ORIGINAL RESEARCH



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Pyrolytic synthesis of graphene-encapsulated zero-valent iron nanoparticles supported on biochar for heavy metal removal

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Abstract

Biochar (BC)-supported graphene-encapsulated zero-valent iron nanoparticle composites (BC-G@Fe⁰) are promising engineering nanocomposites that can be used to scavenge heavy metal from wastewater. However, the production of BC-G@Fe⁰ through carbothermal reduction using biomass as a carbon source remains challenging because of biomass pyrolysis complications. Here, we examined two carbothermal reduction routes for preparing BC-G@Fe⁰ using bamboo as the carbon source. The first route impregnated Fe ions (Fe^{2+/3+}) into unpyrolyzed bamboo particles initially, followed by carbonization at 600–1000 °C. This process produced BC-G@Fe⁰ dominated by iron carbide (Fe₃C), which led to low heavy metal removal efficiency (i.e., Cu²⁺ capacity of < 0.3 mmol g⁻¹). In the second route, bamboo particles were pyrolyzed (600 °C) to biochar first, followed by impregnating this biochar with Fe ions, and then carbonized at 600–1000 °C. This route produces zero-valent iron nanoparticles, which resulted in high heavy metal removal capacities (i.e., 0.30, 1.58, and 1.91 mmol g⁻¹ for Pb²⁺, Cu²⁺, and Ag⁺, respectively). The effects of carbonization temperature (600–1000 °C), iron source (i.e., iron nitrates, iron sulfate, ferrous chloride, and ferric chloride), and iron loading (5–40%) on the morphology, structure, and heavy metal ion aqueous uptake performance of BC-G@ Fe⁰ were also investigated. This study revealed the formation mechanisms of BC-G@Fe⁰ through biomass carbothermal removal capacities for water remediation.

Highlights

- BC-G@Fe⁰ nanocomposite was produced through two carbothermal reduction routes.
- The biomass impregnating-carbonizing route produced graphene-encapsulated iron carbide (Fe $_3$ C) nanoparticles.

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- The pyrolyzing-biochar-impregnating-carbonizing route produced graphene-encapsulated nanoscale zerovalent iron particles.
- BC-G@Fe⁰ nanocomposites exhibited good heavy metal ion removal performance.

Keywords: Bamboo, Biochar, Carbothermal reduction, Fe₃C, Metallic iron, Heavy metal **Graphical Abstract**



1 Introduction

Heavy metal pollution is a global environmental issue that threatens 200 million people worldwide (Tchounwou et al. 2012). Heavy metals such as copper (Cu), lead (Pb), and silver (Ag) have devastating effects on humans (Wani et al. 2015). Cu^{2+} is a toxic heavy metal usually discharged from mining, farming, and corrosion of pipes (Briffa et al. 2020; Samaraweera et al. 2022). Pb²⁺ is the most toxic heavy metal originating from various sources such as leaded gasoline, water pipes, lead-based paint, battery recycling, etc. (Madduri et al. 2020). Ag⁺ is a rare metal that has adverse effects on human and aquatic life. The anthropogenic sources of Ag⁺ include emissions from smelting operations, cloud seeding, and photographic and electrical supplies (Eisler 1996).

Nanoscale zero-valent iron (nanoFe⁰) features a low reduction potential (E⁰) and high reactivity. It is a promising material for heavy metal immobilization from polluted water. Specifically, nanoFe⁰ can capture heavy metal ions such as Pb²⁺, Cu²⁺, and Ag⁺ with the E⁰ higher than - 0.44 eV by reduction, sequestering them as solid metal particles (Zhang et al. 2021b). Moreover, Fe^{2+/3+} ions released from nanoFe⁰ dissolution can immobilize heavy metals from wastewater solution through hydrolysis to iron hydroxide and co-precipitation (Zhang et al. 2021b). However, nanoFe⁰ suffers agglomeration issues because of its ferromagnetic high surface area. Agglomeration reduces the nanoFe⁰ surface area, which limits its mobility in polluted water, thereby reducing its water remediation performance (Huang et al. 2020; Jiao et al. 2019; Ng and Lim 2022). Depositing nanoFe⁰ onto a high surface area carrier can alleviate the agglomeration. Carriers including clay, zeolite, metal-organic frameworks, graphene, and biochar (BC) have been used for nanoFe⁰ dispersion (Asif et al. 2021; Bagheri et al. 2021; Ezzatahmadi et al. 2017; Florea et al. 2022; Li et al. 2018; Liu et al. 2019; Wang et al. 2019; Xing et al. 2020). BC is a low cost and effective candidate for dispersing nanoFe⁰ because of its highly porous high surface area structure and many surface functional groups (Wang et al. 2019). BC-supported nanoFe⁰ composite (BC-Fe⁰) has frequently been prepared by borohydride reduction of $Fe^{2+/3+}$ containing solutions (Yang et al. 2021). However, borohydrides are toxic and expensive, making large scale borohydride reduction a non-sustainable and less appealing BC-Fe⁰ preparation route.

Recently, carbothermal reduction has been used to produce BC-Fe⁰ for water remediation (Fan et al. 2020b; Jiang et al. 2021; Ma et al. 2021). Typical carbothermal reduction process impregnates iron salts or oxides into biomass precursors and heats at high temperatures (e.g., 600-800 °C) under oxygen-limited conditions. The biomass is converted to BC while iron salts or oxides are reduced to nanoFe⁰ particles, which attach to biochar surfaces (Zhang et al. 2022b). Generally, both solid carbon and released pyrolysis gases (CH₄, CO, H₂) are the main reagents causing reduction to Fe^0 (Yan et al. 2018c). However, this carbothermal reduction process is uncontrollable because of the complex biomass pyrolysis complexity. The structure, morphology, crystallinity and size of the reduced iron are hard to regulate. For instance, direct carbothermal reduction of Fe(NO₃)₃-impregnated rice straw at 800 °C produces BC-Fe⁰ dominated by nanoFe⁰ particles, while hydrothermally assisted carbothermal reduction yields BC with distributed nanoFe⁰, FeO, and Fe_2O_3 present (Yang et al. 2022). In contrast, the 800–1000 °C carbothermal reduction of ferric sulfate $[Fe_2(SO_4)_3]$ -impregnated rice husks yields Fe_2O_3 , Fe_3O_4 , and nanoFe⁰ species (Liu et al. 2020). Moreover, iron carbides (Fe₂C) generated in iron-assisted biomass pyrolysis products (Mun et al. 2015; Yan et al. 2018a; Zhang et al. 2018b), have often been overlooked or misinterpreted in the carbothermal production of BC-Fe⁰ (Chen et al. 2021; Liu et al. 2020; Neeli and Ramsurn 2018; Yang et al. 2022). Furthermore, the role of Fe_3C in water remediation is unclear. Studies have explored if Fe₃C facilitates aqueous nitrate reduction (Lan et al. 2020). Fe₃C is a stable compound that is not reactive to heavy metal water contaminants (Farzi et al. 2020). Additionally, the effect of the iron salts on the formation of BC-Fe⁰ is still unclear. For example, carbothermal reduction of iron nitrateimpregnated sawdust at 800 °C gave BC-Fe⁰ dominated by Fe₃C (Mun et al. 2015) while carbothermal reduction of FeCl₃-impregnated sawdust at the same temperature gave mainly nanoFe⁰ (Jiang et al. 2019).

