NW	$h = \lceil 4(T/100)^{2/9} \rceil$	0.983	0.999	1.000	1.000
NW-A	$h = [0.75T^{1/3}]$	0.983	0.999	1.000	1.000
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	0.974	0.998	1.000	1.000
NW-KV	h = T	0.872	0.959	0.999	1.000
M-LLSW	$\nu = 4(T/100)^{2/9} $	0.969	0.996	1.000	1.000
FGLS	BIC	0.453	0.688	0.999	1.000
FGLS-D	BIC	0.125	0.123	0.735	0.903
DURBIN	BIC	0.047	0.047	0.048	0.052
DURBIN	AIC	0.047	0.051	0.054	0.054
Hausman 1	OLS vs FGLS	0.994	0.998	0.516	0.457
Hausman 2	DURBIN vs FGLS-D	0.000	0.000	0.910	0.978
	T=60				
	Truncation	Ψ_1	Ψ_1^*	Ψ_2	Ψ_2^*
OLS	_	1.000	1.000	1.000	1.000
NW	$h = \left\lceil 4(T/100)^{2/9} \right\rceil$	1.000	1.000	1.000	1.000
NW-A	$h = \left\lceil 0.75T^{1/3} \right\rceil$	1.000	1.000	1.000	1.000
NW-LLSW	$h = [1.3T^{1/2}]$	1.000	1.000	1.000	1.000
NW-KV	h = T	0.997	1.000	1.000	1.000
M-LLSW	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$	1.000	1.000	1.000	1.000
FGLS	BIC	0.831	0.978	1.000	1.000
FGLS-D	BIC	0.122	0.128	0.956	0.998
DURBIN	BIC	0.048	0.051	0.051	0.048
DURBIN	AIC	0.049	0.053	0.052	0.047
Hausman 1	OLS vs FGLS	1.000	1.000	0.669	0.273
Hausman 2	DURBIN vs FGLS-D	0.000	0.000	1.000	1.000
	T=250				
	Truncation	Ψ_1	Ψ_1^*	Ψ_2	Ψ_2^*
OLS	-	1.000	1.000	1.000	1.000
NW	$h = \left\lceil 4(T/100)^{2/9} \right\rceil$	1.000	1.000	1.000	1.000
NW-A	$h = \left\lceil 0.75T^{1/3} \right\rceil$	1.000	1.000	1.000	1.000
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	1.000	1.000	1.000	1.000
NW-KV	h = T	1.000	1.000	1.000	1.000
M-LLSW	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$	1.000	1.000	1.000	1.000
FGLS	BIC	1.000	1.000	1.000	1.000
FGLS-D	BIC	0.123	0.129	1.000	1.000
DURBIN	BIC	0.048	0.050	0.050	0.050
DURBIN	AIC	0.048	0.049	0.050	0.050
Hausman 1	OLS vs FGLS	1.000	1.000	0.999	0.465
Hausman 2					

Table 7: Empirical Size of Nominal 5% t-test of $H_0: \beta = 1$ DGPs: (1) Triangular VAR, NDY + GEXOG, (2) Unrestricted VAR, NDY + EBD

		T=50)			
Test	Truncation	$\rho = 0$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$
OLS	_	0.785	0.162	0.441	0.504	0.406
NW	$h = \lceil 4(T/100)^{2/9} \rceil$	0.779	0.105	0.302	0.330	0.247
NW-A	$h = [0.75T^{1/3}]$	0.783	0.117	0.331	0.372	0.282
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	0.742	0.087	0.237	0.228	0.159
NW-KV	h = T	0.662	0.082	0.200	0.184	0.122
M-LLSW	$\nu = 4(T/100)^{2/9} $	0.687	0.075	0.194	0.170	0.124
FGLS	P = [I(I / 100)] BIC	0.775	0.077	0.097	0.113	0.121
FGLS-D	BIC	0.768	0.085	0.078	$0.110 \\ 0.124$	0.100
DURBIN	BIC	0.205	0.078	0.052	0.055	0.059
DURBIN	AIC	0.098	0.082	0.071	0.078	0.078
Hausman 1	OLS vs FGLS	0.782	0.624	0.583	0.491	0.332
Hausman 2	DURBIN vs FGLS-D	0.770	0.085	0.565	0.930	0.955
	Donibilit to Foldo D	T=20		0.000	0.000	0.000
Test	Truncation	$\rho = 0$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$
OLS	_	1.000	0.169	0.820	0.903	0.779
NW	$h = \lceil 4(T/100)^{2/9} \rceil$	1.000	0.081	0.656	0.738	0.516
NW-A	$h = [0.75T^{1/3}]$	1.000	0.081	0.656	0.738	0.516
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	0.999	0.063	0.560	0.620	0.352
NW-KV	h = T	0.979	0.058	0.421	0.447	0.248
M-LLSW	$\nu = 4(T/100)^{2/9} $	0.999	0.060	0.536	0.583	0.319
FGLS	P = [1(1/100)] BIC	1.000	0.053	0.066	0.415	0.683
FGLS-D	BIC	1.000	0.051	0.062	0.441	0.716
DURBIN	BIC	0.049	0.001 0.047	0.050	0.055	0.052
DURBIN	AIC	0.051	0.051	0.054	0.058	0.058
Hausman 1	OLS vs FGLS	0.714	0.443	0.827	0.899	0.665
Hausman 2	DURBIN vs FGLS-D	1.000	0.061	0.974	1.000	1.000
	Donibilit to Foldo D	T=60		0.011	11000	1.000
Test	Truncation	$\rho = 0$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$
OLS	_	1.000	0.174	0.995	0.999	0.989
NW	$h = \left[4(T/100)^{2/9}\right]$	1.000	0.075	0.971	0.991	0.928
NW-A	$I = [0, \pi \pi \pi 1/3]$	1.000	0.072	0.970	0.991	0.920
1 N V V - 1-1	$h = [0.75T^{1/3}]$	1.000		0.310	0.001	0.520
NW-LLSW		1.000	0.058	0.970 0.950	0.985	0.882
	$h = \lfloor 0.75T^{1/3} \rfloor$ $h = \lfloor 1.3T^{1/2} \rfloor$ $h = T$					
NW-LLSW	$ h = \lceil 1.3T^{1/2} \rceil $ h = T	$\begin{array}{c} 1.000 \\ 1.000 \end{array}$	0.058	0.950	$0.985 \\ 0.843$	0.882
NW-LLSW NW-KV	$h = \lceil 1.3T^{1/2} \rceil$	1.000	$\begin{array}{c} 0.058 \\ 0.050 \end{array}$	$\begin{array}{c} 0.950\\ 0.801 \end{array}$	0.985	$\begin{array}{c} 0.882\\ 0.646\end{array}$
NW-LLSW NW-KV M-LLSW	$h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$	$1.000 \\ 1.000 \\ 1.000$	$\begin{array}{c} 0.058 \\ 0.050 \\ 0.057 \end{array}$	$0.950 \\ 0.801 \\ 0.946$	$0.985 \\ 0.843 \\ 0.984$	$\begin{array}{c} 0.882 \\ 0.646 \\ 0.864 \end{array}$
NW-LLSW NW-KV M-LLSW FGLS	$h = \lceil 1.3T^{1/2} \rceil$ h = T $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC	$1.000 \\ 1.000 \\ 1.000 \\ 1.000$	$\begin{array}{c} 0.058 \\ 0.050 \\ 0.057 \\ 0.049 \end{array}$	$\begin{array}{c} 0.950 \\ 0.801 \\ 0.946 \\ 0.066 \end{array}$	$0.985 \\ 0.843 \\ 0.984 \\ 0.912$	$\begin{array}{c} 0.882 \\ 0.646 \\ 0.864 \\ 0.995 \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D	$h = \lceil 1.3T^{1/2} \rceil$ h = T $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC	1.000 1.000 1.000 1.000 1.000	$0.058 \\ 0.050 \\ 0.057 \\ 0.049 \\ 0.049$	$0.950 \\ 0.801 \\ 0.946 \\ 0.066 \\ 0.065$	$\begin{array}{c} 0.985 \\ 0.843 \\ 0.984 \\ 0.912 \\ 0.922 \end{array}$	$\begin{array}{c} 0.882 \\ 0.646 \\ 0.864 \\ 0.995 \\ 0.997 \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN	$h = \lceil 1.3T^{1/2} \rceil$ h = T $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC	$\begin{array}{c} 1.000 \\ 1.000 \\ 1.000 \\ 1.000 \\ 1.000 \\ 0.050 \end{array}$	$\begin{array}{c} 0.058 \\ 0.050 \\ 0.057 \\ 0.049 \\ 0.049 \\ 0.047 \end{array}$	0.950 0.801 0.946 0.066 0.065 0.053	$\begin{array}{c} 0.985 \\ 0.843 \\ 0.984 \\ 0.912 \\ 0.922 \\ 0.050 \end{array}$	$\begin{array}{c} 0.882 \\ 0.646 \\ 0.864 \\ 0.995 \\ 0.997 \\ 0.050 \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN	$h = \lceil 1.3T^{1/2} \rceil$ h = T $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC	$\begin{array}{c} 1.000 \\ 1.000 \\ 1.000 \\ 1.000 \\ 1.000 \\ 0.050 \\ 0.051 \end{array}$	$\begin{array}{c} 0.058 \\ 0.050 \\ 0.057 \\ 0.049 \\ 0.049 \\ 0.047 \\ 0.048 \end{array}$	$\begin{array}{c} 0.950 \\ 0.801 \\ 0.946 \\ 0.066 \\ 0.065 \\ 0.053 \\ 0.055 \end{array}$	$\begin{array}{c} 0.985 \\ 0.843 \\ 0.984 \\ 0.912 \\ 0.922 \\ 0.050 \\ 0.050 \end{array}$	$\begin{array}{c} 0.882 \\ 0.646 \\ 0.864 \\ 0.995 \\ 0.997 \\ 0.050 \\ 0.050 \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1	$h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC OLS vs FGLS	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675 \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ 0.293\\ 0.053\\ \end{array}$	$\begin{array}{c} 0.950 \\ 0.801 \\ 0.946 \\ 0.066 \\ 0.065 \\ 0.053 \\ 0.055 \\ 0.997 \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ 0.050\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.882 \\ 0.646 \\ 0.864 \\ 0.995 \\ 0.997 \\ 0.050 \\ 0.050 \\ 0.990 \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2	$h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC OLS vs FGLS	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ 0.675\\ 1.000\\ \textbf{T=250}\\ \rho=0 \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ 0.293\\ 0.053\\ \hline \textbf{00}\\ \hline \rho=0.5 \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ 0.997\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ 0.050\\ \hline 1.000\\ 1.000\\ \hline \rho = 0.9 \end{array}$	$\begin{array}{c} 0.882 \\ 0.646 \\ 0.864 \\ 0.995 \\ 0.997 \\ 0.050 \\ 0.050 \\ 0.990 \\ 1.000 \\ \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2	$\begin{split} h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ $	1.000 1.000 1.000 1.000 0.050 0.051 0.675 1.000 T=250	0.058 0.050 0.057 0.049 0.049 0.047 0.048 0.293 0.053 00	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.065\\ 0.053\\ 0.055\\ 0.997\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ 0.050\\ 1.000\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.882 \\ 0.646 \\ 0.864 \\ 0.995 \\ 0.997 \\ 0.050 \\ 0.050 \\ 0.990 \\ 1.000 \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2	$h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation $-$ $h = \lceil 4(T/100)^{2/9} \rceil$	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \hline \mathbf{T=256}\\ \rho=0\\ 1.000\\ 1.000\\ \hline \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ 0.293\\ 0.053\\ \hline 0\\ \hline \rho=0.5\\ 0.173\\ 0.062\\ \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ 0.997\\ 1.000\\ \hline\\ \rho=0.7\\ 1.000\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ 0.050\\ \hline 1.000\\ 1.000\\ \hline \rho = 0.9 \end{array}$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ 0.050\\ \hline 0.990\\ 1.000\\ \hline \rho = 0.95\\ \hline 1.000\\ 1.000\\ \hline \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 Test OLS NW NW-A	$h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation $-$ $h = \lceil 4(T/100)^{2/9} \rceil$ $h = \lceil 0.75T^{1/3} \rceil$	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \hline \mathbf{T=256}\\ \rho=0\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ 0.293\\ 0.053\\ \hline \begin{array}{c} 0\\ 0\\ \hline \end{array}\\ \hline \begin{array}{c} \rho = 0.5\\ 0.173 \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.065\\ 0.053\\ 0.055\\ \hline 0.997\\ 1.000\\ \hline \rho = 0.7\\ 1.000 \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ 0.050\\ \hline 1.000\\ \hline 1.000\\ \hline \rho=0.9\\ \hline 1.000 \end{array}$	$\begin{array}{c} 0.882 \\ 0.646 \\ 0.864 \\ 0.995 \\ 0.997 \\ 0.050 \\ 0.050 \\ 0.990 \\ 1.000 \\ \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 Test OLS NW	$h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation $-$ $h = \lceil 4(T/100)^{2/9} \rceil$	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \hline \mathbf{T=256}\\ \rho=0\\ 1.000\\ 1.000\\ \hline \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ 0.293\\ 0.053\\ \hline 0\\ \hline \rho=0.5\\ 0.173\\ 0.062\\ \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ 0.997\\ 1.000\\ \hline\\ \rho=0.7\\ 1.000\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ \hline 0.050\\ \hline 1.000\\ \hline 1.000\\ \hline \rho=0.9\\ \hline 1.000\\ \hline 1.000\\ \hline \end{array}$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ 0.050\\ \hline 0.990\\ 1.000\\ \hline \rho = 0.95\\ \hline 1.000\\ 1.000\\ \hline \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 Test OLS NW NW-A	$\begin{split} h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ $	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \hline \mathbf{T=256}\\ \rho=0\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ \hline 0.293\\ 0.053\\ \hline 0\\ \hline \rho = 0.5\\ \hline 0.173\\ 0.062\\ 0.060\\ \hline \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ 0.997\\ 1.000\\ \hline\\ \rho=0.7\\ 1.000\\ 1.000\\ 1.000\\ \hline\end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ \hline 0.050\\ \hline 1.000\\ \hline 1.000\\ \hline .000\\ \hline 1.000\\ \hline 1.000\\ \hline 1.000\\ \hline 1.000\\ \hline \end{array}$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ \hline 0.050\\ \hline 0.990\\ 1.000\\ \hline 1.000\\ 1.000\\ 1.000\\ \hline \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 Test OLS NW NW-A NW-A NW-LLSW	$\begin{split} h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ $	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \hline \textbf{T=250}\\ \rho=0\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ \hline \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ \hline 0.293\\ 0.053\\ \hline 0\\ \hline \rho = 0.5\\ \hline 0.173\\ 0.062\\ 0.060\\ 0.053\\ \hline \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ 0.997\\ 1.000\\ \hline\\ \rho=0.7\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ \hline 0.050\\ \hline 1.000\\ \hline 0.000\\ \hline 0.000\\$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ \hline 0.990\\ 1.000\\ \hline \\ \rho = 0.95\\ \hline 1.000\\ 1.000\\ 1.000\\ 1.000\\ \hline \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 Test OLS NW NW-A NW-LLSW NW-KV	$\begin{split} h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \hline \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ $	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \hline \textbf{T=256}\\ \rho=0\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ \hline \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ 0.293\\ 0.053\\ \hline \\ \hline \rho = 0.5\\ 0.173\\ 0.062\\ 0.060\\ 0.053\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ 0.997\\ 1.000\\ \hline\\ \rho=0.7\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.997\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ \hline 0.050\\ \hline 1.000\\ \hline 1.000\\ \hline 1.000\\ \hline 1.000\\ \hline 1.000\\ \hline 1.000\\ \hline 0.998\\ \end{array}$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ \hline 0.990\\ 1.000\\ \hline 0.990\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.981\\ \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN Hausman 1 Hausman 2 Test OLS NW NW-A NW-LLSW NW-KV M-LLSW	$\begin{split} h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ $	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \hline \textbf{T=250}\\ \rho=0\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ \hline \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ \hline 0.293\\ 0.053\\ \hline \textbf{0}\\ \hline \boldsymbol{\rho}=0.5\\ 0.173\\ 0.062\\ 0.060\\ 0.053\\ 0.050\\ 0.053\\ \hline \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ 0.997\\ 1.000\\ \hline\\ \rho=0.7\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.997\\ 1.000\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ \hline 0.050\\ \hline 1.000\\ \hline 0.998\\ \hline 1.000\\ \hline \end{array}$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ \hline \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN Hausman 1 Hausman 2 Test OLS NW NW-A NW-LLSW NW-KV M-LLSW FGLS	$\begin{split} h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ $	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \mathbf{T=250}\\ \rho=0\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ \hline \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ \hline 0.293\\ 0.053\\ \hline \rho = 0.5\\ \hline 0.173\\ 0.062\\ 0.060\\ 0.053\\ 0.050\\ 0.053\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ \hline 0.997\\ 1.000\\ \hline \\ \rho=0.7\\ \hline 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.997\\ \hline 1.000\\ 0.056\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ \hline 0.050\\ \hline 1.000\\ \hline 0.998\\ \hline 1.000\\ \hline 1.000\\ \hline 1.000\\ \hline 0.908\\ \hline 0.908\\ \hline 0.900\\ \hline 0.900\\$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ \hline 0.990\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.981\\ 1.000\\ 1.000\\ 1.000\\ \hline 0.901\\ 0.001\\ \hline 0.000\\ \hline 0.001\\ \hline 0.000\\ $
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN Hausman 1 Hausman 2 Test OLS NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D	$h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC OLS vs FGLS DURBIN vs FGLS-D Truncation $-$ $h = \lceil 4(T/100)^{2/9} \rceil$ $h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \hline \textbf{T=250}\\ \hline \rho=0\\ 1.000\\ 1.$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ \hline 0.293\\ 0.053\\ \hline \rho=0.5\\ 0.173\\ 0.062\\ 0.053\\ 0.050\\ 0.053\\ 0.051\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ \hline 0.997\\ 1.000\\ \hline \rho=0.7\\ \hline 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.997\\ 1.000\\ 0.997\\ 1.000\\ 0.056\\ 0.053\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ \hline 0.050\\ \hline 1.000\\ \hline 0.998\\ \hline 1.000\\ \hline 1.000\\$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ \hline \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN Hausman 1 Hausman 2 Test OLS NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN	$h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC OLS vs FGLS DURBIN vs FGLS-D Truncation $-$ $h = \lceil 4(T/100)^{2/9} \rceil$ $h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ \hline 0.675\\ 1.000\\ \hline \textbf{T=250}\\ \hline \rho=0\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.049\\ \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ \hline 0.293\\ 0.053\\ \hline \rho=0.5\\ 0.173\\ 0.062\\ 0.053\\ 0.050\\ 0.053\\ 0.051\\ 0.051\\ 0.048\\ \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ \hline 0.997\\ 1.000\\ \hline 0.000\\ 1.000\\ 1.000\\ 1.000\\ 0.097\\ 1.000\\ 0.056\\ 0.053\\ 0.049\\ \end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ \hline 0.050\\ \hline 1.000\\ \hline 0.998\\ \hline 1.000\\ \hline 1.000\\ \hline 0.052\\ \end{array}$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ \hline \end{array}$
NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN Hausman 1 Hausman 2 Test OLS NW NW-A NW-LLSW NW-A NW-LLSW FGLS FGLS-D DURBIN DURBIN	$h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC OLS vs FGLS DURBIN vs FGLS-D Truncation $-$ $h = \lceil 4(T/100)^{2/9} \rceil$ $h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC	$\begin{array}{c} 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.050\\ 0.051\\ 0.675\\ 1.000\\ \textbf{T=250}\\ \rho=0\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.049\\ 0.049\\ 0.049\\ \end{array}$	$\begin{array}{c} 0.058\\ 0.050\\ 0.057\\ 0.049\\ 0.049\\ 0.047\\ 0.048\\ \hline 0.293\\ 0.053\\ \hline 0\\ \hline \rho = 0.5\\ 0.173\\ 0.062\\ 0.062\\ 0.062\\ 0.063\\ 0.053\\ 0.053\\ 0.051\\ 0.051\\ 0.051\\ 0.048\\ 0.049\\ \hline \end{array}$	$\begin{array}{c} 0.950\\ 0.801\\ 0.946\\ 0.066\\ 0.053\\ 0.055\\ 0.997\\ 1.000\\ \hline\\ \rho=0.7\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.097\\ 1.000\\ 0.056\\ 0.053\\ 0.049\\ 0.050\\ \hline\end{array}$	$\begin{array}{c} 0.985\\ 0.843\\ 0.984\\ 0.912\\ 0.922\\ 0.050\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.998\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.052\\ 0.052\\ 0.052\end{array}$	$\begin{array}{c} 0.882\\ 0.646\\ 0.864\\ 0.995\\ 0.997\\ 0.050\\ 0.050\\ 0.990\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 1.000\\ 0.981\\ 1.000\\ 1.000\\ 1.000\\ 0.051\\ 0.050\\ 0.050\\ 0.050\\ \end{array}$