Our previous studies revealed that graphitic carbon nanostructures usually formed during the carbothermal reduction of iron oxides/salts impregnated into biomass (Yan et al. 2018b). These nanostructures are composed of graphene nanosheets and nanoribbons that form on the surface of iron species (nanoFe⁰ and Fe₃C) via carbon dissolution into the iron, graphene sheet formation and precipitation (Hunter et al. 2022) mechanisms. Layers of graphene sheets can encapsulate the iron particles to varying thicknesses. Recently, we have reported good heavy metal and nutrient removal from wastewater using BC-supported graphene-encapsulated nanoFe⁰ (BC-G@Fe⁰) composites synthesized via in-situ carbothermal reduction of Fe(NO₃)₃ impregnated lignin (Zhang et al. 2021b). BC-G@Fe⁰ composites were produced by the in-situ carbothermal reduction of FeCl₃-impregnated sawdust and rice husk and used as persulfate activators for degrading 2,4-dichlorophenol (Zhang et al. 2021a) and acetaminophen (Zhuo et al. 2022), respectively. Biomass-derived BC-G@Fe⁰ composites have attracted wide research for treating wastewater, but its synthesis mechanism is still unclear because of the biomass chemical heterogeneity and pyrolysis complexity. The formation of both Fe₃C and graphitic nanostructures during iron catalytic graphitization of biomass is attributed to the carbonaceous compounds released during biomass pyrolysis. Thus, it remains a challenge to regulate the formation of Fe₃C nanoparticles and specific graphitic nanostructures during the BC-G@Fe⁰ production.

Considering these knowledge gaps, we sought to develop an effective BC-G@Fe⁰ composite by carbothermal reduction to remove heavy metals. Hence, two carbothermal reduction routes to generate BC-G@Fe⁰ were compared, i.e., the impregnating-carbonizing process and the pre-pyrolyzing-impregnating-carbonizing process (Fig. 1). The effects of the pre-pyrolyzing, carbonization temperature and iron source on the morphology, structure and heavy metal uptake performance of BC-G@Fe⁰ were investigated. Specifically, model heavy metal removals of BC-G@Fe⁰ were evaluated using aqueous Pb²⁺, Cu²⁺, and Ag⁺ solutions. This revealed features of the pyrolytic synthesis mechanism of biomass-derived BC-G@Fe⁰. This knowledge base could guide the application-oriented design of multifunctional iron-BC composites for water remediation.

2 Experiments

2.1 Materials

Bamboo biomass was collected from a local farm (Starkville, MS, USA). Iron(II) chloride tetrahydrate (FeCl₂·4H₂O), iron(III) chloride (FeCl₃), copper nitrate trihydrate [Cu(NO₃)₂·3H₂O], lead nitrate [Pb(NO₃)₂] and hydrochloric acid (HCl) were purchased from Sigma Aldrich. Iron(III) nitrate nonahydrate [Fe(NO₃)₃·9H₂O], and silver nitrate (AgNO₃) were purchased from Alfa Aesar. Iron(II) sulfate heptahydrate [FeSO₄·7H₂O] was purchased from Acros Organics.

2.2 BC preparation

Dried bamboo strips (7% moisture content) with skin removed were ground into powders using a wood miller with a 180 μ m mesh screen. Bamboo powders were pyrolyzed to BC in a tube furnace at 600 °C for 1 h



at a 50 °C min⁻¹ ramp rate under N₂ (1 L min⁻¹). After washing with 1 M HCl and distilled water to remove ash, BC was oven-dried at 100 °C overnight. The dried BC was then ground to fine particles using a pestle.

2.3 Preparation of BC-G@Fe⁰ by direct carbonization of Fe(NO₃)₃ impregnated bamboo particles (route I)

Prior to BC-G@Fe⁰ preparation, $Fe(NO_3)_3$ was mixed with bamboo particles through a solvent impregnation method. Briefly, 3.6 g $Fe(NO_3)_3 \cdot 9H_2O$ was mixed with 10 g bamboo (mass ratio of iron to the oven-dried bamboo is 5/100, labeled as 5%) in a beaker, followed by dispersing the mixture in 60 mL of deionized water. The mixture was then heated on a hot plate to ~ 60 °C while stirring for 2 h until all bamboo particles were saturated with the iron salt solution and had sank to the bottom of the beaker. Then this mixture was heated for another 2–6 h with stirring to evaporate the water, followed by oven drying at 103 °C overnight.

BC-G@Fe⁰ was prepared through direct carbonization of Fe(NO₃)₃-impregnated bamboo particles at seven different targeted temperature levels, i.e., 600, 650, 675, 700, 800, 900, and 1000 °C, respectively. Specifically, 10 g of Fe(NO₃)₃-impregnated bamboo particles was loaded in two ceramic boats that were placed in the heating zone of a 2-inch (outer diameter) electric tubular furnace, followed by ramping (50 °C min⁻¹) to a targeted temperature and holding for 1 h under a N₂ flow (1 L min⁻¹). After cooling the furnace to room temperature over 2 h, the sample was removed. The products from direct carbonization were labeled as BC-G@Fe⁰-DX, where "D" represents direct carbonization, and "X" represents the targeted carbonization temperature level used. The weights of products were measured using a digital balance (resolution 0.1 mg) giving the carbonization yield and allowing calculation of the iron content.

2.4 Preparation of BC-G@Fe⁰ by carbonization of Fe salt-impregnated BC (route II)

Prior to BC-G@Fe⁰ preparation, different iron salts were imbibed into BC (made at 600 °C, see Sect. 2.2) through a solvent impregnation method as described in Sect. 2.3. The type of iron salt used, $Fe(NO_3)_3$, $FeCl_2$, $FeCl_3$, and $FeSO_4$, to impregnate BC was investigated with an iron loading of 15%. The effect of the carbonization temperature (e.g., 600, 700, 800, 900, and 1000 °C) was studied using FeCl₂ to impregnate BC, employing a mass ratio of 15% iron to BC. Iron loading was evaluated using FeCl₂-impregnated BCs with iron loadings of 5%, 10%, 20%, 30%, and 40%.

BC-G@Fe⁰ was then prepared by carbonization of Feimpregnated BC particles at the predefined temperature using the same carbonization parameters (e.g., ramping rate and N2 flow rate) described in Sect. 2.3. The products were labeled as BC-G@Fe⁰-*X*, where "*X*" represents the carbonization temperature used. The product weights were measured, and the iron contents were calculated (shown in Additional file 1: Table S1).

2.5 Adsorption study

Batch sorption experiments determined the Pb^{2+} , Cu^{2+} , and Ag^+ aqueous removal efficiency of BC-G@Fe⁰

samples synthesized from routes I and II. Briefly, BC-G@ Fe^0 samples (50 mg) were dispersed in 40 mL solutions of the heavy metal at each concentration level evaluated. The mixtures were mechanically shaken vigorously for a predefined time at 25 °C. After completing metal uptake, the adsorbents were gravity filtered. The concentrations of Pb²⁺ and Cu²⁺ were determined by atomic absorption spectrophotometry (AAS). The Ag⁺ concentration was determined using inductively coupled plasma mass spectrometry (ICP-MS). Copper, lead, and silver standardized solutions were prepared in the ranges of 0.5–20 mg L⁻¹, 0.5–50 mg L⁻¹, and 0.5–5 mg L⁻¹, respectively. The uptake capacities of BC-G@Fe⁰ were calculated using Eq. 1:

$$\mathbf{Q} = (\mathbf{C}_0 - \mathbf{C}_f) \times \mathbf{V} / \mathbf{m},\tag{1}$$

where Q (mg g⁻¹) represents the metal amount (mg) adsorbed by 1 g of adsorbent; C_0 and C_f are the initial and final metal concentrations (mg L⁻¹) in the evaluated solution, respectively; V is the metal solution volume (L) and m is the adsorbent weight (g).

2.6 Characterization

X-ray diffraction (XRD) analysis was carried out to identify sample compositions using Cu-Ka radiation over the 2θ range of 20–80° with a Rigaku Ultima III X-ray diffractometer at a scanning speed of 1° min⁻¹ and step width of 0.05°. Field emission scanning electron microscopy (FESEM, JEOL-6500F) equipped with energy dispersive spectroscopy (EDS) was used to determine sample morphologies. BC-G@Fe⁰ samples were placed on a conductive carbon adhesive tab that adhere to a stub. Then a 15 nm thick layer of Pt was sputter-coated to make the sample conductive before SEM analysis. The spot diameter of the Fe⁰ nanoparticles in SEM images were calculated using ImageJ software. Transmission electron microscopy (TEM, JEOL-2100) equipped with EDS (Oxford X-max-80) was also used to investigate the surface morphology of BC-G@Fe⁰ samples. TEM specimens were prepared by mixing approximately 10 mg of BC-G@ Fe^0 samples with 5 mL ethanol first, followed by vortexing the suspension for 2 min. Then, a drop of the suspension was deposited onto a carbon film on a 300mesh copper grid that was allowed to stand overnight under a vacuum before TEM analysis. BC-G@Fe⁰ samples for specific surface area and pore volume measurements were degassed at 130 °C for 12 h before analyses by nitrogen sorption isotherms using a TriStar II PLUS (Micrometrics Instruments). The specific surface area, micropore and mesopore volumes were obtained according to N₂ adsorption isotherms using the nonlocal density functional theory (NLDFT) method by assuming a slit pore model (Zhang et al. 2022a).

The surface elemental composition of BC-G@Fe⁰ after heavy metal ion (Pb2+, Cu2+, and Ag+) removal tests were conducted using Thermo Scientific K-Alpha X-ray photoelectron spectroscopic system (XPS) equipped with a monochromatic X-ray source at 1486.6 eV (Al K α line). Briefly, 100 mg of BC-G@Fe⁰ were added to 50 mL of heavy metal ion solution, and the mixture was then shaken mechanically (at a speed of 200 rpm min^{-1}) for 15 min at 25 °C to characterize the surface region chemical structure of BC-G@Fe⁰ after the uptake of heavy metal ions. The initial solution concentration and the initial pH for each of three metal ions were 500 mg L^{-1} and 5, respectively. Following the removal tests, each mixture was first filtered, and the filtrate was then dried for 24 h at 80 °C under vacuum. the surface elemental composition of the dried filtrate swas then investigated using XPS, high-resolution Pb, Cu, and Ag spectra. These were deconvoluted by assigning various peak counts using the Gaussian function in OriginPro 2021 software.

3 Results and discussion

3.1 BC-G@Fe⁰ from direct carbonization of Fe(NO₃)₃ impregnated bamboo particles (route I)

The direct carbonization of iron nitrate-impregnated bamboo biomass particles yields iron-containing nanoparticles supported on bamboo-derived biochar. The decomposition of iron nitrates and biomass occurs at the temperature below 500 °C where iron oxides and carbonaceous gases compounds are produced (Eq. 2). Iron oxides conversion to metallic iron will occur at a temperature above 500 °C under a reducing environment (Crane and Scott 2012), i.e., upon exposure to carbon, CO, H_2 , or CH₄ formed from further biomass thermal degradation (Eq. 2). Meanwhile, the dissolution of carbon atoms into iron particles above 500 °C generates iron carbides (e.g., Fe₃C) (Eq. 3) (Liu et al. 2015). Both metallic iron and Fe₃C nanoparticles were observed in XRD patterns of evaluated BC-G@Fe⁰ (Fig. 2a). Specifically, a small amount of residual Fe₂O₃ was found at 600 °C, while it was almost fully reduced to Fe⁰ above 650 °C. At 675 °C, the carbon (002) peak was observed, indicating that the formation of graphitic carbon nanostructures probably was via the precipitation or extrusion of carbon from iron-carbon solid solutions (i.e., γ -Fe and Fe₃C) (Eqs. 4, 5) (Wirth et al. 2012). At 700 °C, diffraction intensities of both graphitic carbon and Fe₃C increased, indicating that the formation of graphitic nanostructures was exceeded by formation of Fe₃C. Further increasing the temperature from 700 to 1000 °C did not significantly change the phase composition of the products



Figure 2b showed the thermogravimetric analysis of iron nitrate-impregnated bamboo particles. Three main weight loss peaks were observed on the weight derivative curve. The first peak centered at 330 °C occurs with approximately a 50% mass loss, which corresponds to the thermal degradation of bamboo. The second peak centered at 580 °C was related to the reduction of Fe₂O₃ to Fe⁰ and Fe₃C nanoparticles. The third peak centered at 740 °C can be attributed to iron catalytic dehydrogenative BC carbonization and formation of graphene nanostructures. Iron-impregnated bamboo particles carbonized at 1000 °C exhibited a porous structure with many iron-based nanoparticles on their surfaces (Fig. 2c). TEM observations showed that these

iron-based nanoparticles with diameters less than 200 nm were embedded in an entangled graphitic nanoribbon and nanosphere network (Fig. 2d). High magnification TEM images indicated the iron-based (e.g., Fe₃C and Fe⁰) nanoparticles had a core–shell structure consisting mostly of an iron-based nanoparticle cores that were shelled (covered) with 5–10 nm thick graphene layered nanostructures (Fig. 2e). Fe₃C, which may be formed by carbon dissolving into α -Fe (Eq. 6), was also discovered in the outer layer of these nanoparticles (Fig. 2f). Thus, we postulated that nanoG@Fe⁰ from direct carbonization consisted of a tertiary structure with the outer graphene surrounding layered nanostructured shell. The middle layer was Fe₃C and

the core was nanoFe⁰ (Fig. 1), as previously reported (Yan et al. 2013, 2019). Equations (2)–(6) express the general reaction features of the entire process.