Table 8: Empirical Size of Nominal 5% t-test of $H_0: \beta = 1$ DGP: Dynamic Regression, EBD

Table 7 contains results for the two VAR DGPs, NDY + GEXOG and NDY + EBD. In the NDY + GEXOG environment, OLS and FGLS are inconsistent, which produces large size distortions. In contrast, DURBIN and FGLS-D are consistent; they should outperform OLS and FGLS, and they do. DURBIN and FLGS-D should perform similarly, and they do. In the NDY + EBD environment, OLS, FGLS, and FGLS-D are inconsistent, and all have large size distortions. DURBIN, however, remains consistent and performs admirably.

Finally, Table 8 contains results for the dynamic regression DGP, *EBD*. In this environment DURBIN should perform well, and it does, whereas all other test sizes are distorted, except at or near the very special common-factor case of $\rho = 0.5$.

4.5.2 Power

Only tests that are correctly sized are of real interest, because only correctly-sized tests produce trustworthy and interpretable rejections. As we have shown, DURBIN satisfies that requirement, whereas OLS-HAC regression does not. One could simply stop there, but it is of interest to compare rejection frequencies in a few laboratory environments where the DGP is known. We do so in Figure 2 for three of our DGPs with T = 200 and various persistence parameters, comparing OLS-HAC (Kiefer-Vogelsang, LLSW), FGLS, and FGLS-D.

In the top row Figure 2 we show rejection frequencies for the autoregressive disturbances environment, NDY + BD. All estimators are consistent, and all tests have correct size when $\beta = 1$, i.e., when the true parameter equals its value under the null hypothesis. Moving away from the null however, it is clear that OLS-HAC power is inferior to that of DURBIN, because OLS is inefficient relative to DURBIN. Moreover, the inferior power performance of OLS-HAC increases with disturbance persistence (ρ), precisely because the relative inefficiency of OLS increases with persistence. Finally, DURBIN, FGLS and FGLS-D have virtually identical power curves.

In the middle row Figure 2 we show rejection frequencies for the triangular VAR case, NDY+GEXOG. OLS-HAC and FGLS are so badly mis-sized that it is not worth discussing them, whereas FGLS-D is asymptotically correctly sized but is still over-sized for T = 200. Only DURBIN is trustworthy. Moving from the middle-left to middle-right panel (higher persistence), the superiority of Durbin is amplified.

In the bottom row Figure 2 we show rejection frequencies for the unrestricted VAR case, NDY + EBD. FGLS-D fails even asymptotically, so it is not surprising that its finite-sample performance is much worse than in the middle-row triangular VAR NDY + GEXOG case. DURBIN, however, remains trustworthy. Moving from the bottom-left to bottom-right panel

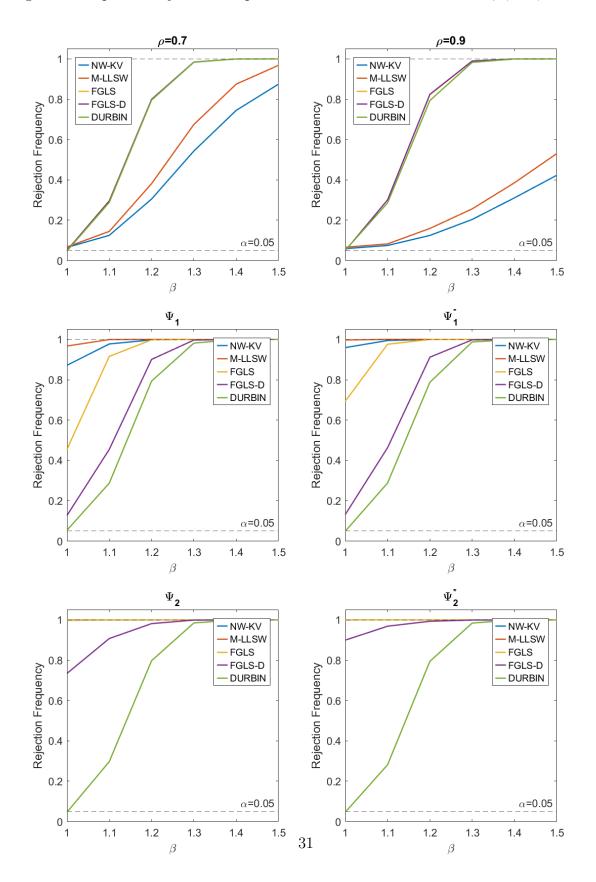


Figure 2: Empirical Rejection Frequencies of Nominal 5% t-Tests of H₀: $\beta = 1, T = 200$

Notes: DGPs: NDY + BD (top row), NDY + GEXOG (middle row), and NDY + EBD (bottom row). See text for details.

(higher persistence), the superiority of DURBIN is amplified, just as in the triangular case.

5 Concluding Remarks and Directions for Future Research

We have considered issues surrounding the time-series application of OLS regression with HAC standard errors. Although the OLS-HAC methodology is often sensible in cross-section regression situations, we argued that it is not generally an effective procedure in time-series regressions. Such regressions usually possess persistent autocorrelation, which causes OLS-HAC regressions to be highly sub-optimal for parameter estimation (in terms of efficiency), inference (in terms of both test size and power), and prediction.

We showed that the OLS-HAC problems are largely avoided by the use of a simple dynamic regression procedure, DURBIN. We demonstrated the significant advantages of DURBIN with detailed simulations covering a range of practical environments and issues. Effectively, DURBIN is a powerful tool for pre-whitened HAC estimation, in the tradition of Andrews and Monahan (1992) – indeed *such* a good pre-whitening tool that there's rarely any need for subsequent HAC estimation.

On the other hand, DURBIN is of course not a panacea. For example, DURBIN may struggle in small samples when dynamics have a strong moving-average component. Our Monte Carlo makes clear, however, that for all but the most extreme environments, DURBIN with lag order selected using standard information criteria performs consistently well. Indeed that is the key message of our paper.

In future work, one could generalize the DURBIN regression in various ways. For example, one could allow different lag lengths for y and the x_i 's. One could also allow for heteroskedasticity, which we suppressed in this paper so as to focus exclusively on autocorrelation, for example by allowing for *GARCH* disturbances in the DURBIN regression.