$$Fe_2O_3 + Carbon/CO/CH_4/H_2 \rightarrow Fe_3C + CO_2$$
 (3)

 $Fe_3C \rightarrow \gamma$ -Fe + Graphene (4)

 γ -Fe $\rightarrow \alpha$ -Fe + Graphene (5)

$$\alpha - Fe + Carbon \to Fe_3C \tag{6}$$

The surface area and pore size of directly carbonized BC-G@Fe⁰ samples were determined by N₂ adsorption isotherms (Fig. 2g). At 600 °C, the N₂ isotherms exhibited a typical Type Ia shape with an H4 hysteresis loop, indicating their microporous structure (Thommes et al. 2015). At 700 °C, N₂ isotherms showed the Type IVa shape with an H2 hysteresis loop, suggesting a developing mesoporous structure with some bottle-neck-shaped mesopores (Thommes et al. 2015). At temperatures of 700-1000 °C, the N2 isotherms of BC-G@Fe0 products showed the Type IVa shape with an H2 hysteresis loop, suggesting they all had bottle-neck-shaped mesoporous structures (Thommes et al. 2015). The microspore volume of BC-G@Fe⁰ samples, made from 600 to 1000 °C, decreased from 0.138 to 0.010 cm³ g⁻¹. As a result, the specific surface area dropped from 329.1 to 102.5 $m^2 g^{-1}$ (Fig. 2h). However, the mesopore volume rose from 0.010 to 0.248 cm³ g⁻¹. This microporous-to-mesoporous transaction with increasing temperature was related to the iron catalytic formation of graphene nanostructures. Specifically, the increase of temperature facilitated graphitic nanostructure (mainly mesoporous graphene nanoribbon and nanosphere) formation (Thompson et al. 2015) as indicated in XRD pattern (Fig. 2a). Moreover, the mobility of iron/iron carbide nanoparticles was increased at higher temperatures, this might also lead to reactive etching of microporous carbon and conversion of micropores to mesopore.

This BC-G@Fe⁰ obtained from route I was used for Cu^{2+} removal via batch adsorption tests, as shown in Fig. 2i. The Cu^{2+} removal by BC-G@Fe⁰ occurs mainly through a two-electron reduction reaction of Cu^{2+} to Cu (Eq. 7). The Cu^{2+} removal capacity is independent of the sample's surface area but dependent on the availability of the iron phases. As carbonization temperature rose from 600 to 700 °C, Cu^{2+} removal capacity (Q_{Cu}) increased from 0.14 to 0.27 mmol g⁻¹, despite 50% decrease of surface area. This took place because Fe₂O₃ was reduced to metallic iron nanoparticles, as illustrated in Fig. 2a.

More Fe⁰ enhanced Cu²⁺ removal by reducing more Cu²⁺ to Cu⁰ by Fe⁰ oxidation. Increasing the carbonization temperature from 700 to 1000 °C did not change the Cu²⁺ uptake capacity. This agrees with XRD scans showing BC-G@Fe⁰ produced between 700 and 1000 °C have similar iron phase compositions. Theoretically, 1 mol of the metallic zero-valent iron nanoparticle can uptake 1 mol of Cu²⁺ ions from an aqueous solution, and the corresponding uptake theoretical capacity (Q_{T-Cu}) is 17.86 mmol g⁻¹.

$$Fe(s) + Cu2+(aq) \rightarrow Fe2+ + Cu(s)$$
(7)

To evaluate the efficiency of direct carbonization of biomass/iron salt mixture (route I) for Fe⁰ production and its heavy metal removal efficiency, we proposed two new parameters, namely iron uptake capacity (Q_{Fe-Cu}) of Cu^{2+} and iron use ratio. Briefly, $Q_{\mbox{\scriptsize Fe-Cu}}$ is calculated by dividing the Q_{Cu} by its iron content, and Fe use ratio is calculated by Q_{Fe-Cu} divided by Q_{T-Cu}. The detailed calculation steps for Q_{T-Cu} , Q_{Fe-Cu} , and Fe use ratio were shown in Supporting information. As shown in Fig. 2i, as carbonization temperature rose from 600 to 700 °C, Q_{Fe-Cu} increased from 0.87 to 1.69 mmol g^{-1} and remained at ~1.65 mmol g^{-1} between 700 and 1000 °C. Similarly, the Fe use ratio increased from 4.9 to 9.4% as the temperature increased from 600 to 700 °C and remained at~9.4% thereafter. This low Fe use ratio was expected because Fe₃C nanoparticles were dominant in BC-G@ Fe^0 products produced by direct carbonization (Fig. 2a). Only small amounts of nanoFe⁰ were present in BC-G@ Fe⁰ that were tightly wrapped by both graphene layer and Fe_3C shells (Fig. 2a, e). Fe_3C did not reduce Cu^{2+} .

3.2 BC-G@Fe⁰ from carbonization of Fe-impregnated BC (route II)

3.2.1 Effect of iron catalyst type

Fe₃C lowered the Fe use ratio for Cu²⁺ uptake. To eliminate the formation of Fe₃C and increase the nanoFe⁰ production in the carbonization products, bamboo particles were initially pyrolyzed at 600 °C for 1 h to make BC and remove carbonaceous gases (e.g., CH₄, CO, etc.) in this first production stage without any $Fe^{2+/3+}$ impregnation. The bamboo-based BC particles produced were subsequently impregnated with iron salts and then further pyrolytically carbonized at 1000 °C to generate BC-G@ Fe⁰. As depicted in XRD analysis in Fig. 3a, this suppressed the formation of Fe₃C. These BC-G@Fe⁰ products contained mostly metallic iron nanoparticles (i.e., α -Fe and γ -Fe). Specifically, carbonizing FeCl₂ and FeCl₃ impregnated in bamboo, only after it was converted to BC at 600 °C, produced mostly α-Fe nanoparticles. Carbonizing $Fe(NO_3)_3$ impregnated BC yielded both α -Fe and γ -Fe nanoparticles. However, carbonizing FeSO₄



impregnated BC yielded α -Fe, γ -Fe, some Fe₃C nanoparticles, as well as Fe₂O₃ nanoparticles that were probably generated from the air passivation of α -Fe and/or γ -Fe nanoparticles. The furnace was cooled to room temperature before the product was exposed to O₂. Additionally, the carbon (002) diffraction peak was also observed in their XRD patterns (Fig. 3a).

Thermogravimetric analyses of bamboo BC are shown in Fig. 3b. Three main weight loss stages were observed. Briefly, the first stage occurred at temperatures of 50–250 °C and was related to loss of free bamboo moisture and decomposition of hydrated iron salts. The second stage occurring between 250 and 700 °C corresponded to the thermal degradation of iron salts. The third stage occurred above 700 °C and was attributed to the reduction of iron oxides and the formation of BC-G@ Fe⁰.

Surface area and pore-size characterizations of BC-G@ Fe⁰ performed by N₂ adsorption experiments are displayed in Additional file 1: Fig S1. The specific surface areas of BC-G@Fe⁰ samples made by route II were only between 2 and 20 m² g⁻¹. This was much lower than the BC-G@Fe⁰ samples produced from route I (i.e., 102.5-329.1 m² g⁻¹). Despite their low surface areas, Cu^{2+} uptake capacities (Q_{Cu}) of BC-G@Fe⁰ particles obtained from route II ranged from 0.57 to 1.01 mmol g^{-1} (Fig. 3c). This was significantly higher than that of BC-G@Fe⁰ samples obtained in route I (Fig. 2i), supporting our hypothesis that Fe₃C formed at the expense of Fe⁰ nanoparticles reduced heavy metal uptake. FeCl2-derived BC-G@Fe⁰ exhibited the highest Q_{Cu} of 1.00 mmol g⁻¹, followed by FeCl₃-derived BC-G@Fe⁰ (0.82 mmol g⁻¹), $FeSO_4$ -derived BC-G@Fe⁰ (0.73 mmol g⁻¹), and $Fe(NO_3)_3$ -derived BC-G@Fe⁰ (0.57 mmol g⁻¹).

To elucidate the reasons for the differences in Q_{Cu} , the morphologies of BC-G@Fe⁰ were obtained from route II using different iron salts. Uniform distribution of iron-based nanoparticles was formed on the surfaces of all samples (Fig. 3d-k). Importantly, the sizes of iron-based nanoparticles varied with the iron salts used. Specifically, Fe(NO₃)₃-derived BC-G@Fe⁰ exhibited the largest Fe-based nanoparticles with the average diameter of 439 nm (measured by ImageJ, as shown in Additional file 1: Fig. S3). These were followed by FeSO₄-derived BC-G@Fe⁰ (average diameter of 171 nm, Additional file 1: Fig. S3), FeCl₃-derived BC-G@Fe⁰ (average diameter of 135 nm, Additional file 1: Fig. S3), and FeCl₂-derived BC-G@Fe⁰ (average diameter of 97 nm, Additional file 1: Fig. S3). Generally, nanoFe⁰ particles with large sizes are less effective for heavy metal uptake because (1) heavy metal precipitates and (2) iron oxides formed on the surfaces. These increasingly prevent effective electron transfer from the nanoFe⁰ core to heavy metal ions. Thus, a larger fraction of Fe⁰ in the larger particles remains unoxidized. Thus, Fe(NO₃)₃-derived BC-G@Fe⁰ exhibits the lowest Q_{Cu} while FeCl₂-derived BC-G@Fe⁰ exhibits the highest Q_{Cu}. In comparison with FeCl₃-derived BC-G@Fe⁰, FeSO₄-derived BC-G@Fe⁰ contains more Fe₃C, causing a lower Q_{Cu} .

The morphology and structure of G@nanoFe⁰ particles in BC-G@Fe⁰ were studied by TEM (Fig. 3l-o). Individual particles display core-shell structures composed of metallic iron nanoparticle cores (nanoFe⁰, dark color portion) and a graphene nanoribbon shell (light color portion and labeled by red arrows). Note that the graphene nanoribbon encapsulations on nanoFe⁰ surfaces are not perfect and homogeneous, i.e., some surfaces have thick graphene nanoribbons. Graphene growth on iron surfaces is crystal-structure dependent (Liu et al. 2012; Vinogradov et al. 2017), i.e., the (100) iron plane is more favorable for graphene formation. Graphene nanoribbons prevent further aggregation of nanoFe⁰ particles by preventing direct Fe⁰/Fe⁰ contact. These shells also increase nanoFe⁰ particle stability by reducing their exposed surface area to other agents.

3.2.2 Effect of carbonization temperature

The effects of temperature and iron loading during the production of BC-G@Fe⁰ were studied by selecting FeCl₂ as the iron source and carbonizing different loadings at 600–1000 °C. Figure 4a shows the XRD patterns of FeCl₂ impregnated BC, which then was carbonized at 600–1000 °C for 1 h (route II). At 600 °C, FeCl₂ was partly converted to Fe₂O₃, but nanoFe⁰ was not formed. At 700 °C, FeO and α -Fe were formed due to the carbothermal reduction of Fe₂O₃, but FeCl₂ and Fe₂O₃ predominated. At 800 °C,

the α -Fe diffraction peak dominated in the XRD pattern, and two small peaks corresponding to graphite and γ -Fe diffractions were observed, suggesting graphene-encapsulated iron nanoparticles had formed. However, a small FeO diffraction was still visible, indicating the carbothermal reduction to Fe⁰ was not completed. At temperatures above 900 °C, carbonization product XRD patterns showed only α -Fe, γ -Fe, and graphite, completing the carbothermal reduction of iron oxides/chlorides. Moreover, higher γ -Fe and graphite diffraction intensities were observed in the BC-G@Fe⁰ produced at 1000 °C.

Q_{Cu} values exhibited significant increases from 0.02 to 0.98 mmol g⁻¹ upon increasing carbonization temperature from 700 to 1000 °C (Fig. 4b). The low Cu^{2+} uptake capacities at 600 and 700 °C resulted from the small amount of nanoFe⁰ formed. Carbonizing at 900 °C increased the Cu²⁺ uptake capacity from 0.02 to 0.44 mmol g^{-1} , because Fe^0 formation rose during the carbothermal reduction. Carbonization at 1000 °C doubled the Cu^{2+} uptake capacity (0.98 mmol g⁻¹), but the XRD patterns did not show many differences between these two samples. SEM characterization found (Fig. 4c, d), nanoparticle clusters were formed on the BC surfaces at 600 and 700 °C, which were nanoparticle clusters of iron oxides/chlorides confirmed by SEM-EDS mapping (Additional file 1: Figs. S4, S5). Higher temperatures promoted the decomposition and reduction of iron oxides/ chlorides to iron. The Fe/Cl and Fe/O element ratios rose. BC-G@Fe⁰ had a rough surface at 800 °C (Fig. 4e), attributed to etching of biochar from the carbothermal reduction. At 900 °C, nanoparticle clusters were observed on the surface of the BC (Fig. 4f). SEM-EDS mapping indicated the clusters consisted mostly of iron and carbon (Additional file 1: Fig. S6). At 1000 °C, micron-sized carbon/iron composite particles were observed in BC-G@ Fe⁰ (Fig. 4g and Additional file 1: Fig. S7, SEM-EDS mapping). The high-resolution TEM image (Fig. 4h) and EDS mapping (Fig. 4i) revealed nanoFe⁰ particles were encapsulated by graphitic carbon, which agree with the XRD results. We previously reported that graphitic carbon coatings protect the core nanoFe⁰ from oxygen passivation and enhances its heavy metal uptake efficiency (Zhang et al. 2021b). SEM-EDS revealed that oxygen was still present in carbon/iron composites synthesized at 900 °C and 1000 °C, suggesting surface oxidation of unprotected nanoFe⁰ particles occurred . Specifically, the iron to oxygen atomic ratio of the 900 °C-derived BC-G@Fe⁰ (Fe:O=0.9:1) was lower than those formed at 1000 °C (Fe:O = 1.5:1), implying nanoFe⁰ formed at 900 °C had a thinner protection layer and suffered more oxidation. This agrees with high intensity γ -Fe and graphitic XRD diffraction peaks of 1000 °C-derived BC-G@Fe⁰, confirming higher temperature facilitates the formation



of graphitic carbon encapsulations of iron nanoparticle (Zhang et al. 2018a).