Appendices

A Additional Monte Carlo: AR Disturbances

T			$\rho = 0$	$\rho = 0.3$	$\rho = 0.5$	$\rho = 0.7$	$\rho = 0.9$	$\rho = 0.95$	$\rho = 0.99$
		FGLS BIC	1	1	1	1	1	1	1
	Median	DURBIN BIC	0	0	1	1	1	1	1
50		DURBIN AIC	0	1	1	1	1	1	1
30		FGLS BIC	1.2	1.2	1.3	1.2	1.3	1.3	1.5
	Mean	DURBIN BIC	0.1	0.4	0.9	1.1	1.1	1.1	1.1
		DURBIN AIC	2.0	2.5	2.9	3.0	3.0	3.1	3.1
		FGLS BIC	1	1	1	1	1	1	1
	Median	DURBIN BIC	0	1	1	1	1	1	1
200		DURBIN AIC	0	1	1	1	1	1	1
200		FGLS BIC	1.1	1.1	1.1	1.1	1.1	1.1	1.5
	Mean	DURBIN BIC	0.0	0.9	1.0	1.0	1.0	1.0	1.0
		DURBIN AIC	1.1	2.1	2.2	2.2	2.2	2.2	2.2
		FGLS BIC	1	1	1	1	1	1	1
	Median	DURBIN BIC	0	1	1	1	1	1	1
600		DURBIN AIC	0	1	1	1	1	1	1
000		FGLS BIC	1.0	1.0	1.0	1.0	1.0	1.0	1.5
	Mean	DURBIN BIC	0.0	1.0	1.0	1.0	1.0	1.0	1.0
		DURBIN AIC	0.7	1.8	1.7	1.7	1.8	1.8	1.7
		FGLS BIC	1	1	1	1	1	1	1
	Median	DURBIN BIC	0	1	1	1	1	1	1
2500		DURBIN AIC	0	1	1	1	1	1	1
2000		FGLS BIC	1.0	1.0	1.0	1.0	1.0	1.0	1.1
	Mean	DURBIN BIC	0.0	1.0	1.0	1.0	1.0	1.0	1.0
		DURBIN AIC	0.7	1.7	1.7	1.7	1.7	1.7	1.7

Table A1: Selected Lags by test Estimators: FGLS, DURBIN AIC, DURBIN BIC DGP: Autoregressive Disturbances, NDY + BD

B Additional Monte Carlo: MA Disturbances

T			$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
		FGLS	1	1	1	2	2	3	3
	Median	DURBIN BIC	0	0	1	1	2	2	2
50	50	DURBIN AIC	0	1	2	3	5	5	5
50		FGLS	1.3	1.3	1.6	2.2	2.9	3.0	3.1
	Mean	DURBIN BIC	0.1	0.3	0.8	1.4	1.9	2.0	2.0
		DURBIN AIC	2.0	2.6	3.4	4.2	5.2	5.6	5.6
		FGLS	1	1	2	3	5	5	5
	Median	DURBIN BIC	0	1	1	2	3	3	3
200		DURBIN AIC	0	1	2	4	8	9	10
200		FGLS	1.1	1.2	1.9	3.1	4.9	5.2	5.4
	Mean	DURBIN BIC	0.0	0.8	1.4	2.3	3.3	3.5	3.5
		DURBIN AIC	1.1	2.4	3.6	5.4	9.1	10.7	11.5
		FGLS	1	1	2	4	7	8	9
	Median	DURBIN BIC	0	1	2	3	5	6	6
600		DURBIN AIC	0	2	3	6	12	14	16
000		FGLS	1.0	1.4	2.5	4.3	7.6	8.5	8.9
	Mean	DURBIN BIC	0.0	1.1	2.1	3.4	5.4	5.9	6.1
		DURBIN AIC	0.7	2.4	3.8	6.2	12.3	15.2	17.0
		FGLS	1	2	3	6	12	15	17
	Median	DURBIN BIC	0	2	3	5	9	11	12
2500		DURBIN AIC	0	2	4	8	17	24	28
2000		FGLS	1.0	2.0	3.4	5.9	12.2	15.3	17.3
	Mean	DURBIN BIC	0.0	1.6	2.9	4.9	9.5	11.2	12.0
		DURBIN AIC	0.7	3.0	4.8	8.1	18.1	24.1	27.2

Table B1: Selected Lags by test Estimators: FGLS, DURBIN AIC, DURBIN BIC DGP: Moving Average Disturbances

Notes: The data-generating process is $y_t = x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = \theta \epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., T. All shocks are N(0, 1) white noise. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

Table B2: Bias, MSE, and Relative Efficiency	y
Estimators: OLS, FGLS, FGLS-D, DURBIN	ſ
DGP: Moving Average Disturbances	

			0.00	T=50	0 0 7	0.00	0.005	0.000
		$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
	OLS	0.0004	-0.0013	0.0008	0.0018	0.0024	-0.0002	-0.0034
Bias	FGLS	0.0004	-0.0010	0.0004	0.0018	0.0027	-0.0008	-0.0014
Dias	FGLS-D	0.0004	-0.0010	0.0013	0.0009	0.0028	-0.0022	-0.0022
	DURBIN	0.0004	-0.0002	0.0028	0.0011	0.0032	-0.0020	-0.0028
	OLS	0.0112	0.0165	0.0208	0.0279	0.0329	0.0344	0.0360
MSE	FGLS	0.0121	0.0167	0.0195	0.0224	0.0231	0.0237	0.0246
NIOL	FGLS-D	0.0114	0.0168	0.0203	0.0235	0.0248	0.0256	0.0267
	DURBIN	0.0131	0.0192	0.0237	0.0275	0.0314	0.0334	0.0350
	OLS	0.8570	0.8612	0.8795	1.0140	1.0485	1.0300	1.0288
RE_{est}	FGLS	0.9250	0.8730	0.8225	0.8167	0.7355	0.7084	0.7032
	FGLS-D	0.8668	0.8755	0.8573	0.8542	0.7900	0.7654	0.7638
				—				
		$\theta = 0$	$\theta = 0.3$	T=200 $\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
	OLS	-0.0008	-0.0005	-0.0005	$\frac{0 - 0.7}{0.0001}$	0 = 0.9 -0.0006	-0.0015	-0.0004
	FGLS	-0.0008	-0.0003	-0.0003 -0.0004	0.0001 0.0004	-0.0005	0.0015	-0.0004 -0.0004
Bias	FGLS-D	-0.0008	-0.0003 -0.0004	-0.0004 -0.0003	0.0004 0.0003	-0.0005 -0.0004	-0.0001	-0.0004 -0.0002
	DURBIN	-0.0008	-0.0004 0.0000	-0.0003	0.0003	-0.0004 -0.0005	0.0001	-0.0002
	OLS	0.0026	0.0000	0.0049	0.0000	0.0076	0.0083	0.0003
	FGLS	0.0026 0.0026	0.0039 0.0037	0.0049 0.0043	$0.0004 \\ 0.0044$	0.0078 0.0040	0.0083 0.0039	0.0088 0.0040
MSE	FGLS-D				$0.0044 \\ 0.0045$			
	DURBIN	0.0026	$0.0037 \\ 0.0050$	0.0043		0.0044	$0.0045 \\ 0.0063$	$0.0047 \\ 0.0066$
		0.0027		0.0053	0.0056	0.0061		
DE	OLS FGLS	0.9666	0.7802	0.9311	1.1610	1.2500	1.3162	1.3237
$\mathrm{RE}_{\mathrm{est}}$	FGLS-D	0.9824	$0.7383 \\ 0.7484$	0.8057	0.7966	$0.6489 \\ 0.7254$	0.6166	$0.6115 \\ 0.7102$
	FGL5-D	0.9673	0.7484	0.8185	0.8160	0.7234	0.7078	0.7102
				T=600				
		$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
	OLS	$\frac{\theta = 0}{0.0004}$	$\theta = 0.3$ 0.0001	$\frac{\theta = 0.5}{0.0003}$	$\theta = 0.7$ -0.0004	$\theta = 0.9$ 0.0005	$\theta = 0.95$ 0.0001	$\theta = 0.99$ -0.0011
Biog	OLS FGLS							
Bias		0.0004	0.0001	0.0003	-0.0004	0.0005	0.0001	-0.0011
Bias	FGLS	$0.0004 \\ 0.0004$	$0.0001 \\ 0.0000$	$0.0003 \\ 0.0006$	-0.0004 -0.0001	$0.0005 \\ 0.0002$	$0.0001 \\ 0.0005$	-0.0011 -0.0006
Bias	FGLS FGLS-D	$0.0004 \\ 0.0004 \\ 0.0004$	$\begin{array}{c} 0.0001 \\ 0.0000 \\ 0.0000 \end{array}$	$0.0003 \\ 0.0006 \\ 0.0005$	-0.0004 -0.0001 -0.0002	$0.0005 \\ 0.0002 \\ 0.0001$	$0.0001 \\ 0.0005 \\ 0.0005$	-0.0011 -0.0006 -0.0007
	FGLS FGLS-D DURBIN	$\begin{array}{c} 0.0004 \\ 0.0004 \\ 0.0004 \\ 0.0003 \end{array}$	$\begin{array}{c} 0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0001 \end{array}$	$\begin{array}{c} 0.0003 \\ 0.0006 \\ 0.0005 \\ 0.0007 \end{array}$	-0.0004 -0.0001 -0.0002 0.0000	$\begin{array}{c} 0.0005 \\ 0.0002 \\ 0.0001 \\ 0.0005 \end{array}$	$\begin{array}{c} 0.0001 \\ 0.0005 \\ 0.0005 \\ 0.0005 \end{array}$	-0.0011 -0.0006 -0.0007 -0.0015
Bias	FGLS FGLS-D DURBIN OLS	$\begin{array}{r} 0.0004 \\ 0.0004 \\ 0.0004 \\ 0.0003 \\ \hline 0.0009 \end{array}$	0.0001 0.0000 0.0000 0.0001 0.0013	$\begin{array}{r} 0.0003 \\ 0.0006 \\ 0.0005 \\ 0.0007 \\ 0.0017 \end{array}$	-0.0004 -0.0001 -0.0002 0.0000 0.0021	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ 0.0026\end{array}$	$\begin{array}{c} 0.0001 \\ 0.0005 \\ 0.0005 \\ 0.0005 \\ 0.0027 \end{array}$	-0.0011 -0.0006 -0.0007 -0.0015 0.0029
	FGLS FGLS-D DURBIN OLS FGLS	$\begin{array}{c} 0.0004 \\ 0.0004 \\ 0.0004 \\ 0.0003 \\ 0.0009 \\ 0.0009 \end{array}$	$\begin{array}{c} 0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ 0.0013 \\ 0.0012 \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ \end{array}$	-0.0004 -0.0001 -0.0002 0.0000 0.0021 0.0014	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ 0.0026\\ 0.0010\\ \end{array}$	$\begin{array}{c} 0.0001 \\ 0.0005 \\ 0.0005 \\ 0.0005 \\ 0.0027 \\ 0.0009 \end{array}$	-0.0011 -0.0006 -0.0007 -0.0015 0.0029 0.0009
	FGLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\end{array}$	$\begin{array}{c} 0.0001 \\ 0.0000 \\ 0.0000 \\ 0.0001 \\ 0.0013 \\ 0.0012 \\ 0.0012 \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ \end{array}$	-0.0004 -0.0001 -0.0002 0.0000 0.0021 0.0014 0.0014	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ 0.0026\\ 0.0010\\ 0.0012\\ \end{array}$	$\begin{array}{c} 0.0001 \\ 0.0005 \\ 0.0005 \\ 0.0005 \\ 0.0027 \\ 0.0009 \\ 0.0011 \end{array}$	-0.0011 -0.0006 -0.0007 -0.0015 0.0029 0.0009 0.0011
	FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0003\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ \hline 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ \hline 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ \end{array}$	-0.0004 -0.0001 -0.0002 0.0000 0.0021 0.0014 0.0014 0.0017	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ \end{array}$	-0.0011 -0.0006 -0.0007 -0.0015 0.0029 0.0009 0.0011 0.0020
MSE	FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS	0.0004 0.0004 0.0003 0.0009 0.0009 0.0009 0.0009 0.0009 0.0009 0.9762	0.0001 0.0000 0.0000 0.0001 0.0013 0.0012 0.0012 0.0017 0.7668	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ \hline 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ \hline 0.9680\\ \end{array}$	-0.0004 -0.0001 -0.0002 0.0000 0.0021 0.0014 0.0014 0.0017 1.2116	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ \hline 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ \end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588 \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS	0.0004 0.0004 0.0003 0.0009 0.0009 0.0009 0.0009 0.0009 0.9762 0.9805	0.0001 0.0000 0.0000 0.0001 0.0013 0.0012 0.0012 0.0017 0.7668 0.7113	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ \hline 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ \hline 0.9680\\ 0.7987\\ 0.8060\\ \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ \hline 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ \hline 1.2116\\ 0.7756\\ 0.7905\\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ 0.5660\\ \end{array}$	$\begin{array}{c} 0.0001 \\ 0.0005 \\ 0.0005 \\ 0.0005 \\ 0.0027 \\ 0.0009 \\ 0.0011 \\ 0.0019 \\ 1.4420 \\ 0.4812 \end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \end{array}$	0.0001 0.0000 0.0000 0.0001 0.0013 0.0012 0.0012 0.0017 0.7668 0.7113 0.7112	0.0003 0.0006 0.0005 0.0007 0.0017 0.0014 0.0014 0.0017 0.9680 0.7987 0.8060 T=2500	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ \hline 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ \hline 1.2116\\ 0.7756\\ 0.7905\\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ 0.5660\\ 0.6386\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ \hline 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ \hline 1.4420\\ 0.4812\\ 0.5750\\ \end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS FGLS-D	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ \hline 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ \hline 0.7668\\ 0.7113\\ 0.7112\\ \hline \theta=0.3 \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ \hline 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ \hline 0.9680\\ 0.7987\\ 0.8060\\ \hline \mathbf{T=2500}\\ \theta=0.5 \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ \hline 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ \hline 1.2116\\ 0.7756\\ 0.7905\\ \hline \theta=0.7 \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ 0.5660\\ 0.6386\\ \hline \\ \theta=0.9 \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ \hline 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ \hline 1.4420\\ 0.4812\\ 0.5750\\ \hline \theta = 0.95 \end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \theta = 0.99 \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \hline\\ \theta=0\\ 0.0001 \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ \hline 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ \hline 0.7668\\ 0.7113\\ 0.7112\\ \hline \\ \theta=0.3\\ \hline 0.0003\\ \hline \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ \hline 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ \hline 0.9680\\ 0.7987\\ 0.8060\\ \hline \mathbf{T=2500}\\ \theta=0.5\\ \hline 0.0000\\ \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \hline \theta=0.7\\ 0.0001\\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ 1.4440\\ 0.5660\\ 0.6386\\ \hline\\ \theta=0.9\\ -0.0001\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ \hline 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ \hline 1.4420\\ 0.4812\\ 0.5750\\ \hline \theta = 0.95\\ \hline 0.0002 \end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ 1.4588\\ 0.4708\\ 0.5733\\ \hline \theta=0.99\\ \hline 0.0004 \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D FGLS-D	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ 0.7668\\ 0.7113\\ 0.7112\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0003\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ 0.9680\\ 0.7987\\ 0.8060\\ \hline \mathbf{T=2500}\\ \theta=0.5\\ 0.0000\\ 0.0000\\ \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \hline\\ \theta=0.7\\ 0.0001\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ 0.5660\\ 0.6386\\ \hline \\ \theta = 0.9\\ \hline -0.0001\\ -0.0001\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ 0.4812\\ 0.5750\\ \hline\\ \theta=0.95\\ 0.0002\\ 0.0001\\ \hline\end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \theta = 0.99\\ \hline 0.0004\\ 0.0001\\ \hline \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D OLS FGLS FGLS FGLS	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ 0.7668\\ 0.7113\\ 0.7112\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0003\\ 0.0002\\ 0.0002\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ 0.9680\\ 0.7987\\ 0.8060\\ \hline \textbf{T=2500}\\ \theta=0.5\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ 0.5660\\ 0.6386\\ \hline \\ \theta = 0.9\\ \hline -0.0001\\ -0.0001\\ -0.0001\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ 0.4812\\ 0.5750\\ \hline\\ \theta = 0.95\\ 0.0002\\ 0.0001\\ 0.0002\\ \end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \theta = 0.99\\ \hline 0.0004\\ 0.0001\\ 0.0001\\ \hline 0.0001\\ \hline \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D OLS FGLS-D FGLS FGLS-D DURBIN	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ 0.7668\\ 0.7113\\ 0.7112\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0003\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ 0.9680\\ 0.7987\\ 0.8060\\ \hline \textbf{T=2500}\\ \theta=0.5\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \hline \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \hline\\ \theta=0.7\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0000\\ \hline\end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ 0.5660\\ 0.6386\\ \hline \\ \theta = 0.9\\ \hline -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ 0.4812\\ 0.5750\\ \hline\\ \theta = 0.95\\ 0.0002\\ 0.0001\\ 0.0002\\ 0.0003\\ \hline\end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \theta = 0.99\\ \hline 0.0004\\ 0.0001\\ 0.0001\\ 0.0001\\ \hline 0.0001\\ \hline 0.0001\\ \hline \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D OLS FGLS FGLS FGLS-D DURBIN OLS	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ 0.7668\\ 0.7113\\ 0.7112\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0003\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0003\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ 0.9680\\ 0.7987\\ 0.8060\\ \hline \textbf{T=2500}\\ \theta=0.5\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0004\\ \hline \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ 1.4440\\ 0.5660\\ 0.6386\\ \hline\\ \theta=0.9\\ -0.0001\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ 0.0006\\ \hline\end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ 0.4812\\ 0.5750\\ \hline\\ \theta = 0.95\\ 0.0002\\ 0.0001\\ 0.0002\\ 0.0003\\ 0.0007\\ \hline\end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \theta = 0.99\\ \hline 0.0004\\ 0.0001\\ 0.0001\\ \hline 0.0001\\ \hline 0.0007\\ \hline \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \hline \\ \theta=0\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ 0.7668\\ 0.7113\\ 0.7112\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0003\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ 0.9680\\ 0.7987\\ 0.8060\\ \hline \textbf{T=2500}\\ \theta=0.5\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0004\\ 0.0003\\ \hline \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ 1.4440\\ 0.5660\\ 0.6386\\ \hline\\ \theta=0.9\\ -0.0001\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ 0.0006\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ 0.4812\\ 0.5750\\ \hline\\ \theta = 0.95\\ 0.0002\\ 0.0001\\ 0.0002\\ 0.0003\\ 0.0007\\ 0.0002\\ \hline\end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \\ \theta = 0.99\\ \hline 0.0004\\ 0.0001\\ \hline \end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \hline \\ \theta=0\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ 0.7668\\ 0.7113\\ 0.7112\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0003\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ 0.0014\\ 0.0017\\ 0.9680\\ 0.7987\\ 0.8060\\ \hline \textbf{T=2500}\\ \theta=0.5\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0003\\ 0.0003\\ \hline \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \hline\\ \theta = 0.7\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0003\\ 0.0003\\ \hline\end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ 0.5660\\ 0.6386\\ \hline \\ \theta = 0.9\\ -0.0001\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ 0.0000\\ \hline 0.0000\\ 0.0002\\ 0.0002\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ 0.4812\\ 0.5750\\ \hline\\ \theta = 0.95\\ 0.0002\\ 0.0001\\ 0.0002\\ 0.0003\\ 0.0007\\ 0.0002\\ 0.$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \theta = 0.99\\ \hline 0.0004\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0002\\ \hline \end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D CLS FGLS FGLS-D DURBIN OLS FGLS FGLS FGLS	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ 0.7668\\ 0.7113\\ 0.7112\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0003\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0004\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ 0.9680\\ 0.7987\\ 0.8060\\ \hline \textbf{T=2500}\\ \theta=0.5\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0004\\ 0.0003\\ 0.0003\\ 0.0004\\ \hline \textbf{0.0004}\\ 0.0003\\ 0.0004\\ \hline \textbf{0.0004}\\ 0.0003\\ 0.0004\\ \hline \textbf{0.0004}\\ 0.0003\\ 0.0004\\ \hline \textbf{0.0004}\\ 0.0003\\ \hline \textbf{0.0004}\\ \hline \textbf{0.0004}\\ 0.0003\\ \hline \textbf{0.0004}\\ \hline \textbf$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \theta=0.7\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0000\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0004\\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ 0.5660\\ 0.6386\\ \hline \\ \theta = 0.9\\ -0.0001\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ 0.0000\\ \hline 0.0000\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ 0.4812\\ 0.5750\\ \hline\\ \theta = 0.95\\ 0.0002\\ 0.0001\\ 0.0002\\ 0.0003\\ 0.0007\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline\end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \\ \theta = 0.99\\ \hline 0.0004\\ 0.0001\\ 0.0001\\ \hline 0.0001\\ 0.0001\\ \hline 0.0007\\ 0.0001\\ \hline 0.0002\\ 0.0004\\ \hline \end{array}$
MSE RE _{est} Bias MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ 0.7668\\ 0.7113\\ 0.7112\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ 0.0014\\ 0.0017\\ 0.9680\\ 0.7987\\ 0.8060\\ \hline \textbf{T=2500}\\ \theta=0.5\\ 0.0000\\ 0.0004\\ 0.9920\\ \hline \end{array}$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \hline\\ \theta = 0.7\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0000\\ 0.0002\\ 0.0000\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0004\\ 1.2350\\ \hline\end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ 1.4440\\ 0.5660\\ 0.6386\\ \hline\\ \theta=0.9\\ -0.0001\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ 1.5383\\ \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ 0.4812\\ 0.5750\\ \hline\\ \theta = 0.95\\ 0.0002\\ 0.0001\\ 0.0002\\ 0.0001\\ 0.0002\\ 0.0003\\ 0.0007\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ 1.5773\\ \hline\end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \theta = 0.99\\ \hline 0.0004\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0002\\ 0.0004\\ \hline 1.5744\\ \hline \end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D CLS FGLS FGLS-D DURBIN OLS FGLS FGLS FGLS	$\begin{array}{c} 0.0004\\ 0.0004\\ 0.0004\\ 0.0003\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.0009\\ 0.9762\\ 0.9805\\ 0.9761\\ \hline \\ \theta=0\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0013\\ 0.0012\\ 0.0012\\ 0.0017\\ 0.7668\\ 0.7113\\ 0.7112\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0003\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0004\\ \end{array}$	$\begin{array}{c} 0.0003\\ 0.0006\\ 0.0005\\ 0.0007\\ 0.0017\\ 0.0014\\ 0.0014\\ 0.0017\\ 0.9680\\ 0.7987\\ 0.8060\\ \hline \textbf{T=2500}\\ \theta=0.5\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0004\\ 0.0003\\ 0.0003\\ 0.0004\\ \hline \textbf{0.0004}\\ 0.0003\\ 0.0004\\ \hline \textbf{0.0004}\\ 0.0003\\ 0.0004\\ \hline \textbf{0.0004}\\ 0.0003\\ 0.0004\\ \hline \textbf{0.0004}\\ 0.0003\\ \hline \textbf{0.0004}\\ \hline \textbf{0.0004}\\ 0.0003\\ \hline \textbf{0.0004}\\ \hline \textbf$	$\begin{array}{c} -0.0004\\ -0.0001\\ -0.0002\\ 0.0000\\ 0.0021\\ 0.0014\\ 0.0014\\ 0.0017\\ 1.2116\\ 0.7756\\ 0.7905\\ \theta=0.7\\ 0.0001\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0000\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0004\\ \end{array}$	$\begin{array}{c} 0.0005\\ 0.0002\\ 0.0001\\ 0.0005\\ \hline 0.0026\\ 0.0010\\ 0.0012\\ 0.0018\\ \hline 1.4440\\ 0.5660\\ 0.6386\\ \hline \\ \theta = 0.9\\ -0.0001\\ -0.0001\\ -0.0001\\ -0.0001\\ 0.0000\\ 0.0000\\ \hline 0.0000\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline \end{array}$	$\begin{array}{c} 0.0001\\ 0.0005\\ 0.0005\\ 0.0005\\ 0.0027\\ 0.0009\\ 0.0011\\ 0.0019\\ 1.4420\\ 0.4812\\ 0.5750\\ \hline\\ \theta = 0.95\\ 0.0002\\ 0.0001\\ 0.0002\\ 0.0003\\ 0.0007\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ \hline\end{array}$	$\begin{array}{c} -0.0011\\ -0.0006\\ -0.0007\\ -0.0015\\ \hline 0.0029\\ 0.0009\\ 0.0011\\ 0.0020\\ \hline 1.4588\\ 0.4708\\ 0.5733\\ \hline \\ \theta = 0.99\\ \hline 0.0004\\ 0.0001\\ 0.0001\\ \hline 0.0001\\ 0.0001\\ \hline 0.0007\\ 0.0001\\ \hline 0.0002\\ 0.0004\\ \hline \end{array}$

Notes: The data-generating process is $y_t = x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = \theta \epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., T. All shocks are N(0, 1) white noise. We select FGLS, FGLS-D, and DURBIN lag orders using BIC. RE_{est} denotes the relative estimation efficiency of DURBIN. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

			T=5	50				
	Truncation	$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
OLS	_	0.051	0.097	0.115	0.132	0.129	0.129	0.130
NW	$h = \lceil 4(T/100)^{2/9} \rceil$	0.066	0.082	0.085	0.094	0.092	0.088	0.093
NW-A	$h = [0.75T^{1/3}]$	0.064	0.084	0.088	0.097	0.096	0.093	0.095
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	0.064	0.074	0.080	0.083	0.082	0.082	0.086
NW-KV	h = T	0.061	0.073	0.077	0.079	0.075	0.075	0.076
M-LLSW	$\nu = 4(T/100)^{2/9} $	0.065	0.072	0.072	0.073	0.076	0.072	0.077
FGLS	P = [I(I / 100)] BIC	0.067	0.072	0.082	0.097	0.101	0.099	0.104
FGLS-D	BIC	0.054	0.092	0.002 0.095	0.093	0.092	0.092	0.094
DURBIN	BIC	0.060	0.092	0.094	0.075	0.002 0.075	0.072	0.078
DURBIN	AIC	0.086	0.096	0.087	0.080	0.085	0.085	0.088
Hausman 1	OLS vs FGLS	0.000	0.753	0.680	0.574	0.477	0.466	0.449
Hausman 2	DURBIN vs FGLS-D		0.133 0.047	0.030 0.073	0.088	0.097	0.400 0.099	0.445
Trausinan 2	DOUDIN VS FOLD-D		T=2		0.000	0.031	0.033	0.030
	Truncation	$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
OLS	_	0.050	0.090	0.110	0.132	0.123	0.133	0.134
NW	$h = \lceil 4(T/100)^{2/9} \rceil$	0.054	0.060	0.065	0.070	0.064	0.070	0.066
NW-A	$h = \lceil 0.75T^{1/3} \rceil$	0.054 0.054	0.060	0.065	0.070	0.064	0.070	0.066
NW-LLSW	$h = \lceil 0.131^{1/2} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$	0.054 0.053	0.050	0.005	0.070 0.059	0.054 0.056	0.066	0.060
NW-KV	$\begin{array}{c} n = 1.3I + \\ h = T \end{array}$	0.033 0.049	0.057 0.055	$0.055 \\ 0.056$	0.059 0.059	0.050 0.053	$0.000 \\ 0.057$	0.062
M-LLSW	$ \mu = 1 $ $ \nu = 4(T/100)^{2/9} $	$0.049 \\ 0.056$	$0.055 \\ 0.057$	0.050 0.056	0.059 0.059	0.053 0.053	0.057 0.062	
FGLS	$\mathcal{D} = \left[4(1/100)^{-7/6}\right]$ BIC	$0.050 \\ 0.052$	0.057 0.053	0.050 0.059	0.059 0.063	$0.055 \\ 0.056$	$0.062 \\ 0.057$	$0.061 \\ 0.059$
FGLS-D	BIC	0.050	0.059	0.057	0.061	0.053	0.055	0.056
DURBIN	BIC	0.052	0.062	0.050	0.051	0.055	0.055	0.055
DURBIN	AIC	0.067	0.053	0.054	0.056	0.059	0.063	0.058
Hausman 1	OLS vs FGLS		0.666	0.545	0.385	0.224	0.208	0.199
Hausman 2	DURBIN vs FGLS-D		0.049	0.055	0.059	0.059	0.064	0.060
	Truncation	$\theta = 0$	T=6 $\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
OLS	_	0.052	0.094	0.117	0.125	0.132	0.130	0.134
NW	$h = \lceil 4(T/100)^{2/9} \rceil$	0.052 0.054	0.054 0.057	0.063	0.066	0.060	0.060	0.066
	$h = \lceil 4(1/100)^{-7} \rceil$ $h = \lceil 0.75T^{1/3} \rceil$							
NW-A	$h = \begin{bmatrix} 0.751 \\ 7^{1/2} \end{bmatrix}$ $h = \begin{bmatrix} 1.3T^{1/2} \end{bmatrix}$	0.054	0.056	0.062	0.065	0.060	0.058	0.065
NW-LLSW		0.055	0.055	0.056	0.059	0.055	0.054	0.057
NW-KV	h = T	0.052	0.050	0.047	0.054	0.052	0.051	0.049
M-LLSW	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$	0.055	0.053	0.055	0.057	0.054	0.052	0.055
FGLS	BIC	0.053	0.047	0.058	0.053	0.047	0.040	0.043
FGLS-D	BIC	0.052	0.046	0.058	0.050	0.047	0.039	0.041
DURBIN	BIC	0.053	0.051	0.055	0.052	0.049	0.050	0.052
DURBIN	AIC	0.067	0.051	0.054	0.056	0.048	0.050	0.052
Hausman 1	OLS vs FGLS		0.588	0.421	0.242	0.101	0.095	0.088
Hausman 2	DURBIN vs FGLS-D		0.050	0.051	0.049	0.048	0.054	0.054
	T	0 0	T=25		0 07	0 0 0	0.05	0.00
OLS	Truncation	$\theta = 0$ 0.046	$\theta = 0.3$ 0.098	$\theta = 0.5$ 0.115	$\theta = 0.7$ 0.132	$\frac{\theta = 0.9}{0.133}$	$\theta = 0.95$ 0.131	$\frac{\theta = 0.99}{0.127}$
NW	$\stackrel{-}{h} = \lceil 4(T/100)^{2/9} \rceil$	$0.040 \\ 0.047$	0.098 0.057	$0.113 \\ 0.057$	$0.132 \\ 0.057$	$0.135 \\ 0.058$	$0.131 \\ 0.059$	0.127 0.056
	$n = [4(1/100)^{-7}]$ $h = [0.7571^{1/3}]$							
NW-A	$h = [0.75T^{1/3}]$	0.046	0.056	0.057	0.055	0.058	0.058	0.056
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	0.047	0.053	0.054	0.052	0.055	0.052	0.050
NW-KV	h = T	0.050	0.049	0.046	0.050	0.050	0.047	0.048
M-LLSW	$\nu = \lfloor 4(T/100)^{2/9} \rfloor$	0.046	0.055	0.053	0.051	0.054	0.051	0.050
FGLS	BIC	0.046	0.055	0.051	0.053	0.047	0.045	0.034
FGLS-D	BIC	0.046	0.053	0.051	0.053	0.044	0.039	0.035
DURBIN	BIC	0.046	0.049	0.050	0.050	0.048	0.051	0.050
DURBIN	AIC	0.058	0.049	0.050	0.049	0.049	0.051	0.048
Hausman 1	OLS vs FGLS		0.473	0.291	0.119	0.067	0.057	0.054
Hausman 2	DURBIN vs FGLS-D		0.052	0.050	0.052	0.053	0.050	0.053
Tradoman 2								