3.2.3 Effect of iron loading

The effect of iron loading on the structure, morphology and Cu²⁺ uptake of BC-G@Fe⁰ samples obtained at 1000 °C, were investigated. All XRD patterns of BC-G@ Fe⁰ samples had α -Fe, γ -Fe, and graphite diffraction peaks (Fig. 5a). The Q_{Cu} of BC-G@Fe⁰ increased from 0.53 to 1.14 mmol g⁻¹ with the increase of iron loading from 5 to 40% (Fig. 5b). This confirms that nanoFe⁰ is responsible for the uptake of Cu²⁺. However, Q_{Fe-Cu} and the Fe use ratio values showed a decrease as the iron loading rose. In particular, the Fe use ratio decreased from 58 to 9% as iron loading went up from 5 to 40%. To investigate this, we characterized BC-G@Fe⁰ samples by SEM. NanoFe⁰ particles were well-dispersed on the BC surfaces at a 5%

iron loading (Fig. 5c). At a 10% loading, nanoFe⁰ clusters appeared because particle aggregation occurred. This aggregation became increasingly severe at higher loading (Fig. 5d–f), causing the Fe use ratio to drop at higher iron loadings.

3.3 Heavy metal removal study

BC-G@FE⁰ samples produced from FeCl₂-impregnated-BC carbonization (route II) with 15% iron loading at 1000 °C were used for the heavy metal ion removal study. The uptake of Pb²⁺ by BC-G@Fe⁰ was pH-dependent. The effect of solution pH was determined within the pH range of 1–7 (Fig. 6a). The uptake capacity of Pb²⁺ drastically increased from 0.006 to 0.17 mmol g⁻¹ as the solution pH increased from 1 to 3, while the capacity only slightly changed as the pH increased from 3 to 7. The removal of Pb²⁺ is minimized at low solution pH (i.e., pH 1 and 2) by



5% (c), 10% (d), 30% (e), and 40% (f) of Fe added as FeCl₂

the reaction between Fe⁰ and H⁺ resulting in oxidation of Fe⁰ to Fe²⁺ (Eq. 8). At pH 3–7, the Pb²⁺ removal is mainly attributed to the reduction of Pb²⁺ to Pb⁰ by Fe⁰ (Eq. 9).

$$Fe^{0}(s) + 2H^{+}(aq) \rightarrow Fe^{2+}(aq) + H_{2}(g)$$
 (8)

$$Fe^{0}(s) + Pb^{2+}(aq) \rightarrow Fe^{2+}(aq) + Pb^{0}(s)$$
 (9)

XPS confirmed the presence of Pb⁰ on the surface of BC-G@Fe⁰ after Pb²⁺ uptake (Fig. 6j). Additionally, the presence of Pb²⁺ on the surface of BC-G@Fe⁰ can be attributed to either the oxidation of reduced Pb⁰ nanoparticles or precipitation of Pb²⁺ compounds during Fe⁰ dissolution (Zhang et al. 2021b).

Kinetic and isotherm studies were carried out at the initial pH of 6. The Pb²⁺ removal rapidly increased in the first 15 min and reached equilibrium (Fig. 6b). The data were fitted to both pseudo-first-order (1st-order) and pseudo-second-order (2nd-order) models with R² values of 0.966 and 0.918 (Additional file 1: Table S2), respectively. The Langmuir (R²=0.711) and Freundlich (R²=0.929) models fitted to isotherm data favoring a multilayer model (Fig. 6c). The maximum Langmuir adsorption capacity was calculated to be 0.31 mmol g⁻¹.

The uptake of Cu^{2+} into BC-G@Fe⁰ is highly pH dependent like Pb²⁺. The effect of solution pH was

determined from pH 1–6 (Fig. 6d). The uptake capacity of Cu^{2+} dramatically increased from 0 to 1.04 mmol g⁻¹ as the solution pH increased from 1 to 3. The uptake capacity slightly differs as the pH increases from 3 to 6. Like Pb²⁺, Cu²⁺ removal is low at acidic pH (i.e., pH 1 and 2) by Eq. 1, At pH 3–7, the Cu²⁺ removal is mainly attributed to the reduction of Cu²⁺ to Cu⁰ by Fe⁰ (Eq. 7). XPS of BC-G@Fe⁰ after Cu²⁺ uptake confirms the reduction of Cu²⁺ to Cu⁰ (Fig. 6k). Moreover, Cu²⁺ is also observed on the surface of BC-G@Fe⁰, which can be attributed to the oxidation of reduced Cu⁰ and the precipitated Cu²⁺ compounds during Fe⁰ dissolving.

Kinetic and isotherm studies were carried out at the initial pH of 5. The Cu²⁺ uptake rapidly increased in the first 10 min, then slowly increased between 10 and 20 min, and finally reached equilibrium after 20 min. Over 90% of ultimate Cu²⁺ uptake was achieved within 5 min, showing the high removal kinetics of our BC-G@ Fe⁰ toward Cu²⁺. The data were fitted to both pseudo-first-order and pseudo-second-order models with R² values of 0.803 and 0.754, respectively (Fig. 6e). Figure 6f shows concertation-dependent Cu²⁺ removal by BC-G@Fe⁰. Adsorption isotherms were drawn to illustrate the relationship between Cu²⁺ concentration. The Langmuir (R²=0.984) and Freundlich (R²=0.904) models gave good fits to isotherm data (Additional file 1:



 $C_0 = 100 \text{ mg L}^{-1}$), **c** isotherms of Pb²⁺ uptake (pH 6, t = 15 min), **d** pH dependence of Cu²⁺ uptake ($C_0 = 100 \text{ mg L}^{-1}$, t = 1 h), **e** kinetics of Cu²⁺ uptake (pH 5, $C_0 = 100 \text{ mg L}^{-1}$), **f** isotherms of Cu²⁺ uptake (pH 5, t = 20 min), **g** pH dependence of Ag⁺ uptake ($C_0 = 200 \text{ mg L}^{-1}$, t = 1 h), **h** kinetics of Ag⁺ uptake (pH 5, $C_0 = 300 \text{ mg L}^{-1}$), **i** isotherms of Ag⁺ uptake (pH 5, t = 20 min). **j**-I XPS spectra of BC-G@Fe⁰ after Pb²⁺ (**j**), Cu²⁺ (**k**), and Ag⁺ (**l**) uptake (pH 5)

Table S2). The maximum Langmuir adsorption capacity is calculated to be 1.58 mmol g^{-1} .

The uptake of Ag^+ by BC-G@Fe⁰ is also pH-dependent. The effect of solution pH is determined within the pH range of 1–6 (Fig. 6g). The uptake capacity of Ag^+ increased from 0.851 to 1.345 mmol g⁻¹ as the solution pH increased from 1 to 3. The uptake capacity becomes almost a constant value as the pH increases from 3 to 6. Like Cu^{2+} and Pb^{2+} , Ag^+ removal is low at acidic pH (i.e., pH 1 and 2) by Eq. 1. At pH 3–6, the Ag^+ removal is mainly attributed to one electron reductions of two Ag^+ to Ag^0 by Fe^0 (Eq. 10).

$$Fe^{0}(s) + 2Ag^{+}(aq) \rightarrow Fe^{2+}(aq) + 2Ag^{0}(s)$$
 (10)

Table 1	Uptake	capacity	of	different	nanoscale	zero	-valent	iron	(nanoFe ⁰)	adsorbents	towards	Pb ²⁺ ,	Cu ²⁺	and	Ag+	in	aqueous
solutions	5																

Metal ion	Adsorbent	Method	Size of nanoFe ⁰	Sorption conditions	Fe content (%)	Uptake Capacity (mmol g ⁻¹)	lron uptake Capacity (mmol g ⁻¹)	References	
Pb ²⁺	Reed biochar supported nanoFe ⁰	ed biochar NaBH ₄ reduc- pported tion anoFe ⁰		Oxic 30 °C, pH 6.0±0.2	67	0.18	0.27	Zhu et al. (2017)	
	Hydrophilic biochar- nanoFe ⁰ from corn stalk	Acid ammo- nium persulfate oxidation	100–230 nm	Oxic 25 ± 1 ℃, pH 6.0	50	2.85	5.70	Li et al. (2020)	
	Lignin-based few-layered graphene- encapsulated iron nanopar- ticles	Carbothermal reduction	5–15 nm	Oxic 25 ℃, pH 6.0	14	0.62	4.43	Zhang et al. (2021b)	
	Shell biomass material sup- ported nanoFe ⁰	NaBH ₄ reduc- tion	60 nm	Oxic 30 °C, pH 6.0	21	0.45	2.14	Wang et al. (2020)	
	Exhausted coffee ground supported nanoFe ⁰	NaBH ₄ reduc- tion	<100 nm	Oxic 25 °C, pH 6.0	17	0.79	4.65	Park et al. (2019)	
	NanoFe ⁰ -mag- netic biochar composites	Reduction by honey	NA	Oxic 30 °C, pH 6.0	10	0.29	2.90	Rama Chand- raiah (2016)	
	Chitosan and NaBH ₄ redubiochar syner- gistically modi- fied sulfurized nanoFe ⁰		NA	Oxic 25 ℃	NA	1.38	NA	Xu et al. (2022)	
	BC-G@Fe ⁰	Carbothermal reduction	20–100 nm	Oxic 25 °C, pH 6.0	18	0.31	1.72	This study	
Cu ²⁺	Amino-mod- ified biochar supporting nanoFe ⁰	NA	~50 nm	Oxic 25 °С, pH 5.0–6.0	50	0.12	0.24	Yang et al. (2018)	
	Rubber seed shell supported nanoFe ⁰	NaBH ₄ reduc- tion	NA	Oxic 30 °C, pH 6.0	50	0.76	1.52	Prabu et al. (2017)	
	Reed biochar supported nanoFe ⁰	NaBH ₄ reduc- tion	10.77– 13.34 nm	Oxic 30 °C, pH 6.0±0.2	67	0.48	0.72	Zhu et al. (2017)	
	Goethite@bag- gase biochar Goethite@ straw biochar	Carbothermal reduction	NA	Охіс 25 °С, рН 6.0	25 25	0.74 0.66	2.96 2.64	Cai et al. (2021)	
	Kenaf bar bio- char supported nanoFe ⁰	NaBH ₄ reduc- tion	100 nm	Oxic pH 6.0	41	1.01	2.46	Liu et al. (2018)	
	Biochar (≤50 mesh) sup- ported nanoFe ⁰	NaBH ₄ reduc- tion	NA	Oxic 25 °C	17	4.11	24.18	Hasan et al. (2020)	
	BC-G@Fe ⁰	Carbothermal reduction	20–100 nm	Oxic 25 °C, pH 5.0	18	1.58	8.78	This study	

Table 1 (continued)

Metal ion	Adsorbent	Method	Size of nanoFe ⁰	Sorption conditions	Fe content (%)	Uptake Capacity (mmol g ⁻¹)	lron uptake Capacity (mmol g ⁻¹)	References
Ag ⁺	Bamboo derived biochar supported nanoFe ⁰	NaBH ₄ reduc- tion	26–40 nm	Oxic 22±0.5 ℃	NA	1.26	NA	Wang et al. (2017b)
	Fe ⁰ -biochar composite with chitosan (BBCF)	Dispersing and soldering commercial nanoFe ⁰ using chitosan	28 nm	Oxic 22±0.5 ℃	33	6.07	18.39	Zhou et al. (2014)
	Bamboo derived HNO ₃ acid modified nanoFe ⁰	NaBH ₄ reduc- tion	30.5 nm	Oxic 22±0.5 ℃	10	1.85	18.5	Wang et al. (2017a)
	BC-G@Fe⁰	Carbothermal reduction	20–100 nm	Oxic 25 °C, pH 5.0	18	1.91	10.61	This study

Bold represent the sample prepared from this study

The reduction of Ag^+ to Ag^0 was confirmed by XPS of BC-G@Fe⁰ after Ag^+ uptake (Fig. 6l). Moreover, the presence of Ag^+ on the surface of BC-G@Fe⁰ can be attributed to the oxidation of reduced Ag^0 and the precipitated Ag^+ compounds during Fe⁰ dissolving.

Kinetic and isotherm studies were carried out at the initial pH of 5 (Fig. 6h, i). The Ag⁺ removal increased in the first 10 min and reached equilibrium after 20 min. The data were fitted to both pseudo-first-order and pseudo-second-order models with R² values of 0.971 and 0.824 (Additional file 1: Table S2), respectively. The Langmuir (R²=0.99) and Freundlich (R²=0.74) models fitted to isotherm data favoring a monolayer model. The maximum Langmuir adsorption capacity was calculated to be 1.913 mmol g⁻¹.