Table B3: Empirical Size of Nominal 5% t-test of $H_0: \beta = 1$ DGP: Moving Average Disturbances

Notes: The data-generating process is $y_t = x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = \theta \epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., T. All shocks are N(0, 1) white noise. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

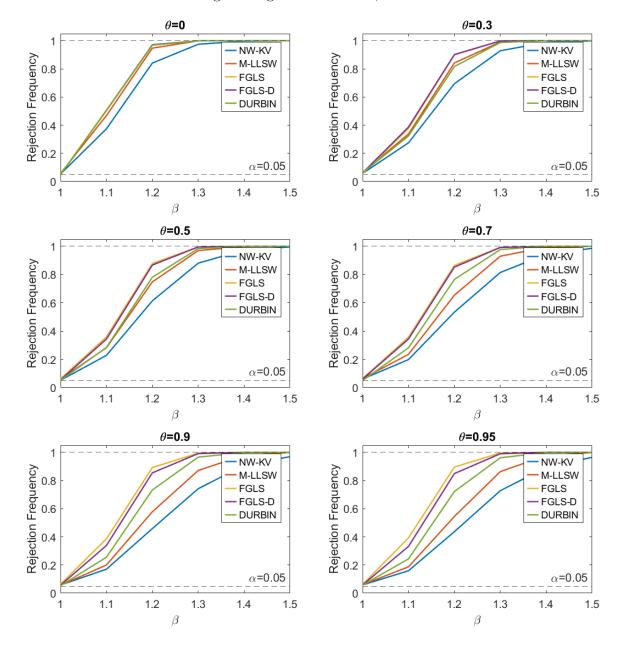


Figure B1: Empirical Rejection frequencies of Nominal 5% t-Test of H₀: β =1 DGP: Moving Average Disturbances, T = 200

Notes: The data-generating process is $y_t = \beta x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = \rho \epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., 200. All shocks are N(0, 1) white noise. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

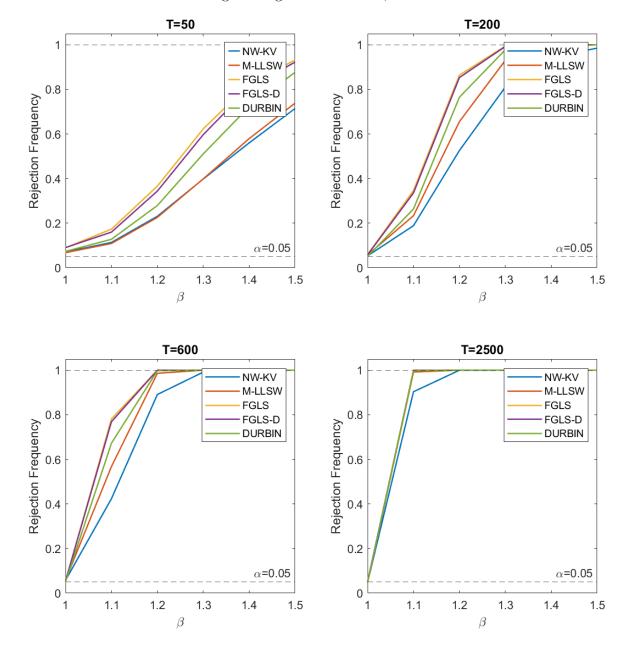


Figure B2: Empirical Rejection frequencies of Nominal 5% t-Test of H₀: β =1 DGP: Moving Average Disturbances, $\theta = 0.7$

Notes: The data-generating process is $y_t = \beta x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = 0.7\epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., T. All shocks are N(0, 1) white noise. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

C Additional Monte Carlo: ARMA Disturbances

T			$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
		FGLS	1	1	2	2	2	2	1
	Median	DURBIN BIC	1	1	2	2	2	3	3
50		DURBIN AIC	1	2	3	4	6	6	6
50		FGLS	1.2	1.6	2.1	2.6	2.9	2.7	2.0
Μ	Mean	DURBIN BIC	1.1	1.3	1.7	2.3	2.9	3.0	3.1
		DURBIN AIC	3.0	3.5	4.1	5.0	6.0	6.2	6.3
		FGLS	1	2	3	4	5	5	4
	Median	DURBIN BIC	1	2	2	3	4	4	4
200		DURBIN AIC	1	2	3	5	9	10	11
200		FGLS	1.1	2.0	2.6	3.7	4.9	4.9	3.9
	Mean	DURBIN BIC	1.0	1.6	2.3	3.1	4.2	4.4	4.5
		DURBIN AIC	2.2	3.4	4.4	6.3	10.2	11.6	12.5
		FGLS	1	2	3	5	7	8	7
	Median	DURBIN BIC	1	2	3	4	6	7	7
600		DURBIN AIC	1	3	4	6	12	15	17
000		FGLS	1.0	2.2	3.3	4.9	7.5	8.0	7.1
	Mean	DURBIN BIC	1.0	2.0	2.9	4.2	6.3	6.8	7.0
		DURBIN AIC	1.7	3.3	4.7	7.0	13.1	16.1	18.0
		FGLS	1	3	4	7	12	14	15
	Median	DURBIN BIC	1	2	4	6	10	12	13
2500		DURBIN AIC	1	3	5	8	18	25	28
2000		FGLS	1.0	2.8	4.2	6.7	12.3	14.6	14.9
	Mean	DURBIN BIC	1.0	2.3	3.7	5.8	10.3	12.0	13.0
		DURBIN AIC	1.7	3.8	5.6	8.9	18.9	24.7	27.5

Table C1: Selected Lags by test Estimators: FGLS, DURBIN AIC, DURBIN BIC DGP: ARMA Disturbances

Notes: The data-generating process is $y_t = x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = 0.7u_{t-1} + \theta\epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., T. All shocks are N(0, 1) white noise. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

Table C2: Bias, MSE, and Relative Efficiency
Estimators: OLS, FGLS, FGLS-D, DURBIN
DGP: ARMA Disturbances

				T=50				
		$\theta = 0$	$\theta = 0.3$	$\frac{1-30}{\theta=0.5}$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
	OLS	-0.0026	-0.0017	-0.0022	0.0006	0.0023	-0.0039	-0.0234
	FGLS	-0.0002	0.0009	0.0009	0.0018	0.0005	-0.0046	0.0023
Bias	FGLS-D	0.0001	0.0006	0.0008	0.0030	-0.0006	-0.0024	0.0021
	DURBIN	0.0003	0.0004	0.0002	0.0031	0.0001	-0.0053	0.0014
	OLS	0.0559	0.0945	0.1271	0.1698	0.3421	0.8138	15.4933
Mar	FGLS	0.0242	0.0250	0.0244	0.0232	0.0276	0.0358	0.1380
MSE	FGLS-D	0.0235	0.0231	0.0219	0.0198	0.0191	0.0199	0.0200
	DURBIN	0.0234	0.0245	0.0268	0.0292	0.0349	0.0369	0.0376
	OLS	2.3893	3.8547	4.7469	5.8198	9.8056	22.0441	411.8199
RE_{est}	FGLS	1.0369	1.0207	0.9108	0.7964	0.7900	0.9687	3.6672
	FGLS-D	1.0059	0.9441	0.8198	0.6778	0.5486	0.5383	0.5310
				T=200				
		$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
	OLS	0.0002	0.0016	-0.0029	-0.0022	-0.0004	-0.0032	-0.0024
Diag	FGLS	-0.0006	0.0009	-0.0010	-0.0007	-0.0001	-0.0003	-0.0005
Bias	FGLS-D	-0.0006	0.0008	-0.0009	-0.0003	0.0000	0.0001	-0.0004
	DURBIN	-0.0006	0.0007	-0.0008	-0.0004	-0.0006	0.0010	-0.0006
	OLS	0.0146	0.0238	0.0318	0.0420	0.0591	0.0932	1.0482
MSE	FGLS	0.0051	0.0048	0.0042	0.0034	0.0026	0.0029	0.0046
MSE	FGLS-D	0.0051	0.0048	0.0042	0.0034	0.0026	0.0027	0.0027
	DURBIN	0.0051	0.0052	0.0053	0.0057	0.0060	0.0066	0.0068
	OLS	2.8789	4.5810	5.9923	7.3801	9.7832	14.1853	155.2254
RE_{est}	FGLS	1.0071	0.9277	0.7980	0.5970	0.4372	0.4432	0.6771
	FGLS-D	1.0026	0.9303	0.7937	0.5921	0.4311	0.4053	0.3961
				T = 600				
		$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
	OLS	-0.0007	0.0007	$\theta = 0.5$ -0.0012	-0.0007	-0.0005	0.0004	-0.0019
Bias	FGLS	-0.0007 0.0007	$0.0007 \\ 0.0000$	$\theta = 0.5$ -0.0012 -0.0001	-0.0007 0.0001	-0.0005 0.0000	$0.0004 \\ 0.0003$	-0.0019 -0.0003
Bias	FGLS FGLS-D	-0.0007 0.0007 0.0007	$0.0007 \\ 0.0000 \\ 0.0000$	$\theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000$	-0.0007 0.0001 0.0002	-0.0005 0.0000 -0.0001	$0.0004 \\ 0.0003 \\ 0.0004$	-0.0019 -0.0003 -0.0003
Bias	FGLS FGLS-D DURBIN	-0.0007 0.0007 0.0007 0.0007	0.0007 0.0000 0.0000 -0.0001	$\theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002$	-0.0007 0.0001 0.0002 -0.0001	-0.0005 0.0000 -0.0001 0.0002	$\begin{array}{c} 0.0004 \\ 0.0003 \\ 0.0004 \\ 0.0007 \end{array}$	-0.0019 -0.0003 -0.0003 -0.0006
Bias	FGLS FGLS-D DURBIN OLS	-0.0007 0.0007 0.0007 0.0007 0.0007	0.0007 0.0000 0.0000 -0.0001 0.0082	$\theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106$	-0.0007 0.0001 0.0002 -0.0001 0.0135	-0.0005 0.0000 -0.0001 0.0002 0.0178	$\begin{array}{r} 0.0004 \\ 0.0003 \\ 0.0004 \\ 0.0007 \\ \hline 0.0227 \end{array}$	-0.0019 -0.0003 -0.0003 -0.0006 0.1273
	FGLS FGLS-D DURBIN OLS FGLS	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0049\\ 0.0016\end{array}$	0.0007 0.0000 0.0000 -0.0001 0.0082 0.0015	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ \hline 0.0106 \\ 0.0013 \end{array}$	-0.0007 0.0001 0.0002 -0.0001 0.0135 0.0009	-0.0005 0.0000 -0.0001 0.0002 0.0178 0.0006	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005 \end{array}$	$\begin{array}{r} -0.0019 \\ -0.0003 \\ -0.0003 \\ -0.0006 \\ 0.1273 \\ 0.0007 \end{array}$
Bias	FGLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0049\\ 0.0016\\ 0.0016\end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ \hline 0.0106 \\ 0.0013 \\ 0.0013 \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ \end{array}$	-0.0005 0.0000 -0.0001 0.0002 0.0178 0.0006 0.0006	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ \end{array}$	$\begin{array}{r} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\end{array}$
	FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0049\\ 0.0016\\ 0.0016\\ 0.0016\end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ -0.0001\\ \hline 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ \hline 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0017 \end{array}$	-0.0007 0.0001 0.0002 -0.0001 0.0135 0.0009 0.0010 0.0017	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ \hline 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0049\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\end{array}$	0.0007 0.0000 0.0000 -0.0001 0.0082 0.0015 0.0015 0.0017 4.8906	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ \hline 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ \hline 6.1570 \end{array}$	-0.0007 0.0001 0.0002 -0.0001 0.0135 0.0009 0.0010 0.0017 7.8409	-0.0005 0.0000 -0.0001 0.0002 0.0178 0.0006 0.0006 0.0006 0.0019 9.6024	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\end{array}$
	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0049\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ \end{array}$	0.0007 0.0000 -0.0001 0.0082 0.0015 0.0015 0.0017 4.8906 0.9163	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ \hline 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ \hline 6.1570 \\ 0.7628 \end{array}$	-0.0007 0.0001 0.0002 -0.0001 0.0135 0.0009 0.0010 0.0017 7.8409 0.5497	-0.0005 0.0000 -0.0001 0.0002 0.0178 0.0006 0.0006 0.0019 9.6024 0.3109	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ \hline 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ \hline 11.9589\\ 0.2779\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544 \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0049\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\end{array}$	0.0007 0.0000 0.0000 -0.0001 0.0082 0.0015 0.0015 0.0017 4.8906	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ \hline 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ \hline 6.1570 \end{array}$	-0.0007 0.0001 0.0002 -0.0001 0.0135 0.0009 0.0010 0.0017 7.8409	-0.0005 0.0000 -0.0001 0.0002 0.0178 0.0006 0.0006 0.0019 9.6024	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS	-0.0007 0.0007 0.0007 0.0007 0.0049 0.0016 0.0016 0.0016 2.9909 0.9998 0.9988	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ \hline 0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 4.8906\\ 0.9163\\ 0.9152\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \end{array}$	-0.0007 0.0001 0.0002 -0.0001 0.0135 0.0009 0.0010 0.0017 7.8409 0.5497 0.5623	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ \hline 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ \hline 9.6024\\ 0.3109\\ 0.3314\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ \hline 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ \hline 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ \hline 63.9303\\ 0.3544\\ 0.2746\\ \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0016\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9988\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ \hline 0.0001\\ \hline 0.0082\\ 0.0015\\ 0.0015\\ \hline 0.0017\\ \hline 4.8906\\ 0.9163\\ 0.9152\\ \hline \theta=0.3 \end{array}$	$\begin{array}{l} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ \hline 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ \hline 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \mathbf{T=2500} \\ \theta = 0.5 \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ \hline 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ \hline 7.8409\\ 0.5497\\ 0.5623\\ \hline \theta=0.7 \end{array}$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ \hline 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ \hline 9.6024\\ 0.3109\\ 0.3314\\ \hline \theta=0.9 \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ \hline 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ \hline 11.9589\\ 0.2779\\ 0.2911\\ \hline \theta=0.95 \end{array}$	$\begin{array}{c} -0.0019 \\ -0.0003 \\ -0.0003 \\ -0.0006 \\ \hline 0.1273 \\ 0.0007 \\ 0.0005 \\ 0.0020 \\ \hline 63.9303 \\ 0.3544 \\ 0.2746 \\ \hline \theta = 0.99 \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.00049\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ \hline 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 4.8906\\ 0.9163\\ 0.9152\\ \hline \\ \theta=0.3\\ \hline 0.0006\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 0.7628 \\ 0.7705 \\ \hline \mathbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \hline \theta=0.7\\ 0.0002\\ \end{array}$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ \hline 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \hline \\ \theta=0.9\\ -0.0005\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$ $\begin{array}{c} \theta = 0.95\\ -0.0003 \end{array}$	$\begin{array}{c} -0.0019 \\ -0.0003 \\ -0.0003 \\ -0.0006 \\ 0.1273 \\ 0.0007 \\ 0.0005 \\ 0.0020 \\ 63.9303 \\ 0.3544 \\ 0.2746 \\ \hline \\ \theta = 0.99 \\ 0.0020 \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D FGLS-D	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0049\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ -0.0003\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ 4.8906\\ 0.9163\\ 0.9152\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0006\\ 0.0003\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \mathbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \\ 0.0000 \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \hline \theta=0.7\\ 0.0002\\ 0.0002\\ 0.0002\\ \end{array}$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ 0.0178\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \\ \hline \theta = 0.9\\ -0.0005\\ 0.0001 \\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \hline\\ \theta=0.95\\ -0.0003\\ 0.0000\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544\\ 0.2746\\ \hline\\ \theta=0.99\\ 0.0020\\ 0.0000\\ \end{array}$
MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D OLS FGLS FGLS FGLS	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0049\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ -0.0003\\ -0.0003\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ 4.8906\\ 0.9163\\ 0.9152\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0006\\ 0.0003\\ 0.0003\\ 0.0003\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \textbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \\ 0.0000 \\ 0.0000 \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \hline\\ \theta=0.7\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ \end{array}$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$ $\begin{array}{c} \theta = 0.95\\ -0.0003\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544\\ 0.2746\\ \hline\\ \theta=0.99\\ 0.0020\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D OLS FGLS-D FGLS FGLS-D DURBIN	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.00049\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ -0.0003\\ -0.0003\\ -0.0003\\ -0.0003\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ 4.8906\\ 0.9163\\ 0.9152\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0006\\ 0.0003\\ 0.0003\\ 0.0004\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \textbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ \hline \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \hline\\ \theta=0.7\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ \end{array}$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$ $\begin{array}{c} \theta = 0.95\\ -0.0003\\ 0.0000\\ 0.0000\\ 0.0002\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544\\ 0.2746\\ \hline\\ \theta=0.99\\ 0.0020\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D OLS FGLS FGLS-D DURBIN OLS	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0049\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ -0.0003\\ -0.0003\\ -0.0003\\ 0.0011\\ \hline\end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ \hline 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ \hline 4.8906\\ 0.9163\\ 0.9152\\ \hline \\ \theta = 0.3\\ \hline 0.905\\ 0.0006\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0004\\ \hline 0.0019\\ \hline \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \textbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0026 \\ \hline \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \hline\\ \theta=0.7\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0001\\ 0.0033\\ \hline\end{array}$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$ $\begin{array}{c} \theta = 0.95\\ -0.0003\\ 0.0000\\ 0.0000\\ 0.0002\\ 0.0044\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544\\ 0.2746\\ \hline\\ \theta = 0.99\\ 0.0020\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ 0.0111\\ \end{array}$
MSE RE _{est}	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.00049\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ -0.0003\\ -0.0003\\ -0.0003\\ -0.0003\\ 0.0011\\ 0.0004\\ \end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ 4.8906\\ 0.9163\\ 0.9152\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \textbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \\ 0.0000 \\ 0.000$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \theta=0.7\\ 0.0022\\ 0.0002$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ 0.0178\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$ $\begin{array}{c} \theta = 0.95\\ -0.0003\\ 0.0000\\ 0.0000\\ 0.0002\\ 0.0004\\ 0.0001\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544\\ 0.2746\\ \hline\\ \theta = 0.99\\ 0.0020\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0001\\ \hline\end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ -0.0003\\ -0.0003\\ -0.0003\\ -0.0003\\ 0.0011\\ 0.0004\\ 0.0004\\ \hline\end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ 4.8906\\ 0.9163\\ 0.9152\\ \end{array}$ $\begin{array}{c} \theta = 0.3\\ 0.0006\\ 0.0003\\ 0.0003\\ 0.0003\\ 0.0004\\ 0.0019\\ 0.0004\\ 0.0004\\ 0.0004\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \textbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0003 \\ 0.0003 \\ \hline \textbf{0.0003} \\ \hline \textbf{0.0003} \\ \hline \textbf{0.0003} \\ \hline \textbf{0.0001} \\ \hline \textbf{0.0003} \\ \hline \textbf{0.00012} \\ \hline \textbf{0.0003} \\ \hline $	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \theta=0.7\\ 0.5623\\ \theta=0.7\\ 0.0002\\$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$ $\begin{array}{c} \theta = 0.95\\ -0.0003\\ 0.0000\\ 0.0000\\ 0.0002\\ 0.0004\\ 0.0001\\ 0.0001\\ 0.0001\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544\\ 0.2746\\ \hline\\ \theta = 0.99\\ 0.0020\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0001\\ \end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D CLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ -0.0003\\ -0.0003\\ -0.0003\\ -0.0003\\ 0.0011\\ 0.0004\\ 0.0004\\ 0.0004\\ 0.0004\\ \hline\end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ 4.8906\\ 0.9163\\ 0.9152\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \textbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0003 \\ 0.0003 \\ 0.0004 \\ \hline \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \theta=0.7\\ 0.5623\\ \theta=0.7\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ \end{array}$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$ $\begin{array}{c} \theta = 0.95\\ -0.0003\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ \hline 0.0044\\ 0.0001\\ 0.0004\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544\\ 0.2746\\ \hline\\ \theta = 0.99\\ 0.0020\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0001\\ 0.0004\\ \hline\end{array}$
MSE RE _{est} Bias MSE	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ -0.0003\\ -0.0003\\ -0.0003\\ -0.0003\\ 0.0011\\ 0.0004\\ 0.0004\\ 0.0004\\ 2.8997\\ \hline\end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ 4.8906\\ 0.9163\\ 0.9152\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \textbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0003 \\ 0.0004 \\ 6.4698 \\ \hline \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \theta=0.7\\ 0.5623\\ \theta=0.7\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ 7.9824\\ \end{array}$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$ $\begin{array}{c} \theta = 0.95\\ -0.0003\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ 0.0004\\ 0.0001\\ 0.0004\\ 10.4866\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544\\ 0.2746\\ \hline\\ \theta = 0.99\\ 0.0020\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0001\\ 0.0004\\ 25.2690\\ \hline\end{array}$
MSE RE _{est} Bias	FGLS FGLS-D DURBIN OLS FGLS-D DURBIN OLS FGLS-D CLS FGLS FGLS-D DURBIN OLS FGLS FGLS-D DURBIN	$\begin{array}{c} -0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0007\\ 0.0016\\ 0.0016\\ 0.0016\\ 2.9909\\ 0.9998\\ 0.9998\\ 0.9998\\ 0.9998\\ 0.9988\\ \hline\\ \theta=0\\ 0.0002\\ -0.0003\\ -0.0003\\ -0.0003\\ -0.0003\\ 0.0011\\ 0.0004\\ 0.0004\\ 0.0004\\ 0.0004\\ \hline\end{array}$	$\begin{array}{c} 0.0007\\ 0.0000\\ 0.0000\\ -0.0001\\ 0.0082\\ 0.0015\\ 0.0015\\ 0.0017\\ 4.8906\\ 0.9163\\ 0.9152\\ \end{array}$	$\begin{array}{c} \theta = 0.5 \\ -0.0012 \\ -0.0001 \\ 0.0000 \\ 0.0002 \\ 0.0106 \\ 0.0013 \\ 0.0013 \\ 0.0013 \\ 0.0017 \\ 6.1570 \\ 0.7628 \\ 0.7705 \\ \hline \textbf{T=2500} \\ \theta = 0.5 \\ 0.0004 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0000 \\ 0.0003 \\ 0.0003 \\ 0.0004 \\ \hline \end{array}$	$\begin{array}{c} -0.0007\\ 0.0001\\ 0.0002\\ -0.0001\\ 0.0135\\ 0.0009\\ 0.0010\\ 0.0017\\ 7.8409\\ 0.5497\\ 0.5623\\ \theta=0.7\\ 0.5623\\ \theta=0.7\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0002\\ 0.0004\\ \end{array}$	$\begin{array}{c} -0.0005\\ 0.0000\\ -0.0001\\ 0.0002\\ 0.0178\\ 0.0006\\ 0.0006\\ 0.0019\\ 9.6024\\ 0.3109\\ 0.3314\\ \end{array}$	$\begin{array}{c} 0.0004\\ 0.0003\\ 0.0004\\ 0.0007\\ 0.0227\\ 0.0005\\ 0.0006\\ 0.0019\\ 11.9589\\ 0.2779\\ 0.2911\\ \end{array}$ $\begin{array}{c} \theta = 0.95\\ -0.0003\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0002\\ \hline 0.0044\\ 0.0001\\ 0.0004\\ \end{array}$	$\begin{array}{c} -0.0019\\ -0.0003\\ -0.0003\\ -0.0006\\ 0.1273\\ 0.0007\\ 0.0005\\ 0.0020\\ 63.9303\\ 0.3544\\ 0.2746\\ \hline\\ \theta = 0.99\\ 0.0020\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0001\\ 0.0001\\ 0.0004\\ \hline\end{array}$

Notes: The data-generating process is $y_t = x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = 0.7u_{t-1} + \theta\epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., T. All shocks are N(0, 1) white noise. We select FGLS, FGLS-D, and DURBIN lag orders using BIC. RE_{est} denotes the relative estimation efficiency of DURBIN. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible.