BC-G@ Fe^0 shows the highest uptake capacity for Ag⁺, followed by Cu^{2+} and then Pb^{2+} . This is expected because their reduction potentials are in the following order from high to low Ag^+ (0.80 V)> Cu^{2+} (0.34 V)> Pb^{2+} (-0.13 V). In particular, the Langmuir capacity of Pb²⁺ is four and five times lower than that of Cu^{2+} and Pb^{2+} , respectively. Such low capacity is because its reduction potential is lower than H^+ (0.00 V), as a result, nanoFe⁰ in BC-G@Fe⁰ is mainly consumed by H⁺ during Pb²⁺ removal (reaction 8) (Busch et al. 2021). From stoichiometry calculations, one mole of nanoFe⁰ could uptake two moles of Ag⁺ and one mole Cu²⁺ via single-displacement reactions, respectively. However, the Langmuir capacity of Ag^+ is only 20% higher than that of Cu^{2+} , which is much lower than expected. Heavy metal removal by BC-G@Fe⁰ is a mass transfer process, where the metal ions migrate to the nanoFe⁰ surface and are followed by surface reduction and deposition. Despite BC-G@Fe⁰ showing a higher potential for Ag⁺ uptake than Cu²⁺ stoichiometrically, the exposed nanoFe⁰ surface area is limited. Once the exposed surfaces are occupied by the reduced heavy metal nanoparticles, the uptake is terminated. Hence, the overall Ag⁺ capacity is much less than the expected value.

Table 1 displays Pb^{2+} , Cu^{2+} and Ag^+ removal in aqueous solutions using different nanoFe⁰ adsorbents. Our BC-G@Fe⁰ shows higher uptake capacities for Pb²⁺, Cu²⁺ and Ag⁺ compared to some of the reported nanoFe⁰ adsorbents. For instance, nanoFe⁰ supported by reed biochar has a Pb²⁺ uptake capacity of 0.18 mmol g^{-1} (Zhu et al. 2017), which is lower than that of the present study. Additionally, BC-G@Fe⁰ exhibits a 13 times greater Cu²⁺ uptake capacity than that of amino-modified biochar supporting nanoFe⁰ (Yang et al. 2018). Furthermore, our BC-G@Fe⁰ exhibits a higher Ag^+ uptake capacity of 1.91 mmol g^{-1} in comparison to bamboo char supported nanoFe⁰ using the NaBH₄ method (Wang et al. 2017b). Li et al. (2020) produced hydrophilic biochar-nanoFe⁰, which had a higher Pb^{2+} uptake capacity than that of our BC-G@Fe⁰. (Li et al. 2020). This can be attributed to their hydrophilic biochar having a high adsorption capacity to Pb²⁺ because of its abundant functional groups. Similarly, expensive chitosan-stabilized nanoFe⁰ particles prepared by Chen et al. also exhibited a higher capacity for than this study (Chen et al. 2019) because chitosan has a high Pb²⁺ sorption capacity via complexation (Fan et al. 2020a). However, they have followed the NaBH₄ reduction method which involves hazardous chemicals

(Chen et al. 2019). Hasan et al. revealed approximately three times higher capacity for Cu^{2+} than this study (Hasan et al. 2020). However, they employed NaBH₄ reduction which is not sustainable for scale up removal of water contaminants. Zhou et al. showed three times higher sorption capacity for Ag⁺ than this study. They have also used chitosan which has an additional advantage of adsorbing Ag⁺ through chitosan amino group complexation, hence, uplifting the uptake of heavy metal ions (Zhou et al. 2014).

4 Conclusion

This study explored BC-G@Fe⁰ composite synthesis by two carbothermal reduction routes and their application to remove heavy metal ions. Route I employed direct carbothermal reduction of iron salt-impregnated biomass, which generated BC-G@Fe⁰-containing grapheneencapsulated Fe₃C nanoparticles. This route led to low heavy metal removal efficiency (i.e., $< 0.3 \text{ mmol g}^{-1}$ for Cu²⁺). Route II first pre-pyrolyzed biomass at 600 °C to biochar and then impregnated that biochar with iron salt. This was followed by carbothermal reduction. Carbonaceous gases (e.g., CH₄ and CO) were responsible for Fe₃C formation. Because they were removed during biomass pyrolysis, subsequent carbothermal reduction of iron salt-impregnated biochar gave BC-G@Fe⁰ containing graphene-encapsulated nanoFe⁰. This results in high heavy metal removal efficiency (i.e., 1.58 mmol g^{-1} for Cu). At our optimized conditions, i.e., the pre-pyrolyzing step employing FeCl₂ as the iron resource, 15% iron loading, 1000 °C carbonization for 1 h, the produced BC-G@ Fe^{0} had Pb^{2+} , Cu^{2+} , and Ag^{+} removal capacities of 0.30, 1.58, and 1.91 mmol g^{-1} , respectively. Future studies will focus on using BC-G@Fe⁰ to remove heavy metals from soil.

Supplementary Information

The online version contains supplementary material available at https://doi.org/10.1007/s42773-022-00196-5.

Additional file 1: Figure S1. Gas adsorption study of iron salts-derived BC-G@Fe⁰ (a) N₂ adsorption isotherms of iron salts-derived BC-G@Fe⁰. (b) Specific surface area and pore volume results. Figure S2. Gas adsorption study of BC-G@Fe⁰. X (a) N₂ adsorption isotherms of BC-G@Fe⁰-600-BC-G@Fe⁰-1000 (b) Specific surface area and pore volume results. Figure S3. Spot diameter distribution of the Fe⁰ nanoparticles made with different impregnated iron salts (route II) shown in the SEM images (Fig. 3h–k). Figure S4. SEM image and EDS elemental mapping of BC-G@Fe⁰-700. Figure S5. SEM image and EDS elemental mapping of BC-G@Fe⁰-900. Figure S6. SEM image and EDS elemental mapping of BC-G@Fe⁰-900. Figure S7. SEM image and EDS elemental mapping of BC-G@Fe⁰-100. Table S1. Fe content in all BC-G@Fe⁰ products prepared by route II. Table S2. Kinetic and Isotherm Parameters for Pb²⁺, Cu²⁺ and Ag⁺ Adsorptions onto BC-G@Fe⁰

Acknowledgements

The authors thank USDA-NIFA provide the funding support for this project. The authors also the Institute of Imaging and Analytical Technology, Mississippi State University (MSU) for providing access to XRD, SEM, and TEM characterizations. This manuscript is publication #SB1077 of the Department of Sustainable Bioproducts, MSU. This publication is a contribution of the Forest and Wildlife Research Center, MSU.

Author contributions

TNK: Investigation, Methodology, Data analysis, Writing original draft, Review & editing. RMON: Investigation, Methodology, Data analysis. CMN: Investigation, Methodology. PMR: Methodology, Data analysis. RVKGT: Methodology. CUPJr: Scientific discussion, Review & editing. YK: Funding acquisition, Scientific discussion; JZ: Funding acquisition, Scientific discussion; Review & editing. XZ: Funding acquisition, Project administration, Conceptualization, Investigation, Data analysis, Writing original draft, Review & editing. All authors read and approved the final manuscript.

Funding

This work was supported by the USDA National Institute of Food and Agriculture (NIFA) (Grant No. 2020-65210-30763).

Availability of data and materials

The authors declare that data will be made available on reasonable request.

Declarations

Competing interests

The authors declare no competing financial interests.

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Received: 22 August 2022 Revised: 1 December 2022 Accepted: 12 December 2022

Published online: 28 December 2022

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