			T=5	0				
	Truncation	$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
OLS	_	0.237	0.263	0.277	0.279	0.291	0.299	0.325
NW	$h = \left[4(T/100)^{2/9}\right]$	0.136	0.143	0.151	0.150	0.136	0.119	0.045
NW-A	$h = [0.75T^{1/3}]$	0.154	0.165	0.172	0.172	0.164	0.148	0.065
NW-LLSW	$h = [1.3T^{1/2}]$	0.103	0.107	0.109	0.111	0.090	0.071	0.021
NW-KV	h = T	0.088	0.096	0.097	0.093	0.073	0.052	0.013
M-LLSW	$\nu = 4(T/100)^{2/9} $	0.081	0.084	0.088	0.084	0.061	0.045	0.014
FGLS	BIC	0.076	0.084	0.086	0.081	0.081	0.081	0.104
FGLS-D	BIC	0.068	0.068	0.068	0.065	0.062	0.060	0.061
DURBIN	BIC	0.055	0.057	0.063	0.062	0.074	0.073	0.073
DURBIN	AIC	0.074	0.078	0.082	0.075	0.088	0.085	0.081
Hausman 1	OLS vs FGLS		0.312	0.250	0.213	0.164	0.120	0.038
Hausman 2	DURBIN vs FGLS-D		0.129	0.124	0.105	0.104	0.104	0.107
	DOUDIN (51 GLO D		T=20		0.100	0.101	0.101	0.101
	Truncation	$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
OLS	_	0.248	0.269	0.274	0.285	0.283	0.296	0.304
NW	$h = \lceil 4(T/100)^{2/9} \rceil$	0.106	0.105	0.112	0.114	0.102	0.101	0.042
NW-A	$h = \lceil 0.75T^{1/3} \rceil$	0.106	0.105	0.112	0.114	0.102	0.101	0.042
NW-LLSW	$h = \lceil 1.3T^{1/2} \rceil$	0.074	0.074	0.077	0.078	0.068	0.063	0.022
NW-KV	h = T	0.065	0.062	0.063	0.061	0.056	0.045	0.016
M-LLSW	$\nu = 4(T/100)^{2/9} $	0.066	0.066	0.068	0.067	0.053	0.045	0.017
FGLS	$\mathcal{D} = \left[4(1/100) \right]$ BIC	0.050	0.053	0.003 0.051	0.049	0.033	0.040	0.039
FGLS-D	BIC	0.051	0.055 0.051	0.048	0.045	0.037	0.040	0.039
DURBIN	BIC	0.031 0.049	0.048	0.040 0.050	0.045 0.056	0.051 0.052	0.040 0.056	0.055 0.055
DURBIN	AIC	0.049 0.053	0.048 0.053	0.055	0.050 0.057	0.052 0.058	0.060	0.061
Hausman 1	OLS vs FGLS	0.000	0.035	0.035	0.108	0.095	0.087	0.001
Hausman 2	DURBIN vs FGLS-D		0.140 0.076	0.125 0.052	0.108	0.033 0.063	0.060	0.054
mausinan 2	DOUDIN VS FOLD-D		T=60		0.000	0.005	0.000	0.000
	Truncation	$\theta = 0$	$\theta = 0.3$	$\theta = 0.5$	$\theta = 0.7$	$\theta = 0.9$	$\theta = 0.95$	$\theta = 0.99$
OLS	_	0.257	0.278	0.276	0.276	0.281	0.298	0.298
	$- h = \lceil 4(T/100)^{2/9} \rceil$				$0.276 \\ 0.087$	$0.281 \\ 0.089$	$0.298 \\ 0.091$	
NW	$ \begin{array}{c} - \\ h = \left\lceil 4(T/100)^{2/9} \right\rceil \\ h = \left\lceil 0.75T^{1/3} \right\rceil \end{array} $	0.086	0.090	0.088	0.087	0.089	0.091	0.052
NW NW-A	$ \begin{array}{c} -\\ h = \lceil 4(T/100)^{2/9} \rceil \\ h = \lceil 0.75T^{1/3} \rceil \\ h = \lceil 1.3T^{1/2} \rceil \end{array} $	$\begin{array}{c} 0.086 \\ 0.081 \end{array}$	$\begin{array}{c} 0.090 \\ 0.084 \end{array}$	$\begin{array}{c} 0.088\\ 0.083\end{array}$	$\begin{array}{c} 0.087 \\ 0.082 \end{array}$	$0.089 \\ 0.082$	$0.091 \\ 0.086$	$0.052 \\ 0.047$
NW NW-A NW-LLSW	$h = \begin{bmatrix} 0.75T^{1/3} \end{bmatrix}$ $h = \begin{bmatrix} 1.3T^{1/2} \end{bmatrix}$	$\begin{array}{c} 0.086 \\ 0.081 \\ 0.058 \end{array}$	$\begin{array}{c} 0.090 \\ 0.084 \\ 0.064 \end{array}$	$0.088 \\ 0.083 \\ 0.061$	$0.087 \\ 0.082 \\ 0.061$	$0.089 \\ 0.082 \\ 0.058$	$0.091 \\ 0.086 \\ 0.060$	$0.052 \\ 0.047 \\ 0.030$
NW NW-A NW-LLSW NW-KV	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$	$\begin{array}{c} 0.086 \\ 0.081 \\ 0.058 \\ 0.054 \end{array}$	$\begin{array}{c} 0.090 \\ 0.084 \\ 0.064 \\ 0.054 \end{array}$	$\begin{array}{c} 0.088 \\ 0.083 \\ 0.061 \\ 0.051 \end{array}$	$\begin{array}{c} 0.087 \\ 0.082 \\ 0.061 \\ 0.053 \end{array}$	$\begin{array}{c} 0.089 \\ 0.082 \\ 0.058 \\ 0.048 \end{array}$	$0.091 \\ 0.086 \\ 0.060 \\ 0.045$	0.052 0.047 0.030 0.019
NW NW-A NW-LLSW NW-KV M-LLSW	$h = \begin{bmatrix} 0.75T^{1/3} \\ h = \begin{bmatrix} 1.3T^{1/2} \end{bmatrix}$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$	0.086 0.081 0.058 0.054 0.054	0.090 0.084 0.064 0.054 0.058	0.088 0.083 0.061 0.051 0.056	0.087 0.082 0.061 0.053 0.058	$\begin{array}{c} 0.089 \\ 0.082 \\ 0.058 \\ 0.048 \\ 0.051 \end{array}$	0.091 0.086 0.060 0.045 0.047	0.052 0.047 0.030 0.019 0.020
NW NW-A NW-LLSW NW-KV M-LLSW FGLS	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ h = T $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC	$\begin{array}{c} 0.086 \\ 0.081 \\ 0.058 \\ 0.054 \\ 0.054 \\ 0.046 \end{array}$	$\begin{array}{c} 0.090 \\ 0.084 \\ 0.064 \\ 0.054 \\ 0.058 \\ 0.050 \end{array}$	$\begin{array}{c} 0.088 \\ 0.083 \\ 0.061 \\ 0.051 \\ 0.056 \\ 0.049 \end{array}$	$\begin{array}{c} 0.087 \\ 0.082 \\ 0.061 \\ 0.053 \\ 0.058 \\ 0.045 \end{array}$	$\begin{array}{c} 0.089 \\ 0.082 \\ 0.058 \\ 0.048 \\ 0.051 \\ 0.038 \end{array}$	0.091 0.086 0.060 0.045 0.047 0.033	$\begin{array}{c} 0.052 \\ 0.047 \\ 0.030 \\ 0.019 \\ 0.020 \\ 0.024 \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ h = T $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046 \end{array}$	$\begin{array}{c} 0.090 \\ 0.084 \\ 0.064 \\ 0.054 \\ 0.058 \\ 0.050 \\ 0.049 \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\end{array}$	$\begin{array}{c} 0.087 \\ 0.082 \\ 0.061 \\ 0.053 \\ 0.058 \\ 0.045 \\ 0.044 \end{array}$	$\begin{array}{c} 0.089 \\ 0.082 \\ 0.058 \\ 0.048 \\ 0.051 \\ 0.038 \\ 0.038 \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \end{array}$	$\begin{array}{c} 0.052 \\ 0.047 \\ 0.030 \\ 0.019 \\ 0.020 \\ 0.024 \\ 0.031 \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\end{array}$	$\begin{array}{c} 0.090 \\ 0.084 \\ 0.064 \\ 0.054 \\ 0.058 \\ 0.050 \\ 0.049 \\ 0.050 \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ \end{array}$	$\begin{array}{c} 0.089 \\ 0.082 \\ 0.058 \\ 0.048 \\ 0.051 \\ 0.038 \\ 0.038 \\ 0.050 \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \end{array}$	$\begin{array}{c} 0.052 \\ 0.047 \\ 0.030 \\ 0.019 \\ 0.020 \\ 0.024 \\ 0.031 \\ 0.053 \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046 \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.038\\ 0.050\\ 0.052\\ \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \end{array}$	$\begin{array}{c} 0.052 \\ 0.047 \\ 0.030 \\ 0.019 \\ 0.020 \\ 0.024 \\ 0.031 \\ 0.053 \\ 0.054 \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\end{array}$	$\begin{array}{c} 0.090 \\ 0.084 \\ 0.064 \\ 0.054 \\ 0.058 \\ 0.050 \\ 0.049 \\ 0.050 \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ \end{array}$	$\begin{array}{c} 0.089 \\ 0.082 \\ 0.058 \\ 0.048 \\ 0.051 \\ 0.038 \\ 0.038 \\ 0.050 \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline\end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC OLS vs FGLS	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ 0.049\\ 0.082\\ 0.050\\ \end{array}$	0.087 0.082 0.061 0.053 0.058 0.045 0.044 0.050 0.051 0.074	0.089 0.082 0.058 0.048 0.051 0.038 0.038 0.038 0.050 0.052 0.071	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ \hline 0.073 \end{array}$	$\begin{array}{c} 0.052 \\ 0.047 \\ 0.030 \\ 0.019 \\ 0.020 \\ 0.024 \\ 0.031 \\ 0.053 \\ 0.054 \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC OLS vs FGLS	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ 0.089\end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ 0.049\\ 0.082\\ 0.050\\ \end{array}$	0.087 0.082 0.061 0.053 0.058 0.045 0.044 0.050 0.051 0.074	0.089 0.082 0.058 0.048 0.051 0.038 0.038 0.038 0.050 0.052 0.071	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ \hline 0.073 \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline\end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1	$\begin{split} h &= \lceil 0.75T^{1/3} \rceil \\ h &= \lceil 1.3T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \\ \hline $	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \end{array}$	0.090 0.084 0.064 0.054 0.058 0.050 0.049 0.050 0.051 0.089 0.052 T=25	0.088 0.083 0.061 0.051 0.056 0.049 0.047 0.050 0.049 0.049 0.082 0.050 00	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ 0.074\\ 0.052\\ \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.038\\ 0.050\\ 0.052\\ 0.071\\ 0.054\\ \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ \hline 0.073 \\ 0.056 \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline 0.037\\ 0.058\\ \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation - $h = \lceil 4(T/100)^{2/9} \rceil$	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3 \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline \textbf{00}\\ \hline \boldsymbol{\theta}=0.5 \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ 0.074\\ 0.052\\ \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.038\\ 0.050\\ 0.052\\ \hline 0.071\\ 0.054\\ \hline \theta = 0.9 \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ \hline 0.073 \\ 0.056 \\ \hline \theta = 0.95 \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline 0.037\\ 0.058\\ \hline \theta = 0.99 \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation - $h = \lceil 4(T/100)^{2/9} \rceil$	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ \hline \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ \hline 0.049\\ \hline 0.082\\ 0.050\\ \hline \textbf{00}\\ \hline \boldsymbol{\theta}=0.5\\ \hline 0.284\\ \hline $	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ \hline 0.074\\ 0.052\\ \hline \theta = 0.7\\ 0.284\\ \hline 0.284$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.038\\ 0.050\\ 0.052\\ 0.071\\ 0.054\\ \hline \theta = 0.9\\ 0.282\\ 0.282\\ \hline \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ 0.073 \\ 0.056 \\ \hline \theta = 0.95 \\ 0.278 \\ 0.278 \\ 0.278 \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ 0.037\\ 0.058\\ \hline \theta = 0.99\\ 0.300\\ \hline \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2	$ \begin{split} h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4 (T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ h &= \lceil 4 (T/100)^{2/9} \rceil \\ h &= \lceil 0.75 T^{1/3} \rceil \end{split} $	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \hline \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ 0.067\\ \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline \textbf{00}\\ \hline \boldsymbol{\theta}=0.5\\ \hline 0.284\\ 0.076\\ \hline \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ 0.074\\ 0.052\\ \hline \theta = 0.7\\ 0.284\\ 0.072\\ \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.050\\ 0.052\\ 0.071\\ 0.054\\ \hline \theta = 0.9\\ 0.282\\ 0.074\\ \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.040 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ \hline 0.073 \\ 0.056 \\ \hline \theta = 0.95 \\ \hline 0.278 \\ 0.068 \\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline 0.037\\ 0.058\\ \hline \theta = 0.99\\ \hline 0.300\\ 0.057\\ \hline \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A	$h = \lceil 0.75T^{1/3} \rceil$ $h = \lceil 1.3T^{1/2} \rceil$ $h = T$ $\nu = \lfloor 4(T/100)^{2/9} \rfloor$ BIC BIC BIC BIC AIC OLS vs FGLS DURBIN vs FGLS-D Truncation - $h = \lceil 4(T/100)^{2/9} \rceil$	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \hline\\ \theta=0\\ 0.247\\ 0.067\\ 0.063\\ \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ 0.067\\ 0.064\\ 0.051\\ \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline \textbf{00}\\ \hline \boldsymbol{\theta}=0.5\\ \hline 0.284\\ 0.076\\ 0.071\\ \hline \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ 0.074\\ 0.052\\ \hline \theta = 0.7\\ 0.284\\ 0.072\\ 0.068\\ \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.038\\ 0.050\\ 0.052\\ 0.071\\ 0.054\\ \hline \theta = 0.9\\ 0.282\\ 0.074\\ 0.069\\ \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.040 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ \hline 0.073 \\ 0.056 \\ \hline \theta = 0.95 \\ \hline 0.278 \\ 0.068 \\ 0.064 \\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-A NW-LLSW	$\begin{split} h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4 (T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ h &= \lceil 4 (T/100)^{2/9} \rceil \\ h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \end{split}$	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \hline \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ 0.067\\ 0.064\\ 0.051\\ 0.050\\ \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline {\bf 00}\\ \hline {\bf 0}\\ \hline \hline {\bf 0}\\ \hline \hline {\bf 0}\\ \hline $	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ \hline 0.074\\ 0.052\\ \hline \theta = 0.7\\ \hline 0.284\\ 0.072\\ 0.068\\ 0.056\\ 0.052\\ \hline \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.050\\ 0.052\\ \hline 0.071\\ 0.054\\ \hline \theta = 0.9\\ \hline 0.282\\ 0.074\\ 0.069\\ 0.053\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.040 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ \hline \end{array} \\ \begin{array}{c} 0.073 \\ 0.056 \\ \hline \end{array} \\ \begin{array}{c} \theta = 0.95 \\ 0.278 \\ 0.068 \\ 0.064 \\ 0.050 \\ 0.045 \\ \end{array} \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline\\ \theta=0.99\\ \hline\\ \theta=0.99\\ \hline\\ 0.300\\ 0.057\\ 0.053\\ 0.043\\ 0.033\\ \hline\end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW	$\begin{split} h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4 (T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \\ \hline $	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \hline\\ \theta=0\\ 0.247\\ 0.067\\ 0.063\\ 0.051\\ \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ 0.067\\ 0.064\\ 0.051\\ 0.050\\ 0.049\\ \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline {\bf 00}\\ \hline {\bf \theta}=0.5\\ \hline 0.284\\ 0.076\\ 0.071\\ 0.056\\ \hline \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ \hline 0.074\\ 0.052\\ \hline \theta = 0.7\\ \hline 0.284\\ 0.072\\ 0.068\\ 0.056\\ \hline \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.038\\ 0.050\\ 0.052\\ \hline 0.071\\ 0.054\\ \hline \theta = 0.9\\ \hline 0.282\\ 0.074\\ 0.069\\ 0.053\\ \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ \hline \end{array} \\ \begin{array}{c} \theta = 0.95 \\ 0.278 \\ 0.068 \\ 0.064 \\ 0.050 \\ 0.045 \\ 0.045 \\ 0.045 \\ \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW FGLS	$\begin{split} h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4 (T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ $	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ 0.067\\ 0.064\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline {0}\\ \hline \theta = 0.5\\ 0.284\\ 0.076\\ 0.071\\ 0.056\\ 0.071\\ 0.056\\ 0.053\\ 0.054\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ 0.074\\ 0.052\\ \hline \theta = 0.7\\ 0.284\\ 0.072\\ 0.068\\ 0.056\\ 0.052\\ 0.053\\ \hline \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.050\\ 0.052\\ \hline 0.071\\ 0.054\\ \hline \theta = 0.9\\ 0.282\\ 0.074\\ 0.069\\ 0.053\\ 0.050\\ 0.052\\ 0.038\\ \hline \end{array}$	$\begin{array}{c} 0.091\\ 0.086\\ 0.060\\ 0.045\\ 0.047\\ 0.033\\ 0.034\\ 0.050\\ 0.049\\ \hline \theta = 0.95\\ 0.056\\ \hline \theta = 0.95\\ 0.278\\ 0.068\\ 0.064\\ 0.050\\ 0.045\\ 0.045\\ 0.029\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline 0.037\\ 0.058\\ \hline \theta = 0.99\\ 0.300\\ 0.057\\ 0.053\\ 0.043\\ 0.033\\ 0.029\\ 0.026\\ \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN DURBIN Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW	$\begin{split} h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4 (T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \\ \hline $	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ 0.067\\ 0.064\\ 0.051\\ 0.050\\ 0.049\\ \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline {0}\\ \hline \theta = 0.5\\ 0.284\\ 0.076\\ 0.071\\ 0.056\\ 0.053\\ 0.054\\ \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ \hline 0.074\\ 0.052\\ \hline \theta = 0.7\\ 0.284\\ 0.072\\ 0.068\\ 0.056\\ 0.052\\ 0.053\\ 0.047\\ \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.050\\ 0.052\\ \hline 0.071\\ 0.054\\ \hline \theta = 0.9\\ 0.282\\ 0.074\\ 0.069\\ 0.053\\ 0.050\\ 0.052\\ \hline \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ 0.073 \\ 0.056 \\ \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN Hausman 1 Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW FGLS FGLS-D DURBIN	$\begin{split} h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ $	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ 0.067\\ 0.064\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline \theta = 0.5\\ \hline \theta = 0.5\\ \hline 0.284\\ 0.076\\ 0.071\\ 0.056\\ 0.053\\ 0.054\\ 0.050\\ 0.049\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ \hline 0.074\\ 0.052\\ \hline \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.050\\ 0.052\\ \hline 0.071\\ 0.054\\ \hline \theta = 0.9\\ 0.282\\ 0.074\\ 0.069\\ 0.053\\ 0.050\\ 0.052\\ 0.038\\ 0.039\\ 0.048\\ \hline \end{array}$	$\begin{array}{c} 0.091\\ 0.086\\ 0.060\\ 0.045\\ 0.047\\ 0.033\\ 0.034\\ 0.050\\ 0.049\\ \hline 0.073\\ 0.056\\ \hline \theta = 0.95\\ \hline \theta = 0.95\\ 0.278\\ 0.068\\ 0.064\\ 0.050\\ 0.045\\ 0.045\\ 0.045\\ 0.045\\ 0.029\\ 0.033\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline 0.037\\ 0.058\\ \hline \theta = 0.99\\ \hline 0.300\\ 0.057\\ 0.053\\ 0.043\\ 0.033\\ 0.029\\ 0.026\\ 0.032\\ 0.051\\ \hline \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN Hausman 1 Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW FGLS FGLS-D DURBIN DURBIN	$\begin{split} h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ h &= \lceil 4(T/100)^{2/9} \rceil \\ h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{AIC} \end{split}$	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ 0.067\\ 0.064\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline \theta = 0.5\\ \hline \theta = 0.5\\ \hline 0.284\\ 0.076\\ 0.076\\ 0.071\\ 0.056\\ 0.053\\ 0.054\\ 0.050\\ 0.049\\ 0.051\\ 0.052\\ \hline \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ \hline 0.074\\ 0.052\\ \hline \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.050\\ 0.052\\ \hline 0.071\\ 0.054\\ \hline \theta = 0.9\\ 0.282\\ 0.074\\ 0.069\\ 0.053\\ 0.050\\ 0.052\\ 0.038\\ 0.039\\ 0.048\\ 0.049\\ \hline \end{array}$	$\begin{array}{c} 0.091 \\ 0.086 \\ 0.060 \\ 0.045 \\ 0.047 \\ 0.033 \\ 0.034 \\ 0.050 \\ 0.049 \\ 0.073 \\ 0.056 \\ \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline 0.037\\ 0.058\\ \hline \theta = 0.99\\ 0.300\\ 0.057\\ 0.053\\ 0.043\\ 0.033\\ 0.029\\ 0.026\\ 0.032\\ 0.051\\ 0.050\\ \hline \end{array}$
NW NW-A NW-LLSW NW-KV M-LLSW FGLS FGLS-D DURBIN Hausman 1 Hausman 1 Hausman 2 OLS NW NW-A NW-LLSW FGLS FGLS-D DURBIN	$\begin{split} h &= \lceil 0.75 T^{1/3} \rceil \\ h &= \lceil 1.3 T^{1/2} \rceil \\ h &= T \\ \nu &= \lfloor 4(T/100)^{2/9} \rfloor \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{BIC} \\ \text{OLS vs FGLS} \\ \text{DURBIN vs FGLS-D} \\ \hline \\ $	$\begin{array}{c} 0.086\\ 0.081\\ 0.058\\ 0.054\\ 0.054\\ 0.046\\ 0.046\\ 0.046\\ 0.047\\ \end{array}$	$\begin{array}{c} 0.090\\ 0.084\\ 0.064\\ 0.054\\ 0.058\\ 0.050\\ 0.049\\ 0.050\\ 0.051\\ \hline 0.089\\ 0.052\\ \hline \mathbf{T=25}\\ \theta=0.3\\ 0.273\\ 0.067\\ 0.064\\ 0.051\\ 0.050\\ 0.049\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.088\\ 0.083\\ 0.061\\ 0.051\\ 0.056\\ 0.049\\ 0.047\\ 0.050\\ 0.049\\ \hline 0.082\\ 0.050\\ \hline \theta = 0.5\\ \hline \theta = 0.5\\ \hline 0.284\\ 0.076\\ 0.071\\ 0.056\\ 0.053\\ 0.054\\ 0.050\\ 0.049\\ 0.051\\ \hline \end{array}$	$\begin{array}{c} 0.087\\ 0.082\\ 0.061\\ 0.053\\ 0.058\\ 0.045\\ 0.044\\ 0.050\\ 0.051\\ \hline 0.074\\ 0.052\\ \hline \end{array}$	$\begin{array}{c} 0.089\\ 0.082\\ 0.058\\ 0.048\\ 0.051\\ 0.038\\ 0.050\\ 0.052\\ \hline 0.071\\ 0.054\\ \hline \theta = 0.9\\ 0.282\\ 0.074\\ 0.069\\ 0.053\\ 0.050\\ 0.052\\ 0.038\\ 0.039\\ 0.048\\ \hline \end{array}$	$\begin{array}{c} 0.091\\ 0.086\\ 0.060\\ 0.045\\ 0.047\\ 0.033\\ 0.034\\ 0.050\\ 0.049\\ 0.073\\ 0.056\\ \hline \theta = 0.95\\ 0.278\\ 0.068\\ 0.068\\ 0.064\\ 0.050\\ 0.045\\ 0.045\\ 0.045\\ 0.045\\ 0.045\\ 0.045\\ 0.029\\ 0.033\\ 0.051\\ 0.050\\ \hline \end{array}$	$\begin{array}{c} 0.052\\ 0.047\\ 0.030\\ 0.019\\ 0.020\\ 0.024\\ 0.031\\ 0.053\\ 0.054\\ \hline 0.037\\ 0.058\\ \hline \theta = 0.99\\ \hline 0.300\\ 0.057\\ 0.053\\ 0.043\\ 0.033\\ 0.029\\ 0.026\\ 0.032\\ 0.051\\ \hline \end{array}$

Table C3: Empirical Size of Nominal 5% t-test of $H_0: \beta = 1$ DGP: ARMA Disturbances

Notes: The data-generating process is $y_t = x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = 0.7u_{t-1} + \theta\epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., T. All shocks are N(0, 1) white noise. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details. 41

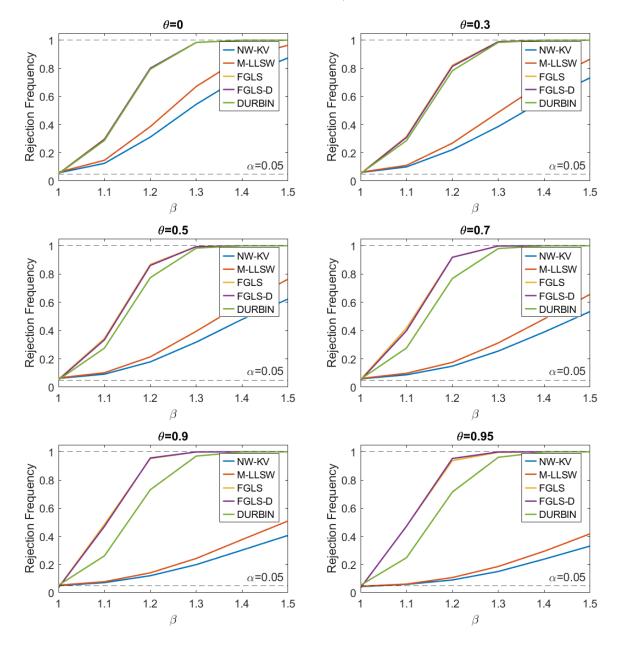


Figure C1: Empirical Rejection Frequencies of Nominal 5% t-Test of H₀: β =1, DGP: ARMA Disturbances, T = 200

Notes: The data-generating process is $y_t = \beta x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = 0.7u_{t-1} + \theta \epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., 200. All shocks are N(0, 1) white noise. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

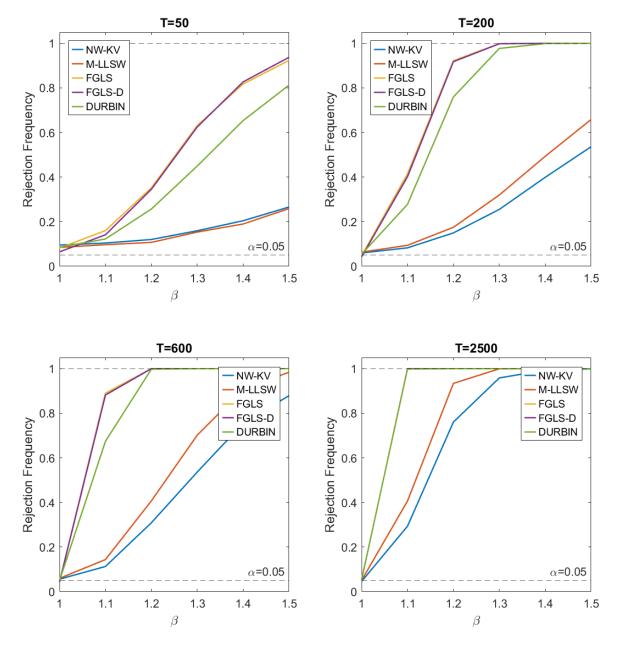


Figure C2: Empirical Rejection Frequencies of Nominal 5% t-Test of H₀: β =1, DGP: ARMA Disturbances, θ = 0.5

Notes: The data-generating process is $y_t = \beta x_t + u_t$, $x_t = 0.7x_{t-1} + \epsilon_{x,t}$, $u_t = 0.7u_{t-1} + 0.5\epsilon_{u,t-1} + \epsilon_{u,t}$, t = 1, ..., T. All shocks are N(0, 1) white noise. We perform 10000 Monte Carlo replications, drawing x_0 and u_0 from their stationary distributions and using common random numbers whenever possible. See text for details.

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